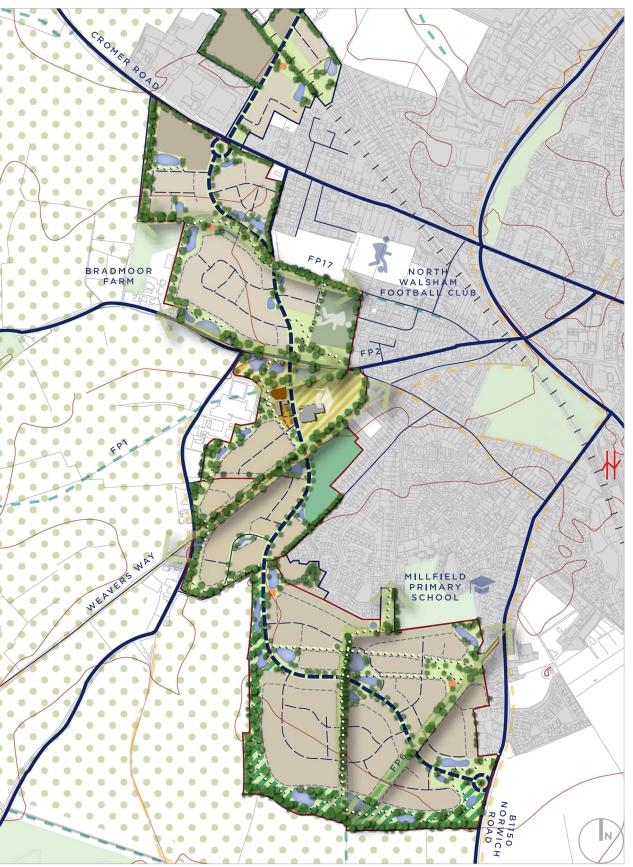
Appendix A – Masterplan





LEGEND Residentia**l** Employment Local Centre & Plaza School Link Road Proposed Vegetation Proposed Open Space Proposed Infiltration Basins Proposed Footpath Link Public Right of Way Recreational Route Brid**l**eway Existing Road Surrounding Countryside

North Walsham Train Station
Existing Green or Open Space
Secondary Local Facilities

LEAP

NEAP
Allotments
Sport Provision

Appendix B – Percentage Impact Assessment



								AM Po-	ak Hour	9	6 Impact As	sessment					DM Do	ak Hour				
					2029			AIVI Pe	ak noui	2036	_				2029		FIVI FE	ak nour		2036		
			Di		DS Vehicles	%	6 increase		DM Total \	DS /ehicles	-	% increase)	DM Total V	DS /ehicles		•	DM Total V	DS ehicles	3	% increas	se
	1 A to C		Turn	Arm	Turn Arm	Turn		Arm	Turn Arm	Turn Arm	Turn		Arm	Turn Arm	Turn Arm		Arm	Turn Arm		Arm	Turn	Arm
	A to C		2		2	3%	0		1	8	700%	53		4	4	-86% -1%		4	21 16		300%	
	A to D B to A	N Bradfield	0	2	0 2	0% -5%		3%	0 1	33 54	0% 533%		5300%	0 19	0 6	0% -13 0%	-67%	0 7	32 13	69	0% 62 160%	886%
Junction 1 -	B to C		354		354	0%	4		372	293	-21%	63		558	564	1%		571	476		-17%	
Bradfield Road / Cromer Road	B to D C to B	W Cromer	0 480	356	4 360 478	0% 0%		1%	0 375 507	126 438 375	0% -26%		17%	0 562 448	8 576 428	0% 14 -5%	2%	0 576 475	197 348	686	0% 110 -27%	19%
Priority Junction / Proposed Road	C to A	F 0	0	400	3	0%	8	00/	0	32	0%	1	00/	0	0	0%	40/	0	15	400	0%	00/
. repessa ridaa	C to D D to A	E Cromer	0	480	7 488	0% 0%		2%	0 507	101 508 45	0% 0%		0%	0 448	27 454 0	0% 6 0%	1%	0 475	99	462	0% -13 0%	-3%
	D to B	Link Road	0	0	7 39 46	0% 0%	46	_	0	73 343	0% 0%	343		0 0	4 18 22	0% 0% 22	_	0	185 86	291	0% 0% 291	
	Junction	LIIIK ROAU	Ü	838	897	070	59	7%	883	1343	076	460	52%	1029	1058	29	3%	1058	00	1508	450	43%
	A to B	W Cromer	78 277		69 329 398	-12% 19%	43	12%	83 288 371	0 380 380	-100% 32%	9	2%	93 481 574	102 490 593	10% 2% 19	3%	87 494 581	580	580	-100% 17% -1	0%
Junction 2 - Crome Road / Greens	r B to A		132		110	-17%	-14		105	0	-100%	-139		123	84	-32%		90	0		-100%	
Road Priority Junction	B to C C to B	S Greens	30 69	161	37 147 70	27% 1%	34	-9%	34 139 66	0 0	-100% -100%	40	-100%	60 183 81	66 150 80	10% -33 -1%	-18%	54 144 80	0	0	-100% -144 -100%	-100%
	C to A Junction	E Cromer	350	419 935	383 453 997	10%	63	8% 7%	402 468 978	508 508 888	26%	-90	9% -9%	325 406 1163	378 458 1200	16% 52 38	13% 3%	380 460 1185	466	466 1046	23% 6 -139	1% -12%
	A to D		29		29	1%		1 /0	29	30	3%		-3/0	54	54	0%	3 /0	55	53	1040	-4%	-12/0
	A to C	N B1145	250 168	447	250 170 449	0% 1%	2	0%	263 171 463	264 201 495	0% 18%	32	7%	298 191 543	296 193 543	0% 1% 0	0%	300 194 549	324 209	586	8% 8% 37	7%
	B to D	-	55		62	13%	50		54	53	-2%			137	152	11%		145	143		-1%	
Junction 3 - B1145 / A149 / A149	B to C	W Cromer	174 95	324	97 382	28%	58	18%	176 103 333	210 125 388	19% 21%	55	17%	263 141 542	268 148 568	2% 5% 27	5%	264 154 563	276 181	600	5% 18% 37	7%
Cromer Road / Cromer Road	C to D		0 235		0 265	0% 13%	29		0 283	285	0% 1%	15		23 213	20 264	-13% 24%		30 266	29 252		-3% -5%	
Signalised Junction	C to A	S A149	250	485	249 514	0%	29	6%	271 554	284 569	5%	2	3%	258 494	233 517	-9% 24	5%	279 575	283	564	1% -11	-2%
	D to C		2		2	15% 0%	0		2	2	0% 0%	0		9	9	1% 2%		9	9		0%	
	D to A	E Cromer	3	11	3 11	2%		3%	3 11	3 11	0%		0%	0 18	0 18	0% 0	1%	0 18	0	18	0% 0	0%
	Junction A to D		140	1267	1356	0%	89	7%	1361	1463	0%	102	7%	1597 149	1647	0%	3%	1705 148	148	1768	0%	4%
	A to C	N.M de alac.	0	440	0	0%	0	00/	0	0	0%	0	00/	0	0	0%	00/	0	0	4.40	0%	00/
	A to B B to D	N Mundesley	31	140	0 140 34	0% 11%		0%	0 148 32	0 148 32	0% 0%		0%	0 149 97	0 149	0% 0 4%	0%	0 148 98	99	148	0% 0 1%	0%
Junction 4 - Crome Road / Mundesley	2100	W Cromer	0 44	74	0 48 83	0% 11%	8	11%	0 43 75	0 40 72	0% -7%	-3	-4%	0 71 168	0 82 183	0% 16% 15	9%	0 74 172	73	172	-1% 0	0%
Road / Market Street / Aylsham	C to D	VV Gronioi	126		124	-2%		1170	134	127	-5%		170	133	123	-7%	070	138	140	112	1%	070
Road Signalised Junction	C to B	S Aylsham	249	375	0 250 374	0% 0%	-1	0%	0 258 392	0 284 411	0% 10%	19	5%	0 265 398	251 374	0% -5% -24	-6%	0 282 420	295	435	0% 5% 15	4%
	D to C	·	0		0	0%	0		0	0	0%	0		0	0	0%		0	0		0%	
	D to B	E Market	0	0	0 0	0% 0%	0	0%	0 0	0 0	0% 0%	0	0%	0 0	0 0	0% 0% 0	0%	0 0	0	0	0% 0% 0	0%
	Junction A to B		0	590	596	0%	7	1%	615	631	0%	16	3%	715	705	-9 0%	-1%	740	0	755	0%	2%
Junction 5 -	A to C	E Aylsham	0	0	0 0	0%	0	0%	0 0	0 0	0%	0	0%	0 0	0 0	0% 0	0%	0 0	0	0	0% 0	0%
Aylsham Road /	B to A B to C	W Aylsham	141	141	0 144	2% 0%	3	2%	146 0 146	172 0 172	18% 0%	26	18%	115 0 115	0 100	-13% 0% -15	-13%	115 0 115	147	147	28% 0% 32	28%
Park Lane Priority Junction	C to B	-	150 235		143 230 373	-5% -2%	-12	20/	168 247 415	208 237 445	24% -4%	30	7%	127 284 411	146 275 422	15%	20/	133 306 439	138 288	426	4%	20/
	C to A Junction	S Park	235	385 526	230 373 517	-270	-9	-3% -2%	247 415 561	237 445 617	-4%	56	10%	284 411 526	275 422 522	-3% 10 -4	3% -1%	306 439 554	200	426 573	-6% -13 19	-3% 3%
	A to B	E Aylsham	110 39		104 38 142	-6% -3%	-8	-5%	123 44 167	160 47 207	30% 7%	40	24%	93 34 127	107 39 146	15% 14% 19	15%	98 37 135	105 33	138	7% -11% 3	2%
Junction 6 - Aylsham Road /	B to A	L Aylanam	132		136	3%	4		137	162	18%	26	2470	99	84	-15%	1070	97	130		34%	
Skeyton New Road Priority Junction	B to C C to B	W Aylsham	2	135	2 138	-2% 2%		3%	2 139	3 165	50% 0%		19%	11 110 5	7 91	-39% -19 -1%	-17%	10 107 5	13	143	30% 36 0%	34%
1 Honly Sunction	C to A	S Skeyton	10		10 13	-1%	0	-1%	10 13	10 13	0%	0	0%	16 21	16 21	0% 0	0%	17 22	17	22	0% 0	0%
	Junction A to D		73	297	293 52	-28%	-4	-1%	77	0 385	-100%	66	21%	258 86	258 82	-5%	0%	264 82	0	303	-100%	15%
	A to C A to B	N Greens	25 50		32 55 139	26% 10%	-9	-6%	24 49 150	0 0	-100% -100%	-150	-100%	23 65 174	32 69 183	38% 6% 8	5%	20 65 167	0	0	-100% -100% -167	-100%
Junction 7 - B1145	B to D	IN CIECIIS	131		114	-13%		-0 /0	137	194	42%		-10076	103	98	-5%	370	115	201	U	75%	-10076
Aylsham Road / Aylsham Road /	B to C	W Aylsham	31	162	10 37 161	0% 22%	0	0%	0 34 171	0 194	-100%	23	13%	5 46 154	5 59 161	3% 26% 7	5%	6 41 162	6	207	0% -100% 45	28%
Greens Road / Tungate Road	C to D	,	34		29	-14%	_		34	34	0%	,		19	14	-27%		21	36		71%	
Crossroads	C to B	S Tungate	5	43	10 43	-1% 96%	0	0%	5 43	0 38	-100%	-5	-12%	23 46	23 41	-6% 4% -5	-10%	22 47	0	40	-100% -7	-15%

Junction	D to C		12		10	210/		12	20		2170/		12		12	110/			16		21		0.49/		
	D to C		13 126		126	-21% 0% -:	.8	12 142	38 230		217% 62% 9		13 81	-	12 78	-11% -4%			16 81	ŀ	31 173		94% 114%		
	D to A	E Aylsham	128		103 240	-19%		0% 105 259	0	268	-100%	3%	115	209	67 157	-41%	-52	-25%	82	179	0	204	-100%	25	14%
	Junction		00	619	582			623	404	500	-123	3 -20%	00	583	542	C0/	-41	-7%	40	555	04	451		-104	-19%
	A to B	E Aylsham	90		84 12 96	-7% -4%	7	98 14 112	121	145	23% 71%	29%	66 18	85	63 29 91	-6% 56%	7	8%	48 25	73	81 20	101	69% -20%	28	38%
Junction 8 -	B to A		81		81	0%	1	85	107		26% -24		70		58	-17%	<u> </u>	0,1	74		83		12%		00,0
Aylsham Road / Station Road	B to C	W Aylsham	156	237	115 196	-26%	-	7% 162 247	116	223	-28%	-10%	139	209	135 193	-2%	-15	-7%	146	220	100	183	-32%	-37	-17%
Priority Junction	C to B	S Station	177 39	216	157 42 199	-12% 8%	7	163 3% 41 204	109	152	-33% 5%	-25%	144 70	214	95 50 145	-34% -29%	-69	-32%	130 58	188	100	160	-54% 72%	-28	-15%
	Junction	3 Station	39	555	491		_	2% 563	40	520	-43		70	507	429	-2370	-78	-15%	30	481	100	444	12/0	-37	-8%
	A to B		3		3	0%)	3	9		200%		2		2	0%			2		2		0%		
Junction 9 - Station	A to C	E Skeyton	46	49	46 49	0%		1% 48 51	41	50	-15%	-2%	44	46	44 46	0%	0	0%	48	50	49	51	2%	1	2%
Road / Skeyton	B to A	N Station	5 162	167	122 128	-25%	10	4% 171 176	135	140	-21% -36	-20%	154	157	158 164	115% 3%	7	5%	170	173	117	120	-31%	-53	-31%
New Road Priority Junction	C to B		214		197	-8%		202	144		-29%		212		143	-32%		070	186		160	.20	-14%	00	0170
•	C to A	S Station	10		10 208	3%		7% 13 215	11	155	-15%	-28%	14	225	11 154	-20%	-71	-32%	18	204	17	177	-6%	-27	-13%
	Junction A to D		1	440	384	0%	6 -	3% 442	1	345	-97 0%	-22%	0	428	364	0%	-64	-15%	0	427	0	348	0%	-79	-19%
	A to C		0		0			0	0		0% 0		0	-	0	0%			0	F	0		0%		
	A to B	N Oak	2	3	2 3	0%		2 3	2	3	0%	0%	8	8	8 8	0%	0	0%	8	8	8	8	0%	0	0%
	B to D		167		138	-17%		178	163		-8%		152		158	4%			158	L	149		-6%		
Junction 10 -	B to C	W Station	42	208	0 169	-26%	10	9% 0 221	12	175	-72% -46 0%	-21%	43	198	41 3 202	-5% 0%	4	2%	57	218	13	165	-77% 0%	52	249/
Station Road / Oak Road / Skeyton	B to A C to D	W Station	28		28	0%		30	22	175	-27%	-21%	20	130	22	12%	4	Z70	22	۷10	33	100	50%	-53	-24%
Road Crossroads	C to B		64		65	1%		64	18	[-72% -54		32		33	4%			33	İ	75	ŀ	127%		
Junction	C to A	S Skeyton	0	92	0 93	0%		% 0 94	0	40	0%	-57%	0	52	0 56	0%	4	7%	0	55	0	108	0%	53	96%
	D to C		37 157		36 140	-3% -11%	7	43 151	32 135		-26% -11% -28		41 185	-	113	-39%			38 163	ŀ	73 95		92% -42%		
	D to A	E Station	137	207	14 191	11%		3% 19 213	18	185	-5%	-13%	4	230	4 159	-39%	-72	-31%	4	205	4	172	0%	-33	-16%
	Junction			511	455			1% 531		403	-12			488	425		-64	-13%		486		453		-33	-7%
	A to D		25		20	-17%		25	23		-8%		18		18	-2%			20		20		0%		
	A to C		143		130	-9%	.9	155	146		-6% -25		132	-	150	14%			136	<u> </u>	137		1%		
	A to B A to A	N Station	15 12		3 166	-15% -76%		5% 15 210	15	185	-93%	-12%	12	172	12	-2% -89%	9	5%	13	179	20	180	54% -70%	1	1%
	B to D	14 Otation	0	100	0	0%		0	0	100	0%	1270	2	172	2	0%	<u> </u>	370	2	173	2	100	0%		170
	B to C		21		21	0%)	23	23]	0%		2		2	0%			2		2		0%		
Junction 11 -	B to A		64		64	0%		65	76		17%		10		10	-1%			10		10		0%		
Station Road / Millfield Road /	B to B C to D	W Morris	0	85	0 85	0% 0%		0 88	0	99	0% 0%	13%	0	14	0 14	0% 0%	0	0%	0	14	0	14	0% 0%	0	0%
Morris Road Mini-	C to B		9		13	42%		13	12	1	-8%		4		4	3%			5	ŀ	5		0%		
roundabout	C to A		132		120	-9%	9	136	102		-25%	,	168		108	-36%			141		111		-21%		
	C to C	S Millfield	11	152	0 133	-100%	_	2% 10 159	0	114	-100%	-28%	3	175	0 112	-100%	-62	-36%	4	150	0	116	-100%	-34	-23%
	D to C		0		0	0%		0	0		0%		0	-	0	0% 0%			0	F	0	ŀ	0% 0%		
	D to A		0		4	0%	1	0	12	1	0% 12		43		40	-7%			43	ŀ	48		12%		
	D to D	E Station	0	0	0 4	0%		0 0	0	12	0%	#DIV/0!	0	43	0 40	0%	-3	-7%	0	43	0	48	0%	5	12%
	Junction			432	388		4 -	0% 457		410	-47	-10%		403	347		-57	-14%		386		358		-28	-7%
	A to B	N Norwich	73 311		78 334 412	7% 7%	8	92 356 448	81 387	468	-12% 9%	4%	56 417	472	54 429 483	-3% 3%	11	2%	80 443	523	113 516	629	41% 16%	106	20%
Junction 12 - B1150 Norwich	B to A	N NOIWICH	86		73	-16%		92	119	400	20%		39	412	45	15%	- 11	270	55	323	74	029	35%	100	2070
Road / Millfield	B to C	W Millfield	124	210	103 176	-17%	-	6% 130 222	78	197	-40%	-11%	71	109	78 123	10%	13	12%	63	118	43	117	-32%	-1	-1%
Road Priority Junction	C to B	0.11	104		78	-25%	3	92	60		-35% 41		141	507	83	-41%		4.401	102	550	32	400	-69%	00	4704
Sanotion	C to A Junction	S Norwich	332	436 1029	371 449 1037	12%		% 356 448 % 1118	429	489 1154	21%	9% 3%	396	537 1119	395 478 1083	0%	-59 -35	-11% -3%	457	559 1200	431	463 1209	-6%	-96 9	-17% 1%
	A to B		25		29	18%		25	32	1134	28%		42	1113	41	-3%	.55	370	47	1200	45	1203	-4%	J	1 /0
Junction 13 -	A to C	N Norwich	383		413 442	8%	3	447 472	466	498	4% 26	6%	469	511	481 522	2%	11	2%	516	563	626	671	21%	108	19%
B1150 Norwich	B to A	W/ Ot-1:	71	74	67	-5%	4	74	63	<u> </u>	-15%	4.00	43	47	41	-5%	,	50 /	49		48	50	-2%	,	00/
Road / Station Road Priority	B to C C to B	W Station	0	71	0 67	10%		0 74	1	64	0% 400%	-14%	10	47	3 44	-11% -15%	-2	-5%	12	53	13	52	0% 8%	-1	-2%
Junction	C to A	S Norwich	410	412	435 437	6%	5	452 453	546	551	21%	22%	417	427	426 435	2%	8	2%	502	514	494	507	-2%	-7	-1%
	Junction			891	946	5		999		1113	114	11%		985	1001		16	2%		1130		1230		100	9%
	A to D		66		64	-3%		76	77		1%		60		60	0%			65	Ţ	67	7	3%		
	A to C A to B	E Norwich	219 152		213 150 427	-3% -1%	1	268 2% 182 526	270 189	536	1% 10 4%	2%	223 118	401	224 117 400	1% -1%	-1	0%	257 141	463	317 147	531	23% 4%	68	15%
	B to D	L HOIWICH	143		151	5%		153	165	330	8%	2 /0	279	701	279	0%	-1	0 70	272	700	288	551	6%	00	1370
Junction 14 -	B to C		160		197	23%	9	168	172]	2% 27		233		240	3%			238	į	241		1%		
B1150 Norwich	B to A	N A149	121		125 473	3%		1% 129 450	140	477	9%	6%	63	575	59 577	-7%	2	0%	60	570	70	599	17%	29	5%
Road / A149 / Norwich Road	C to D		50 154		50 181	18%	3	56 184	108 170		93% -8% 73		52 148	-	53 171	3% 15%			60 204	-	94 167		57% -18%		
Signalised Junction		W Norwich	273	477	269 500	-2%		3% 290 530	325	603	12%	14%	253	453	240 465	-5%	11	2%	288	552	280	541		-11	-2%
	D to C		29		32	10%		36	51		42%	,	55		59	6%			65	- /-	114	2 1 1	75%		
	D to B		179		181		5	184	207		13% 48		228		231	1%			230		244	,	6%		
	D to A	S A149	126	335 1674	126 340 1739	0%		% 125 345 1851	135	393 2009	8% 158	14%	95	378 1808	94 383 1825	-1%	5 17	1%	95	390 1975	100	458 2129	5%	68 154	17% 8%
	Junction			10/4	1/39		6	1851		2009	158	9%		1000	1823		17	1%		19/0		2129		104	070

	A to B		61		63		5%			64		63		-2%			51		50	-1%			78		87		12%		
	A to C		22		24		8%	5		22		32		45%	9		20		20	0%			20		33		65%		
	A to A	N King's	0	82	0	87	0%		6%	0	86	0	95	0%		10%	0	71	0 70	0%	0	0%	0	98	0	120	0%	22	22%
Junction 15 -	B to A		196		193		-1%			203		199		-2%			166		172	3%			183		155		-15%		
Grammar School	B to C		310		314		1%	0		323		384		19%	55		240		220	-9%			257		293		14%		
Road / King's Arms Street Mini-	B to B	W Grammar	15	521	14	521	-7%		0%	19	545	17	600	-11%		10%	4	411	1 392	-75%	-18	-4%	5	445	3	451	-40%	6	1%
roundabout	C to B		364		352		-3%			445		460		3%			351		351	0%			382		441		15%		
Touridabout	C to A		127	l	123		-4%	-17		156		181		16%	40		155		160	3%			181		185		2%		
	C to C	E Grammar	0	492	0	475	0%		-3%	0	601	0	641	0%		7%	0	506	0 511	0%	5	1%	0	563	0	626	0%	63	11%
	Junction			1095		1083		-12	-1%		1232		1336	1	104	8%		987	973		-14	-1%		1106		1197		91	8%
	A to B		145		148		2%			160		183		14%			93		90	-3%		.,,,	99		106		7%		
	A to C	S B1145	203	348	201	349	-1%	1	0%	216	376	227	410	5%	34	9%	306	399	292 383	-4%	-16	-4%	336	435	358	464	7%	29	7%
Junction 22 -	B to A	0 2 1 1 10	77	0.0	77	0.0	0%		070	83	0.0	89		7%		070	165		166	1%		170	165	.00	187		13%		. ,,
B1145 / Laundry	B to C	W Laundry	0	77	0	77	0%	0	0%	0	83	0	89	0%	6	7%	8	173	8 174	-1%	1	1%	8	173	8	195	0%	22	13%
Loke Priority	C to B	VV Edundry	12		12		0%		070	12		12	- 00	0%		1 70	6	110	5	-16%		170	5	110	5	100	0%		1070
Junction	C to A	N B1145	370	382	371	383	0%	1	0%	380	392	407	419	7%	27	7%	378	384	378 383	0%	-1	0%	384	389	400	405	4%	16	4%
	Junction	14 11 143	370	808	371	809	070	2	0%	300	851	401	918	. 70	67	8%	570	956	940	070	-16	-2%	304	997	400	1064	770	67	7%
	A to D		17	000	17	003	00/	2	0 70	10	001	18	310	-5%	01	0 /0	4	330	4	Ω0/.	-10	-2 /0	4	331	1	1004	00/	01	1 70
	A to C		184	-	184		0%	0		195		207			14		120		121	0%			124		132	-	60/		
	A to B	N B1145	49	250	49	250	0%	U	0%	50	264	53	270	6%	14	5%	39	164	39 164	0%	0	0%	124	100	40	176	-2%	7	4%
		N B1145		250		250			0%	50	204		278			5%	15	104		0%	U	0%	41	169	40	176	-2%		4%
	B to D		52	-	52		0%	0		<u> </u>		53		-2%	40		10		15	1%			10		16	-	0%		
Junction 23 -	B to C		179		180		0%	U		181		194		- 70	10		155		155	0%			158		163		3%		
B1145 / Lyngate	B to A	E Lyngate	48	280	48	280	-1%		0%	50	285	48	295	-4%		4%	70	240	70 240	0%	1	0%	73	247	72	251	-1%	4	2%
Road / Folgate	C to D		26		26		-1%			27		26		-4%			15		14	-10%			10		18		13%		
Road Staggered Crossroads	C to B		56		56		0%	-17		59		60		270	-17		150		146	-3%			163		172		6%		
Ciossidads	C to A	S B1145	120	202	119	201	-1%		-1%	131	217	142	228	8%		5%	148	313	140 299	-6%	-17	-4%	161	340	175	365	9%	-17	7%
	D to C		19		19		0%			19		19		0%			109		107	-2%			110		109		-1%		
	D to B		21	ļ	21		1%	0		21		21		0%	0		67		67	0%			68		68		0%		
	D to A	W Folgate	13	53	13	53	-1%		0%	13	53	13	53	0%		0%	21	197	21 195	0%	-2	-1%	21	199	21	198	0%	-1	-1%
	Junction			785		784		-1	0%		819		854		35	4%		913	898		-15	-2%		955		990		35	4%

								AM Do	ak Hour	% Impact	Assessmer	nt (with Mi	tigation)				DM Doc	ak Hour				
					2029			AIVI FE		2036					2029		FIVI FE			2036		
			D		DS Vehicles	% i	increase		DM Total \	DS /ehicles	-	% increase	•	DM Total V	DS /ehicles	% increase		DM Total V	DS ehicles		% increas	se
	A to C		Turn 0	Arm	Turn Arm	Turn 0%	Į.	Arm	Turn Arm	Turn Arm	Turn 0%		Arm	Turn Arm	Turn Arm	Turn A	Arm	Turn Arm	Turn A	Arm	Turn 600%	Arm
	A to B	N Prodfield	2	,	2	3%	0	20/	1	8 33 54	700%	53	5300%	4 0 19	4 0 6	-1%	670/	4	16	69	300%	9969/
	A to D B to A	N Bradfield	2		2	-5%		3%	3	19	533%		5300%	4	4	0% -13 0%	-67%	5	13	69	0% 62 160%	886%
Junction 1 - Bradfield Road /	B to C	W Cromer	354 0	356	354 4 360	0% 0%	4	1%	372 0 375	293 126 438	-21% 0%	63	17%	558 0 562	564 8 576	1% 0% 14	2%	571 0 576	476 197	686	-17% 0% 110	19%
Cromer Road Priority Junction /	C to B		480		478	0% 0%	8		507	375 32	-26% 0%	1		448	428	-5% 0%		475	348 15		-27% 0%	
Proposed Road	C to D	E Cromer	0	480	7 488	0%	Ů	2%	0 507	101 508	0%		0%	0 448	27 454	0% 6	1%	0 475	99	462	0% -13	-3%
	D to A D to B		0		7	0% 0%	46		0	45 225	0% 0%	343		0	4	0% 0%		0	20 185		0% 0%	
	D to C Junction	Link Road	0	0 838	39 46 897	0%	59	7%	0 0	73 343 1343	0%	460	52%	0 0 1029	18 22 1058	0% 22 29	3%	0 0 1058	86	291 1508	0% 291 450	43%
	A to B	W Cromor	78 277		69	-12% 19%	43	12%	83 288 371	0 380 380	-100% 32%	9		93 481 574	102	10%		87 494 581	0 580		-100%	
Junction 2 - Cromer Road / Greens	B to A	W Cromer	132		329 398 110	-17%	-14		105	0	-100%	-139	2%	123	84	2% 19 -32%	3%	90	0	580	17% -1 -100%	0%
Road Priority Junction	B to C C to B	S Greens	30 69		37 147 70	27% 1%		-9%	34 139 66	0 0	-100% -100%		-100%	60 183 81	66 150 80	10% -33 -1%	-18%	54 144 80	0	0	-100% -144 -100%	-100%
Junction	C to A Junction	E Cromer	350	419 935	383 453 997	10%	63	8% 7%	402 468 978	508 508 888	26%	-90	9% -9%	325 406 1163	378 458 1200	16% 52 38	13% 3%	380 460 1185	466	466 1046	23% 6 -139	1% -12%
	A to D		29		29	1%		1 /0	29	30	3%		-370	54	54	0%	370	55	53	1040	-4%	-12/0
	A to C	N B1145	250 168	447	250 170 449	0% 1%	2	0%	263 171 463	264 201 495	0% 18%	32	7%	298 191 543	296 193 543	0% 1% 0	0%	300 194 549	324 209	586	8% 8% 37	7%
haration 0. B4445	B to D		55 174		62 223	13% 28%	58		54 176	53 210	-2% 19%	55		137 263	152 268	11% 2%		145 264	143 276		-1% 5%	
Junction 3 - B1145 / A149 / A149	B to A	W Cromer	95		97 382	2%	33	18%	103 333	125 388	21%		17%	141 542	148 568	5% 27	5%	154 563	181	600	18% 37	7%
Cromer Road / Cromer Road	C to D		235		265	0% 13%	29		283	285	0% 1%	15		23	20 264	-13% 24%		30 266	29 252		-3% -5%	
Signalised Junction	C to A D to C	S A149	250 2	485	249 514	0% 15%		6%	271 554	284 569	5% 0%		3%	258 494 9	233 517	-9% 24 1%	5%	279 575 9	283	564	1% -11 0%	-2%
	D to B	5.0	6		6	0%	0	00/	6	6	0%	0	00/	9	9	2%	407	9	9	40	0%	201
	D to A Junction	E Cromer	3	11 1267	3 11 1356	2%	89	3% 7%	3 11 1361	3 11 1463	0%	102	0% 7%	0 18 1597	0 18 1647	0% 0 51	1% 3%	0 18 1705	0	18 1768	0% 0 63	0% 4%
	A to D		140		140	0% 0%	0		148	148	0% 0%	0		149	149	0% 0%		148	148		0% 0%	
	A to B	N Mundesley	0	140	0 140	0% 11%		0%	0 148 32	0 148 32	0%		0%	0 149 97	0 149	0% 0 4%	0%	0 148 98	0	148	0% 0	0%
Junction 4 - Cromer	2.00		0		0	0%	8		0	0	0% 0%	-3		0	0	0%		0	0		1% 0%	
Road / Mundesley Road / Market	B to A C to D	W Cromer	44 126		48 83 124	11% -2%		11%	43 75 134	40 72 127	-7% -5%		-4%	71 168 133	82 183 123	16% 15 -7%	9%	74 172 138	73 140	172	-1% 0 1%	0%
Street / Aylsham Road Signalised	C to B	S Aylsham	0 249		0 250 374	0% 0%	-1	0%	0 258 392	0 284 411	0% 10%	19	5%	0 265 398	0 251 374	0% -5% -24	60/	0 282 420	0 295	435	0% 5% 15	4%
Junction	D to C	S Ayisilalii	0	3/3	0	0%		U%	0	0	0%		5%	0	0	0%	-6%	0	0	430	0%	476
	D to B	E Market	0	0	0 0	0% 0%	0	0%	0 0	0 0	0% 0%	0	0%	0 0	0 0	0% 0% 0	0%	0 0	0	0	0% 0% 0	0%
	Junction A to B		0	590	596	0%	7	1%	615	631	0%	16	3%	715	705	-9 0%	-1%	740	0	755	15 0%	2%
Junction 5 -	A to C	E Aylsham	0	0	0 0	0%	0	0%	0 0	0 0	0%	0	0%	0 0	0 0	0% 0	0%	0 0	0	0	0% 0	0%
Aylsham Road / Park Lane Priority	B to A	W Aylsham	141	l	0 144	2% 0%	3	2%	146 0 146	0 172	18% 0%	26	18%	115 0 115	0 100	-13% 0% -15	-13%	115 0 115	147 0	147	28% 0% 32	28%
Junction	C to B	S Park	150 235		143 230 373	-5% -2%	-12	-3%	168 247 415	208 237 445	24% -4%	30	7%	127 284 411	146 275 422	15% -3% 10	3%	133 306 439	138 288	426	4% -6% -13	-3%
	Junction			526	517		-9	-2%	561	617		56	10%	526	522	-4	-1%	554		573	19	3%
haratian 0	A to B A to C	E Aylsham	110 39		104 38 142	-6% -3%	-8	-5%	123 44 167	160 47 207	30% 7%	40	24%	93 34 127	107 39 146	15% 14% 19	15%	98 37 135	105 33	138	7% -11% 3	2%
Junction 6 - Aylsham Road /	B to A	W Aylsham	132	135	136 2 138	3% -2%	4	3%	137 2 139	162 3 165	18% 50%	26	19%	99	84 7 91	-15% -39% -19	-17%	97 10 107	130	143	34% 30% 36	34%
Skeyton New Road Priority Junction	C to B		3 10		3	2% -1%	0		3	3	0% 0%	0		5	5	-1%		5	5		0%	
	C to A Junction	S Skeyton		297	10 13 293	-1%	-4	-1% -1%	10 13 319	10 13 385	0%	66	0% 21%	258	16 21 258	0% 0	0% 0%	264	17	22 303	0% 0 39	0% 15%
	A to D A to C		73 25		52 32	-28% 26%	-9		77 24	0	-100% -100%	-150		86	82 32	-5% 38%		82 20	0		-100% -100%	
	A to B	N Greens	50	148	55 139 114	10%		-6%	49 150 137	0 0	-100%		-100%	65 174 103	69 183 98	6% 8	5%	65 167 115	0 201	0	-100% -167	-100%
Junction 7 - B1145 Aylsham Road /	B to D B to C		0		10	-13% 0%	0		0	0	42% 0%	23		5	5	-5% 3%		6	6		75% 0%	
Aylsham Road / Greens Road /	B to A C to D	W Aylsham	31 34		37 161 29	22% -14%		0%	34 171 34	0 194 34	-100% 0%		13%	46 154 19	59 161 14	26% 7 -27%	5%	41 162 21	0 36	207	-100% 45 71%	28%
Tungate Road Crossroads	C to B	S Tungate	4	43	4 10 43	-1% 96%	0	0%	4 5 43	4 0 38	0% -100%	-5	-12%	4 23 46	4 23 41	-6%	-10%	4 22 47	4	40	0%	-15%
lunation	C to A	3 Turigate	၁	43	10 43	90%		U70	0 43	0 38	-100%		-12%	23 40	23 41	4% -5	-10%	22 41	U	40	-100% -7	-15%

Junction	D to C		12		10	210/		12	20		2170/		12		12	110/			16		21		0.49/		
	D to C		13 126		126	-21% 0% -:	.8	12 142	38 230		217% 62% 9		13 81	-	12 78	-11% -4%			16 81	ŀ	31 173		94% 114%		
	D to A	E Aylsham	128		103 240	-19%		0% 105 259	0	268	-100%	3%	115	209	67 157	-41%	-52	-25%	82	179	0	204	-100%	25	14%
	Junction		00	619	582			623	404	500	-123	3 -20%	00	583	542	C0/	-41	-7%	40	555	04	451		-104	-19%
	A to B	E Aylsham	90		84 12 96	-7% -4%	7	98 14 112	121	145	23% 71%	29%	66 18	85	63 29 91	-6% 56%	7	8%	48 25	73	81 20	101	69% -20%	28	38%
Junction 8 -	B to A		81		81	0%	1	85	107		26% -24		70		58	-17%	<u> </u>	0,1	74		83		12%		00,0
Aylsham Road / Station Road	B to C	W Aylsham	156	237	115 196	-26%	-	7% 162 247	116	223	-28%	-10%	139	209	135 193	-2%	-15	-7%	146	220	100	183	-32%	-37	-17%
Priority Junction	C to B	S Station	177 39	216	157 42 199	-12% 8%	7	163 3% 41 204	109	152	-33% 5%	-25%	144 70	214	95 50 145	-34% -29%	-69	-32%	130 58	188	100	160	-54% 72%	-28	-15%
	Junction	3 Station	33	555	491		_	2% 563	40	520	-43		70	507	429	-2370	-78	-15%	30	481	100	444	1270	-37	-8%
	A to B		3		3	0%)	3	9		200%		2		2	0%			2		2		0%		
Junction 9 - Station	A to C	E Skeyton	46	49	46 49	0%		1% 48 51	41	50	-15%	-2%	44	46	44 46	0%	0	0%	48	50	49	51	2%	1	2%
Road / Skeyton	B to A	N Station	5 162	167	122 128	-25%	10	4% 171 176	135	140	-21% -36	-20%	154	157	158 164	115% 3%	7	5%	170	173	117	120	-31%	-53	-31%
New Road Priority Junction	C to B		214		197	-8%		202	144		-29%		212		143	-32%		070	186		160	.20	-14%	00	0170
•	C to A	S Station	10		10 208	3%		7% 13 215	11	155	-15%	-28%	14	225	11 154	-20%	-71	-32%	18	204	17	177	-6%	-27	-13%
	Junction A to D		1	440	384	0%	6 -	3% 442	1	345	-97 0%	-22%	0	428	364	0%	-64	-15%	0	427	0	348	0%	-79	-19%
	A to C		0		0			0	0		0% 0		0	-	0	0%			0	F	0		0%		
	A to B	N Oak	2	3	2 3	0%		2 3	2	3	0%	0%	8	8	8 8	0%	0	0%	8	8	8	8	0%	0	0%
	B to D		167		138	-17%		178	163		-8%		152		158	4%			158	L	149		-6%		
Junction 10 -	B to C	W Station	42	208	0 169	-26%	10	9% 0 221	12	175	-72% -46 0%	-21%	43	198	41 3 202	-5% 0%	4	2%	57	218	13	165	-77% 0%	52	249/
Station Road / Oak Road / Skeyton	B to A C to D	W Station	28		28	0%		30	22	175	-27%	-21%	20	130	22	12%	4	Z70	22	۷10	33	100	50%	-53	-24%
Road Crossroads	C to B		64		65	1%		64	18	[-72% -54		32		33	4%			33	İ	75	ŀ	127%		
Junction	C to A	S Skeyton	0	92	0 93	0%		% 0 94	0	40	0%	-57%	0	52	0 56	0%	4	7%	0	55	0	108	0%	53	96%
	D to C		37 157		36 140	-3% -11%	7	43 151	32 135		-26% -11% -28		41 185	-	113	-39%			38 163	ŀ	73 95		92% -42%		
	D to A	E Station	137	207	14 191	11%		3% 19 213	18	185	-5%	-13%	4	230	4 159	-39%	-72	-31%	4	205	4	172	0%	-33	-16%
	Junction			511	455			1% 531		403	-12			488	425		-64	-13%		486		453		-33	-7%
	A to D		25		20	-17%		25	23		-8%		18		18	-2%			20		20		0%		
	A to C		143		130	-9%	.9	155	146		-6% -25		132	-	150	14%			136	<u> </u>	137		1%		
	A to B A to A	N Station	15 12		3 166	-15% -76%		5% 15 210	15	185	-93%	-12%	12	172	12	-2% -89%	9	5%	13	179	20	180	54% -70%	1	1%
	B to D	14 Otation	0	100	0	0%		0	0	100	0%	1270	2	172	2	0%	<u> </u>	370	2	173	2	100	0%		170
	B to C		21		21	0%)	23	23]	0%		2		2	0%			2		2		0%		
Junction 11 -	B to A		64		64	0%		65	76		17%		10		10	-1%			10		10		0%		
Station Road / Millfield Road /	B to B	W Morris	0	85	0 85	0% 0%		0 88	0	99	0% 0%	13%	0	14	0 14	0% 0%	0	0%	0	14	0	14	0% 0%	0	0%
Morris Road Mini-	C to B		9		13	42%		13	12	1	-8%		4		4	3%			5	ŀ	5		0%		
roundabout	C to A		132		120	-9%	9	136	102		-25%	,	168		108	-36%			141		111		-21%		
	C to C	S Millfield	11	152	0 133	-100%	_	2% 10 159	0	114	-100%	-28%	3	175	0 112	-100%	-62	-36%	4	150	0	116	-100%	-34	-23%
	D to C		0		0	0%		0	0		0%		0	-	0	0% 0%			0	F	0	ŀ	0% 0%		
	D to A		0		4	0%	1	0	12	1	0% 12		43		40	-7%			43	ŀ	48		12%		
	D to D	E Station	0	0	0 4	0%		0 0	0	12	0%	#DIV/0!	0	43	0 40	0%	-3	-7%	0	43	0	48	0%	5	12%
	Junction			432	388		4 -	0% 457		410	-47	-10%		403	347		-57	-14%		386		358		-28	-7%
	A to B	N Norwich	73 311		78 334 412	7% 7%	8	92 356 448	81 387	468	-12% 9%	4%	56 417	472	54 429 483	-3% 3%	11	2%	80 443	523	113 516	629	41% 16%	106	20%
Junction 12 - B1150 Norwich	B to A	N NOIWICH	86		73	-16%		92	119	400	20%		39	412	45	15%	- 11	270	55	323	74	029	35%	100	2070
Road / Millfield	B to C	W Millfield	124	210	103 176	-17%	-	6% 130 222	78	197	-40%	-11%	71	109	78 123	10%	13	12%	63	118	43	117	-32%	-1	-1%
Road Priority Junction	C to B	0.11	104		78	-25%	3	92	60		-35% 41		141	507	83	-41%		4.401	102		32	400	-69%	00	4704
Sanotion	C to A Junction	S Norwich	332	436 1029	371 449 1037	12%		% 356 448 % 1118	429	489 1154	21%	9% 3%	396	537 1119	395 478 1083	0%	-59 -35	-11% -3%	457	559 1200	431	463 1209	-6%	-96 9	-17% 1%
	A to B		25		29	18%		25	32	1134	28%		42	1113	41	-3%	.55	370	47	1200	45	1203	-4%	J	1 /0
Junction 13 -	A to C	N Norwich	383		413 442	8%	3	447 472	466	498	4% 26	6%	469	511	481 522	2%	11	2%	516	563	626	671	21%	108	19%
B1150 Norwich	B to A	W/ Ot-1:	71	74	67	-5%	4	74	63	<u> </u>	-15%	4.00	43	47	41	-5%	,	50 /	49		48	50	-2%	,	00/
Road / Station Road Priority	B to C C to B	W Station	0	71	0 67	10%		0 74	1	64	0% 400%	-14%	10	47	3 44	-11% -15%	-2	-5%	12	53	13	52	0% 8%	-1	-2%
Junction	C to A	S Norwich	410	412	435 437	6%	5	452 453	546	551	21%	22%	417	427	426 435	2%	8	2%	502	514	494	507	-2%	-7	-1%
	Junction			891	946	5		999		1113	114	11%		985	1001		16	2%		1130		1230		100	9%
	A to D		66		64	-3%		76	77		1%		60		60	0%			65	Ţ	67	7	3%		
	A to C A to B	E Norwich	219 152		213 150 427	-3% -1%	1	268 2% 182 526	270 189	536	1% 10 4%	2%	223 118	401	224 117 400	1% -1%	-1	0%	257 141	463	317 147	531	23% 4%	68	15%
	B to D	L HOIWICH	143		151	5%		153	165	330	8%	2 /0	279	701	279	0%	-1	0 70	272	700	288	551	6%	00	1370
Junction 14 -	B to C		160		197	23%	9	168	172]	2% 27		233		240	3%			238	į	241		1%		
B1150 Norwich	B to A	N A149	121		125 473	3%		1% 129 450	140	477	9%	6%	63	575	59 577	-7%	2	0%	60	570	70	599	17%	29	5%
Road / A149 / Norwich Road	C to D		50 154		50 181	18%	3	56 184	108 170		93% -8% 73		52 148	-	53 171	3% 15%			60 204	-	94 167		57% -18%		
Signalised Junction		W Norwich	273	477	269 500	-2%		3% 290 530	325	603	12%	14%	253	453	240 465	-5%	11	2%	288	552	280	541		-11	-2%
	D to C		29		32	10%		36	51		42%	,	55		59	6%			65	- /-	114	2 1 1	75%		
	D to B		179		181		5	184	207		13% 48		228		231	1%			230		244	,	6%		
	D to A	S A149	126	335 1674	126 340 1739	0%		% 125 345 1851	135	393 2009	8% 158	14%	95	378 1808	94 383 1825	-1%	5 17	1%	95	390 1975	100	458 2129	5%	68 154	17% 8%
	Junction			10/4	1/39		6	1851		2009	158	9%		1000	1823		17	1%		19/0		2129		104	070

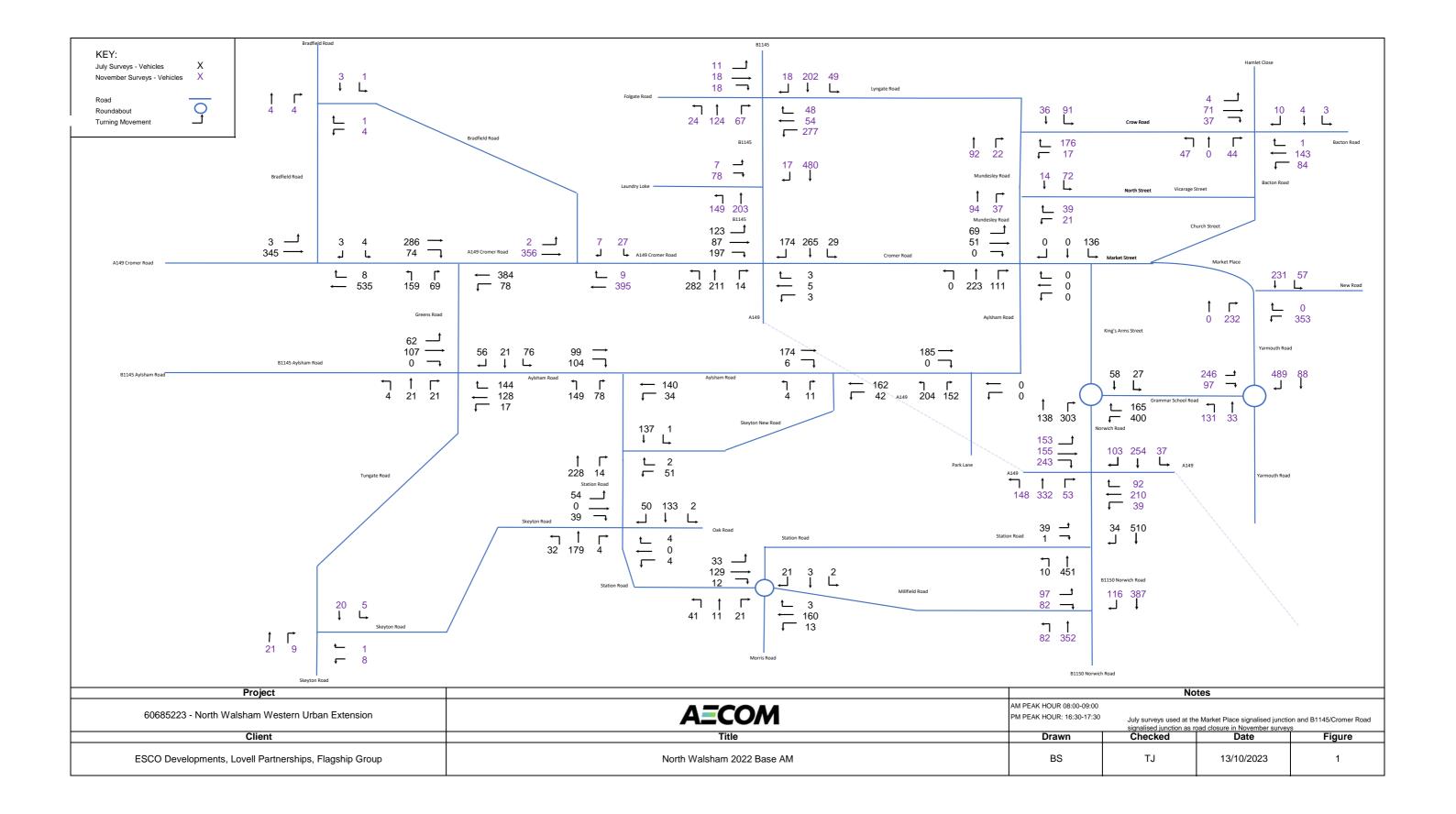
	A to B		61		63		5%			64		63		-2%			51		50	-1%			78		87		12%		
	A to C		22		24		8%	5		22		32		45%	9		20		20	0%			20		33		65%		
	A to A	N King's	0	82	0	87	0%		6%	0	86	0	95	0%		10%	0	71	0 70	0%	0	0%	0	98	0	120	0%	22	22%
Junction 15 -	B to A		196		193		-1%			203		199		-2%			166		172	3%			183		155		-15%		
Grammar School	B to C		310		314		1%	0		323		384		19%	55		240		220	-9%			257		293		14%		
Road / King's Arms Street Mini-	B to B	W Grammar	15	521	14	521	-7%		0%	19	545	17	600	-11%		10%	4	411	1 392	-75%	-18	-4%	5	445	3	451	-40%	6	1%
roundabout	C to B		364		352		-3%			445		460		3%			351		351	0%			382		441		15%		
Touridabout	C to A		127	l	123		-4%	-17		156		181		16%	40		155		160	3%			181		185		2%		
	C to C	E Grammar	0	492	0	475	0%		-3%	0	601	0	641	0%		7%	0	506	0 511	0%	5	1%	0	563	0	626	0%	63	11%
	Junction			1095		1083		-12	-1%		1232		1336	1	104	8%		987	973		-14	-1%		1106		1197		91	8%
	A to B		145		148		2%			160		183		14%			93		90	-3%		.,,,	99		106		7%		
	A to C	S B1145	203	348	201	349	-1%	1	0%	216	376	227	410	5%	34	9%	306	399	292 383	-4%	-16	-4%	336	435	358	464	7%	29	7%
Junction 22 -	B to A	0 2 1 1 10	77	0.0	77	0.0	0%		070	83	0.0	89		7%		070	165		166	1%		170	165	.00	187		13%		. ,,
B1145 / Laundry	B to C	W Laundry	0	77	0	77	0%	0	0%	0	83	0	89	0%	6	7%	8	173	8 174	-1%	1	1%	8	173	8	195	0%	22	13%
Loke Priority	C to B	VV Edundry	12		12		0%		070	12		12	- 00	0%		1 70	6	110	5	-16%		170	5	110	5	100	0%		1070
Junction	C to A	N B1145	370	382	371	383	0%	1	0%	380	392	407	419	7%	27	7%	378	384	378 383	0%	-1	0%	384	389	400	405	4%	16	4%
	Junction	14 11 143	370	808	371	809	070	2	0%	300	851	401	918	. 70	67	8%	570	956	940	070	-16	-2%	304	997	400	1064	770	67	7%
	A to D		17	000	17	003	00/	2	0 70	10	001	18	310	-5%	01	0 /0	4	330	4	Ω0/.	-10	-2 /0	4	331	1	1004	00/	01	1 70
	A to C		184	-	184		0%	0		195		207			14		120		121	0%			124		132	-	60/		
	A to B	N B1145	49	250	49	250	0%	U	0%	50	264	53	270	6%	14	5%	39	164	39 164	0%	0	0%	124	100	40	176	-2%	7	4%
		N B1145		250		250			0%	50	204		278			5%	15	104		0%	U	0%	41	169	40	176	-2%		4%
	B to D		52	-	52		0%	0		<u> </u>		53		-2%	40		10		15	1%			10		16	-	0%		
Junction 23 -	B to C		179		180		0%	U		181		194		- 70	10		155		155	0%			158		163		3%		
B1145 / Lyngate	B to A	E Lyngate	48	280	48	280	-1%		0%	50	285	48	295	-4%		4%	70	240	70 240	0%	1	0%	73	247	72	251	-1%	4	2%
Road / Folgate	C to D		26		26		-1%			27		26		-4%			15		14	-10%			10		18		13%		
Road Staggered Crossroads	C to B		56		56		0%	-17		59		60		270	-17		150		146	-3%			163		172		6%		
Ciossidads	C to A	S B1145	120	202	119	201	-1%		-1%	131	217	142	228	8%		5%	148	313	140 299	-6%	-17	-4%	161	340	175	365	9%	-17	7%
	D to C		19		19		0%			19		19		0%			109		107	-2%			110		109		-1%		
	D to B		21	ļ	21		1%	0		21		21		0%	0		67		67	0%			68		68		0%		
	D to A	W Folgate	13	53	13	53	-1%		0%	13	53	13	53	0%		0%	21	197	21 195	0%	-2	-1%	21	199	21	198	0%	-1	-1%
	Junction			785		784		-1	0%		819		854		35	4%		913	898		-15	-2%		955		990		35	4%

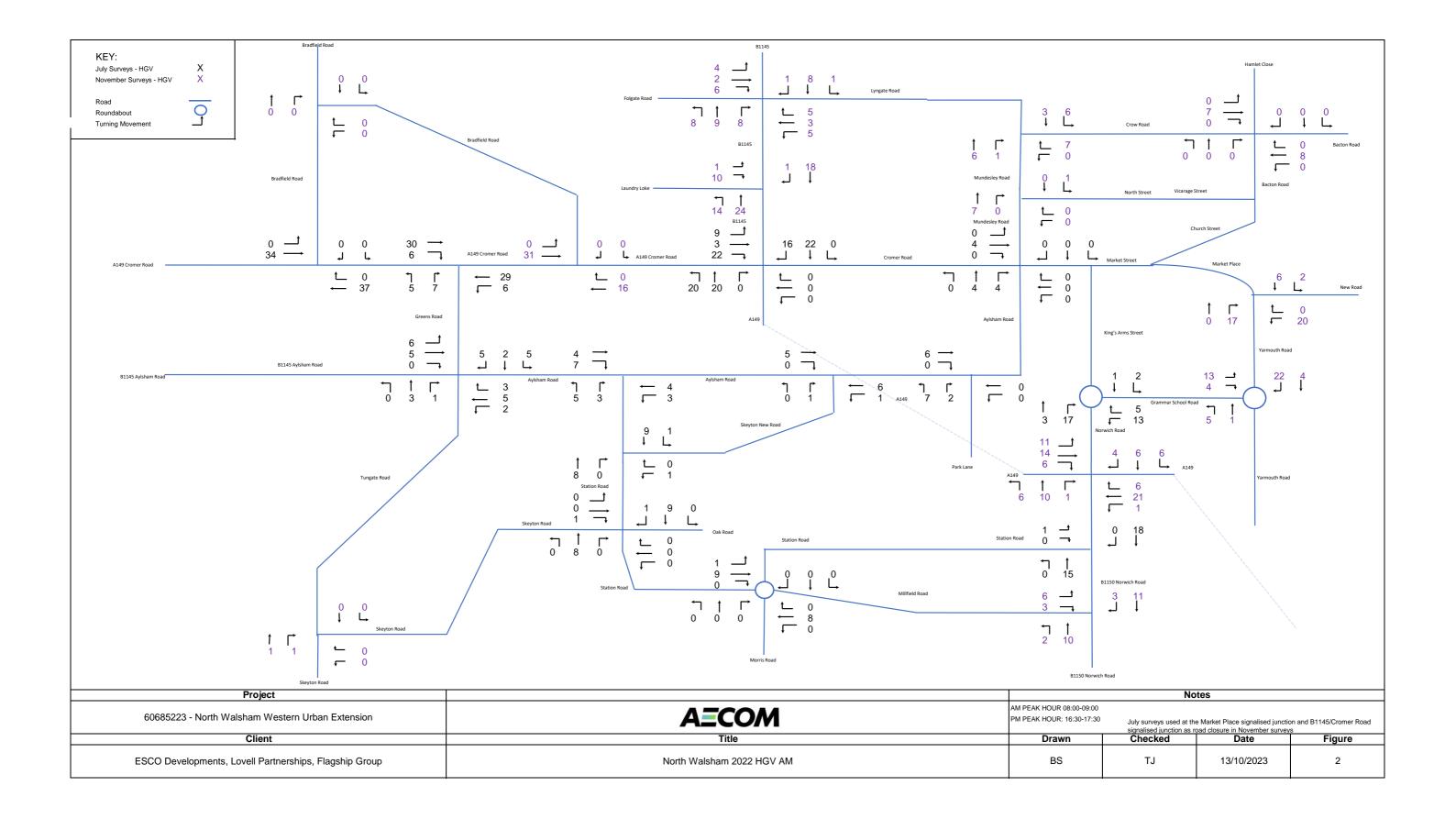
													% Impact As	sessment															
								AM Pe	ak Hour													PM Pe	ak Hour						
			DM		2029 DS	1			D	м		2036 S	1			DI	М	DS	2029	ı				M		2036 OS	1		
		-		al Vehicles			% increase				/ehicles		- ,	% increase				/ehicles	<u>, </u>		% increase				/ehicles		-	6 increase	
			Turn Arm	Turn		Turn		Arm		Arm		Arm	Turn		Arm		Arm		Arm	Turn		Arm		Arm		Arm	Turn		Arm
	A to D	-	105 639		105 670	0% 5%			107 660		111 839		4% 27%			146 548		146 553		0% 1%			153 564	-	158 630	-	3% 12%		
	A to B	E Norwich	7		7	0%	•		7		8	1	14%			10		10		-4%			9	1	9		0%		
	A to A		0 751		0 783	0%	32	4%	4	778	0	958	-100%	180	23%	0	704	0	708	0%	4	1%	4	730	0	797	-100%	67	9%
	B to D	-	10		0	0%			12		12		0%			3		10		-2%			2		11	<u> </u>	50%		
Junction 1 -	B to A	S Millfield	10		10	1% -1%			9		10	1	0% 11%			7		7		-2% 3%			12		8	_	-8% 0%		
Rectory Road /	B to B		0 21		0 21	0%	0	0%	0	21	0	22	0%	1	5%	0	20	0	20	0%	0	0%	0	22	0	22	0%	0	0%
B1150 Norwich Road / Mill Road	C to D	-	86		85	-1%			84		87		4%			99		100		1%			100		103	<u>.</u>	3%		
Mini-Roundabout	C to B	W Norwich	571		578	6% 1%			602		659		0% 9%			639		670		-2% 5%			672		802	<u>:</u>	0% 19%		
	C to C		0 664		0 670	0%	6	1%	0	693	0	753	0%	60	9%	0	740	0	771	0%	31	4%	0.2	774	0	907	0%	133	17%
	D to C		108		108	0%			108		109		1%			80		80		0%			84		82	!	-2%		
	D to B	N Rectory	150		151	5% 1%			154		152	-	-1%			127		126		15% 0%			129		131	4	0% 2%		
	D to D	14 Rectory	0 261		0 263	0%	2	1%	0	266	0	265	0%	-1	0%	0	208	0	208	0%	0	0%	0	213	0	213	0%	0	0%
	Junction		1696	_	1736		40	2%		1758		1998		240	14%		1673		1708		35	2%		1739		1939		200	12%
	A to D		511		543	6% 0%			524		714		36% 0%			422		426		1% 0%			449	1	512	1	14% 0%		
	A to B	N High	54		54	0%			57		62	1	9%			42		40		-4%			37		43	8	16%		
	A to A		0 565		0 597	0%	33	6%	0	581	0	776	0%	195	34%	0	463	0	466	0%	3	1%	0	486	0	555	0%	69	14%
	B to D	-	234	:	234	0% 0%			237		233		-2% 0%			273		273		0% 0%			273		275	<u> </u>	1% 0%		
Junction 2 - B1150	B to A	E B1354	37		37	1%			35		37	1	6%			43		44		1%			46	1	45	4	-2%		
Norwich Road / B1354 Church	B to B		0 271		0 271	0%	0	0%	0	272	0	270	0%	-2	-1%	0	316	0	317	0%	1	0%	0	319	0	320	0%	1	0%
Street / High Street	C to D		0		0	0%			0		0		0% 0%			0		0		0% 0%			0		0	1	0% 0%		
/ Petrol Station Gyratory	C to B	S Petrol	0		0	0% 0%			0		0	1	0%			0		0		0%			0	1	0	1	0%		
2,1,	C to C		0 0		0 0	0%	0	0%	0	0	0	0	0%	0	0%	0	0	0	0	0%	0	0%	0	0	0	0	0%	0	0%
	D to C		349		350	0% 0%			368		360		0% -2%			264		262		-1%			271	-	274	1	0% 1%		
	D to A	W Norwich	401		407	2%	•		407		470	1	15%			498		527		6%			519	1	675		30%		
	D to D		0 750		0 758	0%	8	1%	0	775	0	830	0%	55	7%	0	762	0	789	0%	27	4%	0	790	0	949	0%	159	20%
	Junction A to B		1586 553	_	1626 587	6%	41	3%	574	1628	764	1876	33%	248	15%	437	1541	441	1572	1%	31	2%	456	1595	527	1824	16%	229	14%
	A to C	E Station	1 554		1 588	-4%	34	6%	2	576	2	766	0%	190	33%	1	438	1	442	0%	4	1%	0	456	0	527	0%	71	16%
Junction 3 - High Street / Station	B to A		422		428	1%			421		487	1	16%			522		552		6%			544	-	704		29%		
Road Priority	B to C C to B	S High	15 437		16 444	2% -1%	6	1%	15	436	16	503	7%	67	15%	18 27	540	18 27	570	-3% 0%	30	6%	17 27		16 27		-6%	159	28%
Junction	C to A	N High	2 11		2 10	-3%	0	-1%	1	10	1	10	0% 0%	0	0%	8	36	9	36	1%	0	0%	10	4	10	-	0% 0%	0	0%
	Junction	ŭ	1002	2	1043		40			1022		1279		257			1014		1048		34			1054		1284		230	
	A to D		34		34	0% 0%			30		32		7% 0%			28		28		-1% 0%			25	1	25	1	0% 0%		
	A to B	N Rectory	24 57		24 57	0%	0	0%	25	55	25	57	0%	2	4%	17	45	18	45	1%	0	0%	20	45	18	43	-10%	-2	-4%
	B to D		236		235	0%			241		238		-1%			289		288		0%			289		304		5%		
Junction 4 - Church	B to C	E D40E4	50 288		2 51 288	0% 1%		00/	4	294	50	292	0%	2	40/	0	314	26	314	0%	0	00/	0	242	25	220	0%	47	F0/
Loke / B1354 / Rectory Road	B to A C to D	E B1354	50 288 4		4	1%	0	0%	49	294	30	292	2% 50%	-2	-1%	26 2	314	20	314	1% 0%	0	0%	23	312	3	329	9% 50%	17	5%
Crossroads	C to B		4		4	0%			4		4]	0%			2		2		3%			4]	4		0%		
Junction	C to A	S Church	0 8		0 8	0%	0	1%	0	6	0	7	0%	1	17%	0	4	0	4	0%	0	1%	0	6	0	7	0%	1	17%
	D to C	-	333		10 332	3% 0%			13 343		13 340	1	-1%			267		264		-17% -1%			268		282	1	0% 5%		
	D to A	W B1354	62 404		61 404	-1%	-1	0%	64	420	63	416	-2%	-4	-1%	36	304	36	302	0%	-3	-1%	36	305	37	320	3%	15	5%
	Junction	A	758	_	758		-1	0%		775		772	-	-3	0%		668	227	665	- 10:	-3	0%		668		699		31	5%
Link 5 - B1150 Norwich Road, at	A to B B to A	A - to West B - to East	743 751 149 ⁴		778 756 1533	5% 1%	39	3%	759 784	1543	948 837	1	25% 7%	242	16%	695 762	1457	699 790	1489	1% 4%	32	2%	720 800	-	785 947		9% 18%	212	14%
bridge	Junction	J to East	1494	_	1533	1 70	39		704	1543	037	1785	1 70	242		702	1457	730	1489	7/0	32		000	1520	547	1732	1076	212	
1:10 1:: 0:		A - to North	438		444	1%			438		504	45	15%			540		569		5%			564	4	720		28%		
Link 6 - High Street	B to A Junction	B - to South	563 1001 1001	_	597 1041 1041	6%	40	4% 4%	579	1017 1017	775	1279 1279	34%	262 262	26% 26%	463	1003	467	1037	1%	33 33	3% 3%	487	1051 1051	558	1278 1278	15%	227 227	22% 22%
	JULICUOIT		100		1041	1	40	4 /0		1017		12/9		202	2070		1003		1031		33	370		1001		12/0		221	22/0

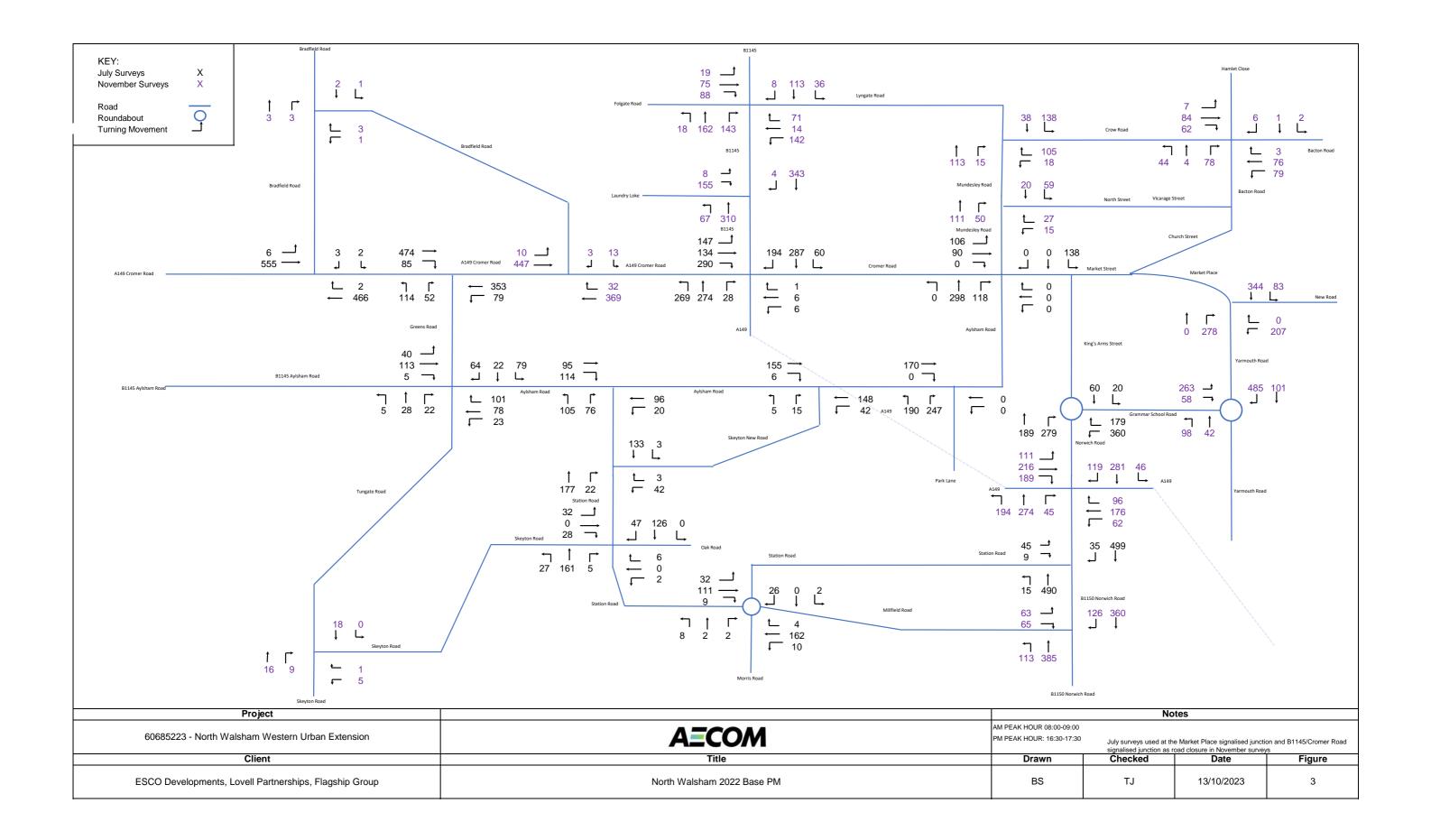
													% Impact As	sessment	(with Mitig	gation)													
								AM Pe	ak Hour													PM Pe	ak Hour						
			DM	DS	2029				D	м	Г п	2036 S	1			DI	м	DS	2029	1				M		2036 DS	1		
				I Vehicles		q	% increase				/ehicles	<u> </u>		% increase	,			/ehicles			% increase				/ehicles		-	% increase	
			Turn Arm	Turn Arı	m T	Turn		Arm		Arm		Arm	Turn		Arm		Arm		Arm	Turn		Arm		Arm		Arm	Turn		Arm
	A to D		105 639	105 670		0%			107 660		111 839		4%			146 548		146 553		0% 1%			153 564	-	158 630	-	3%		
	A to B	E Norwich	7	7	-	5% 0%			7		8		27% 14%			10		10		-4%			9	ł	9	5	12% 0%		
	A to A		0 751	0	783	0%	32	4%	4	778	0	958	-100%	180	23%	0	704	0	708	0%	4	1%	4	730	0	797	-100%	67	9%
	B to D		0	0		0%			0		0		0%			3		3		-2%			2		3	3	50%		
	B to C	S Millfield	10	11	-	1% -1%			12		12		0% 11%			11		10		-2% 3%			12	-	11		-8% 0%		
Junction 1 - Rectory Road /	B to B	O Willing City	0 21	0	21	0%	0	0%	0	21	0	22	0%	1	5%	0	20	0	20	0%	0	0%	0	22	0	22	0%	0	0%
B1150 Norwich	C to D		86	85		-1%			84		87		4%			99		100		1%			100		103	3	3%		
Road / Mill Road Mini-Roundabout	C to B	M/ Norwich	7	8		6% 1%			7		659		0%			2		670		-2%			672	-	2	2	0%		
	C to A	W Norwich	571 0 664	578	670	0%	6	1%	602	693	059	753	9% 0%	60	9%	639	740	0	771	5% 0%	31	4%	672	774	800	905	19% 0%	131	17%
	D to C		108	108	0.0	0%		170	108		109		1%	- 00	070	80		80		0%	Ü.	170	84		82		-2%	101	,
	D to B		3	3		5%			4		4		0%			1		1		15%			0		0)	0%		
	D to A	N Rectory	150 0 261	151	263	1% 0%	. 2	1%	154	266	152	265	-1% 0%	-1	0%	127	208	126	208	0% 0%	0	0%	129	213	131	213	2% 0%	0	0%
	Junction		1696		1736	076	40		U	1758	0	1998	076	240		0	1673	U	1708	0%	35		0	1739	0	1937	076	198	
	A to D		511	543		6%			524		716		37%			422		426		1%			449		510		14%		
	A to C		0	0		0%			57		62		0%			0		0		0%			0		0	0	0%		
	A to B	N High	54 0 565	54	597	0% 0%	33	6%	0	581	0	778	9% 0%	197	34%	42	463	40	466	-4% 0%	3	1%	37	486	43	553	16% 0%	67	14%
	B to D		234	234	00.	0%		070	237		233		-2%		0170	273	.00	273	.00	0%	Ů	170	273		275		1%	0.	. 170
	B to C		0	0		0%			0		0		0%			0		0		0%			0		0)	0%		
Junction 2 - B1150 Norwich Road /	B to A	E B1354	37 0 271	37	271	1% 0%	. 0	0%	35	272	37	270	6% 0%	-2	-1%	43	316	44	317	1% 0%	1	0%	46	319	45	320	-2% 0%	1	0%
B1354 Church	C to D		0 2/1	0	2/1	0%	U	076	0	212	0	270	0%	-2	-170	0	310	0	317	0%	-	0%	0	319	0	320	0%	-	076
Street / High Street / Petrol Station	C to B		0	0		0%			0		0		0%			0		0		0%			0]	0)	0%		
Gyratory	C to A	S Petrol	0	0		0%		00/	0	•	0		0%	•	00/	0		0	•	0%	•	00/	0		0	0	0%		00/
	C to C		0 0	0	0	0% 0%	0	0%	0	0	0	0	0% 0%	0	0%	0	0	0	0	0% 0%	0	0%	0	0	0	0	0% 0%	0	0%
	D to B		349	350		0%			368		360		-2%			264		262		-1%			271	1	274	Į.	1%		
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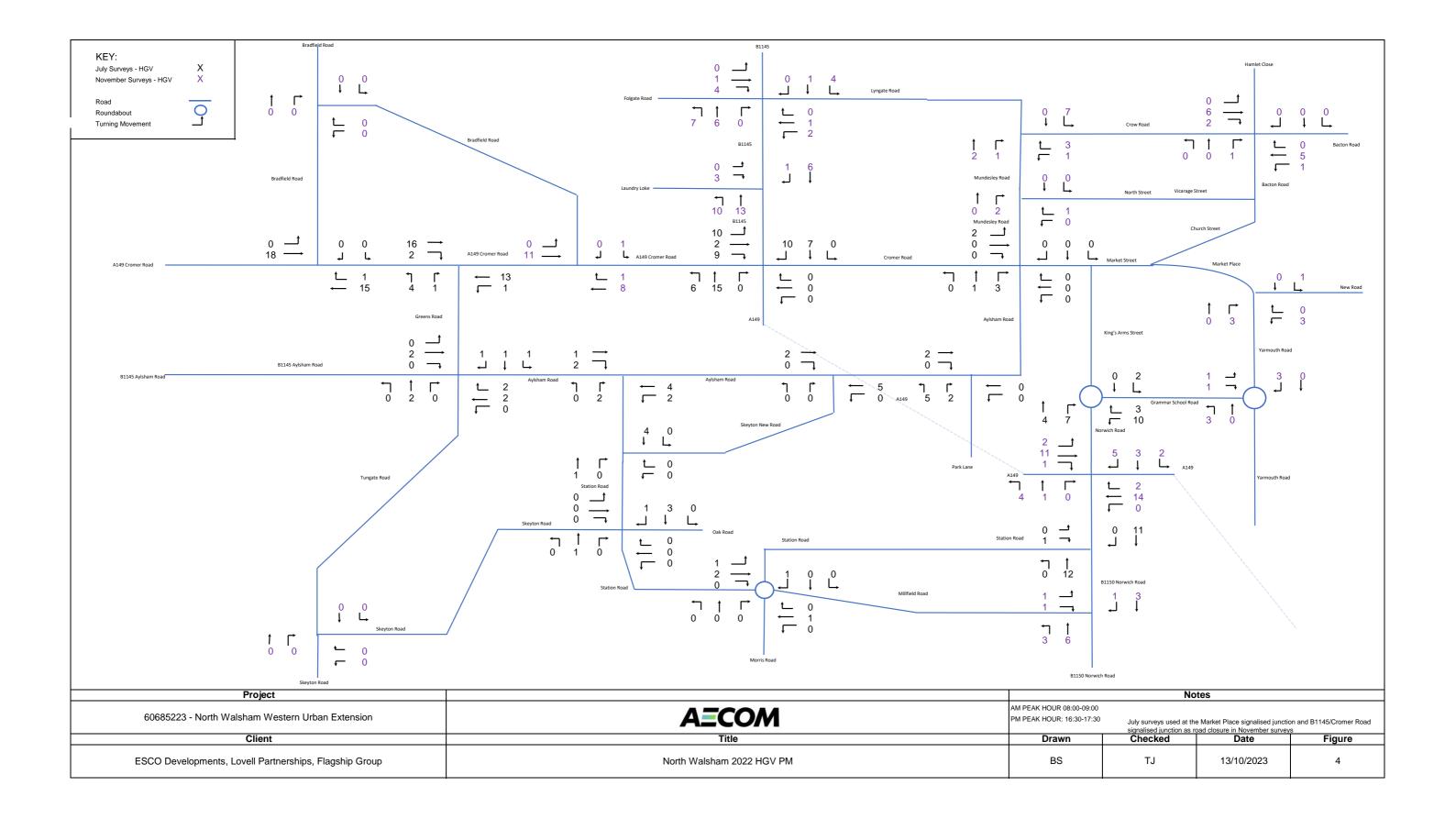
Appendix C – Flow Diagrams

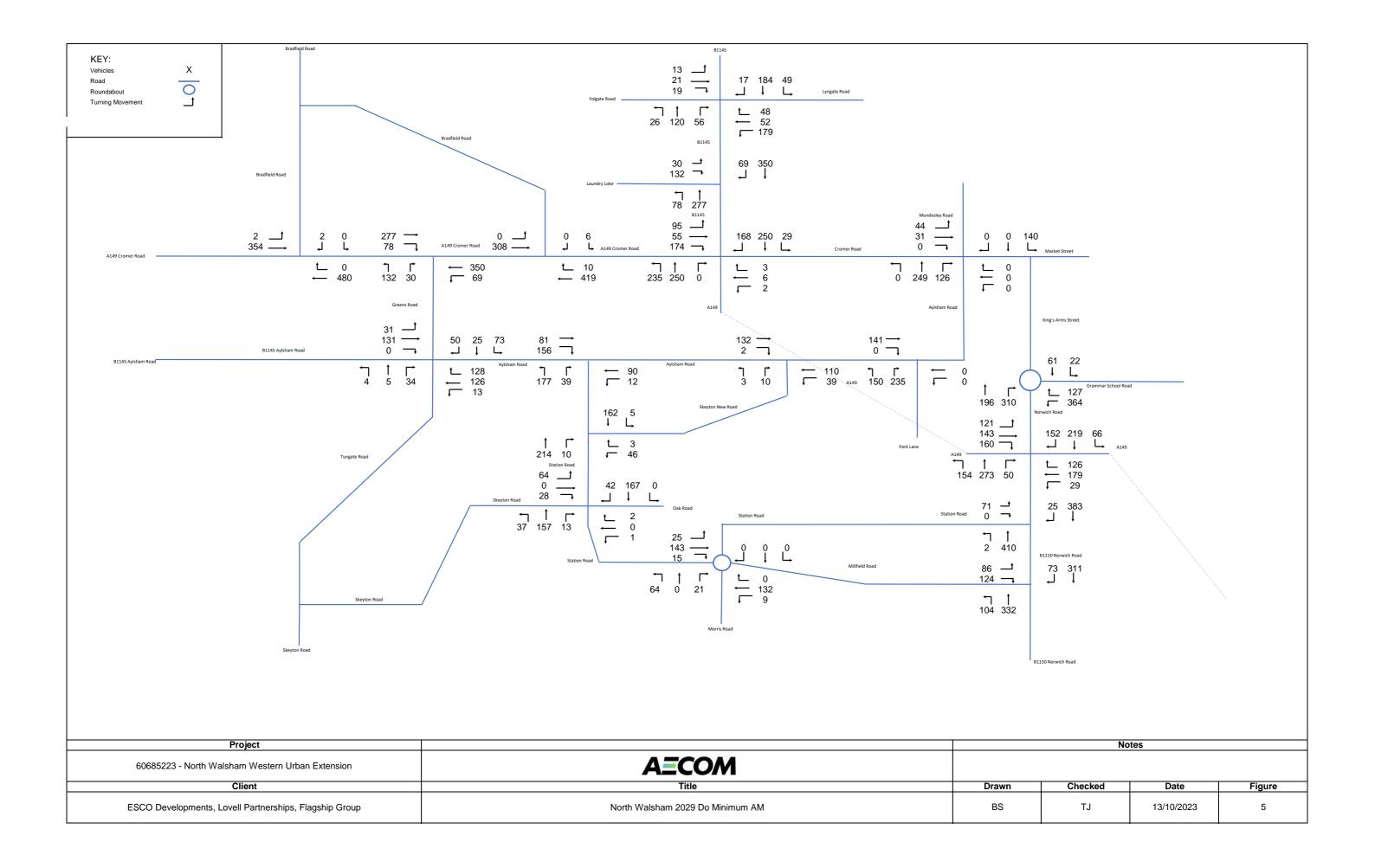


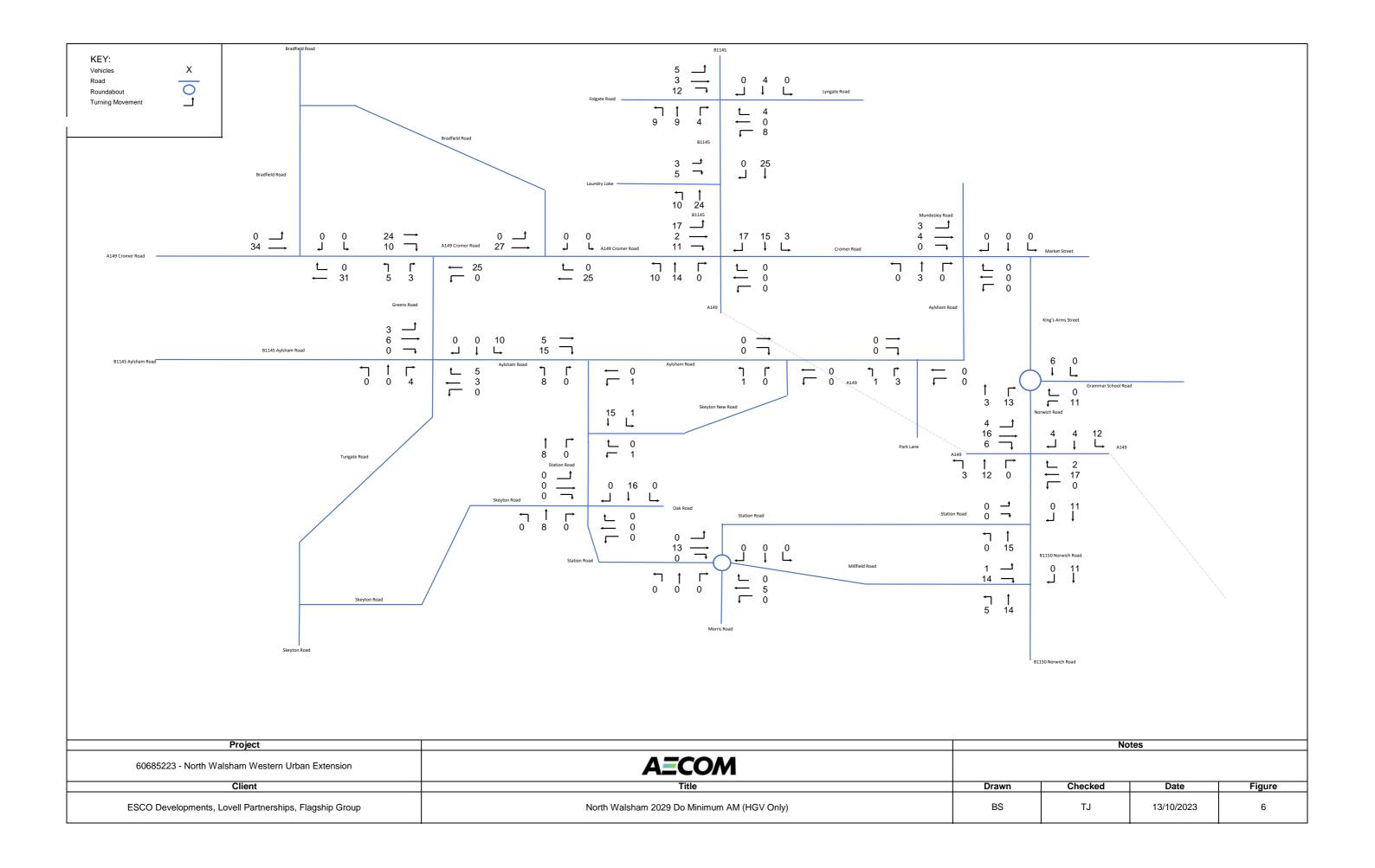


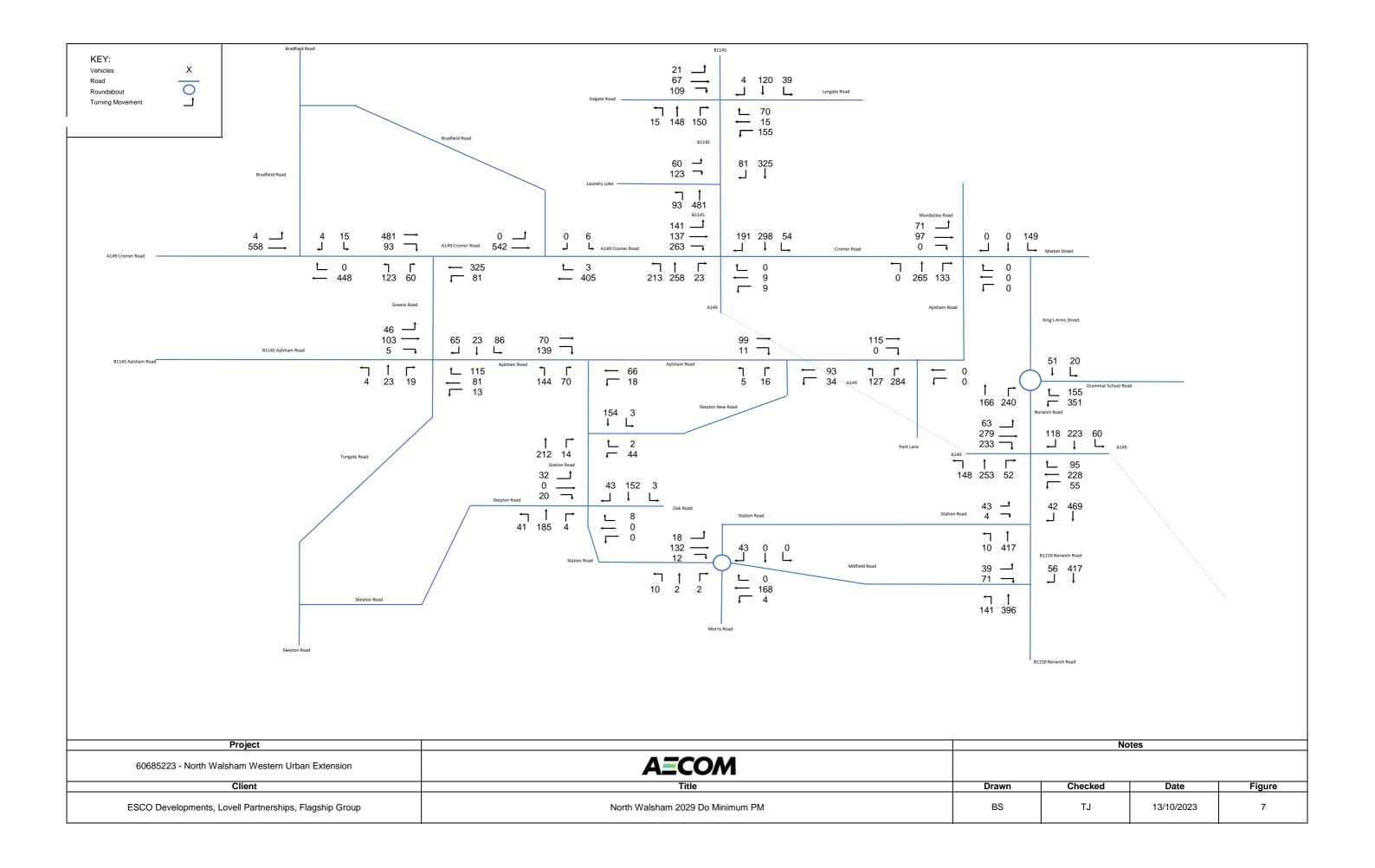


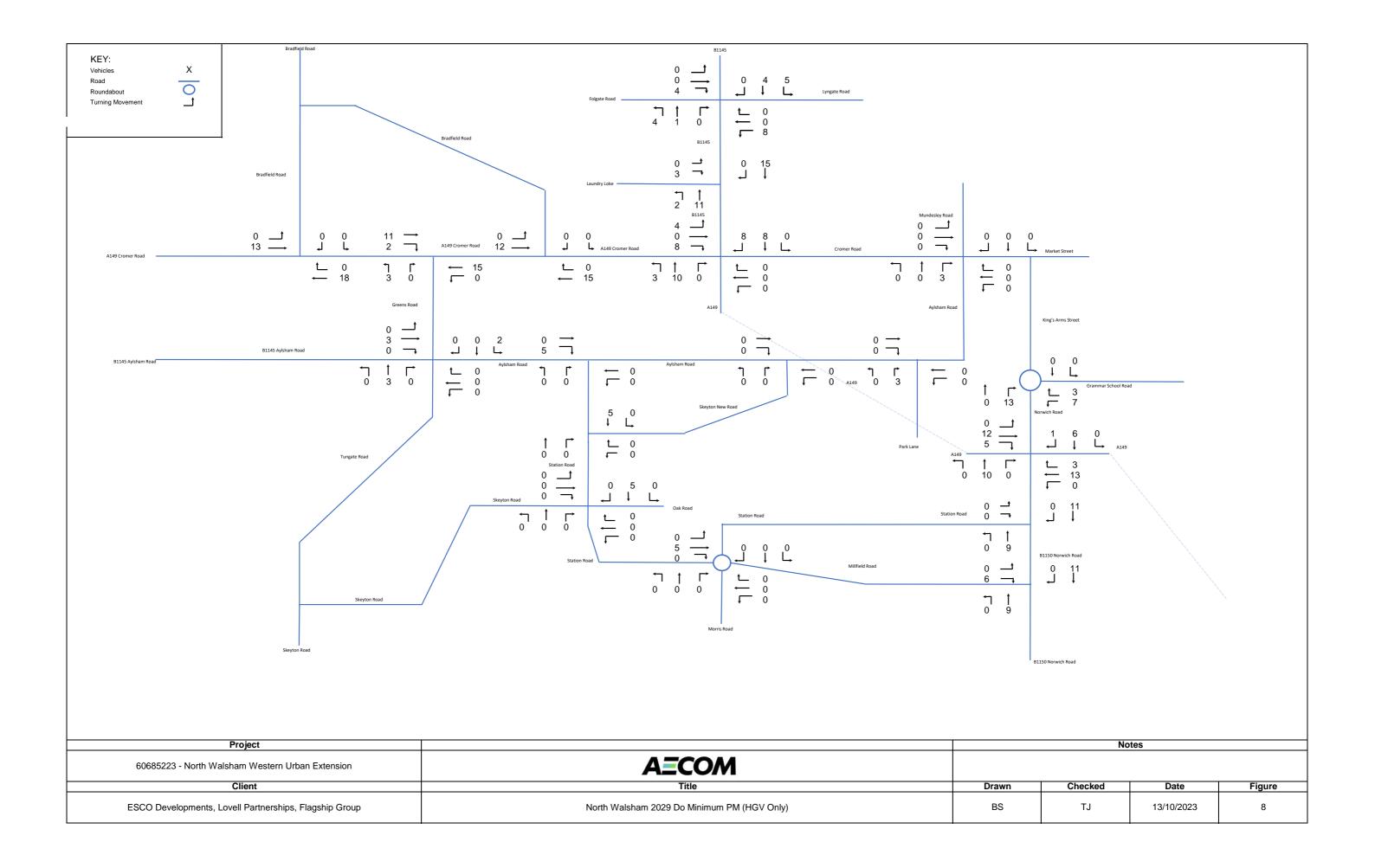


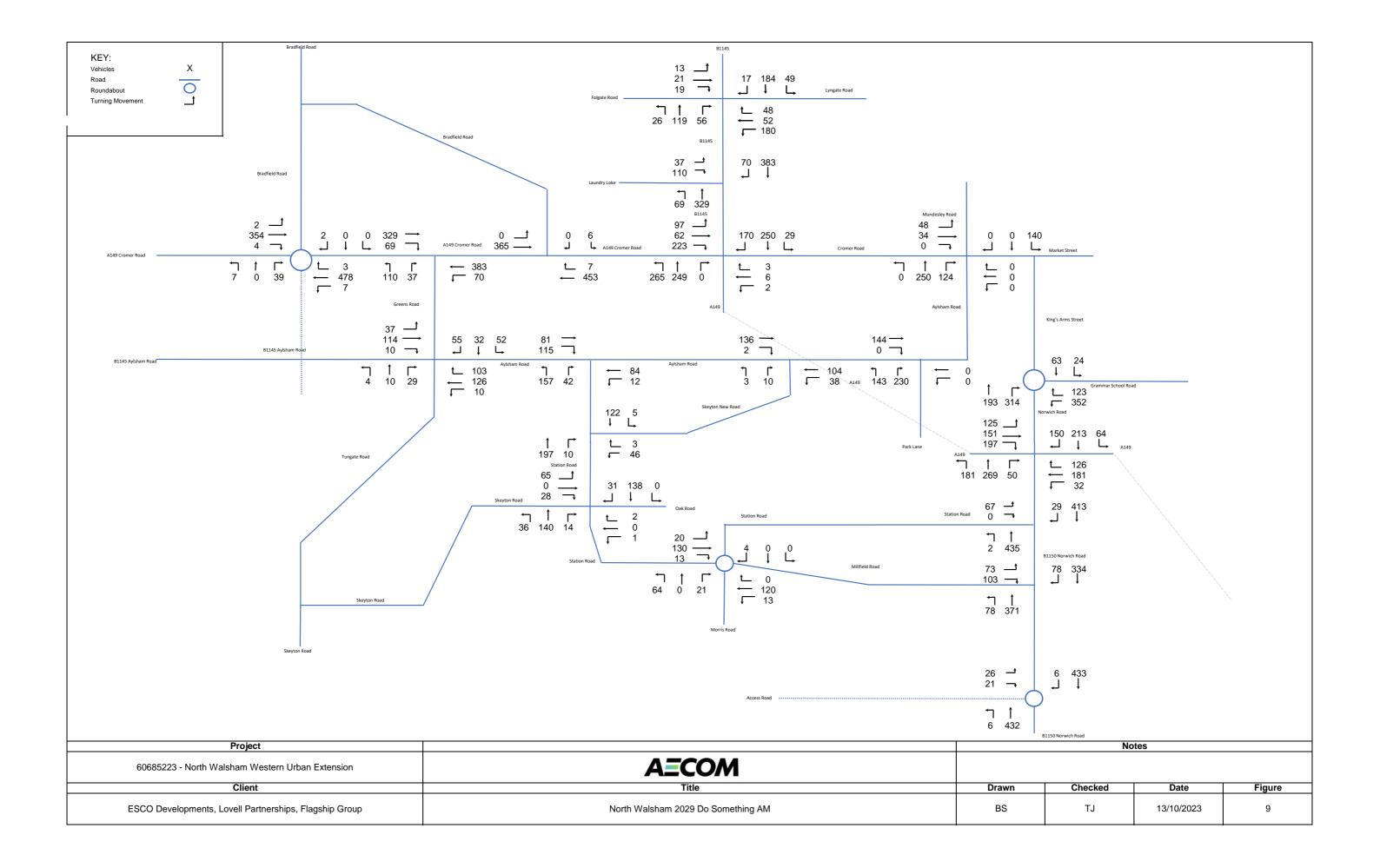


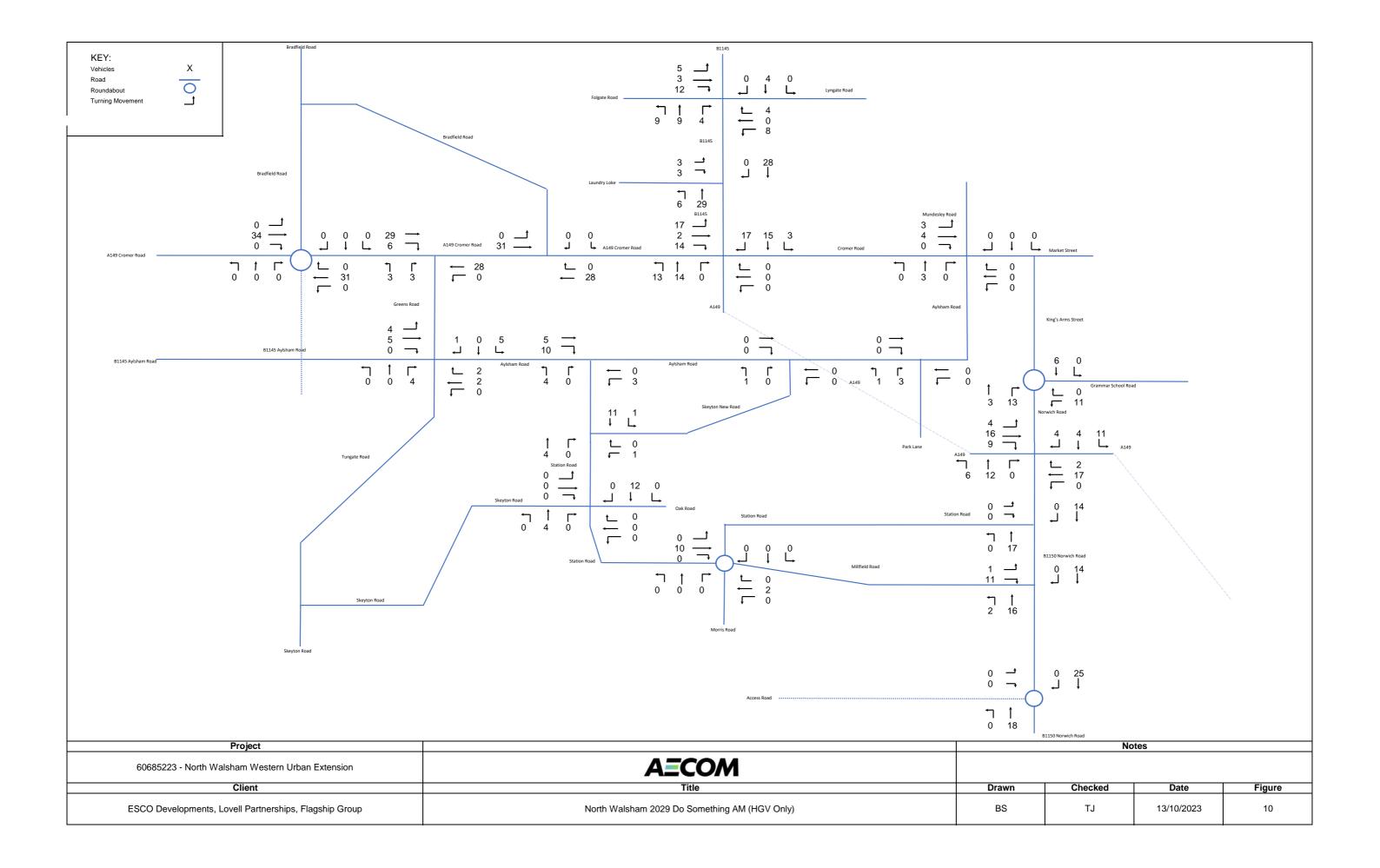


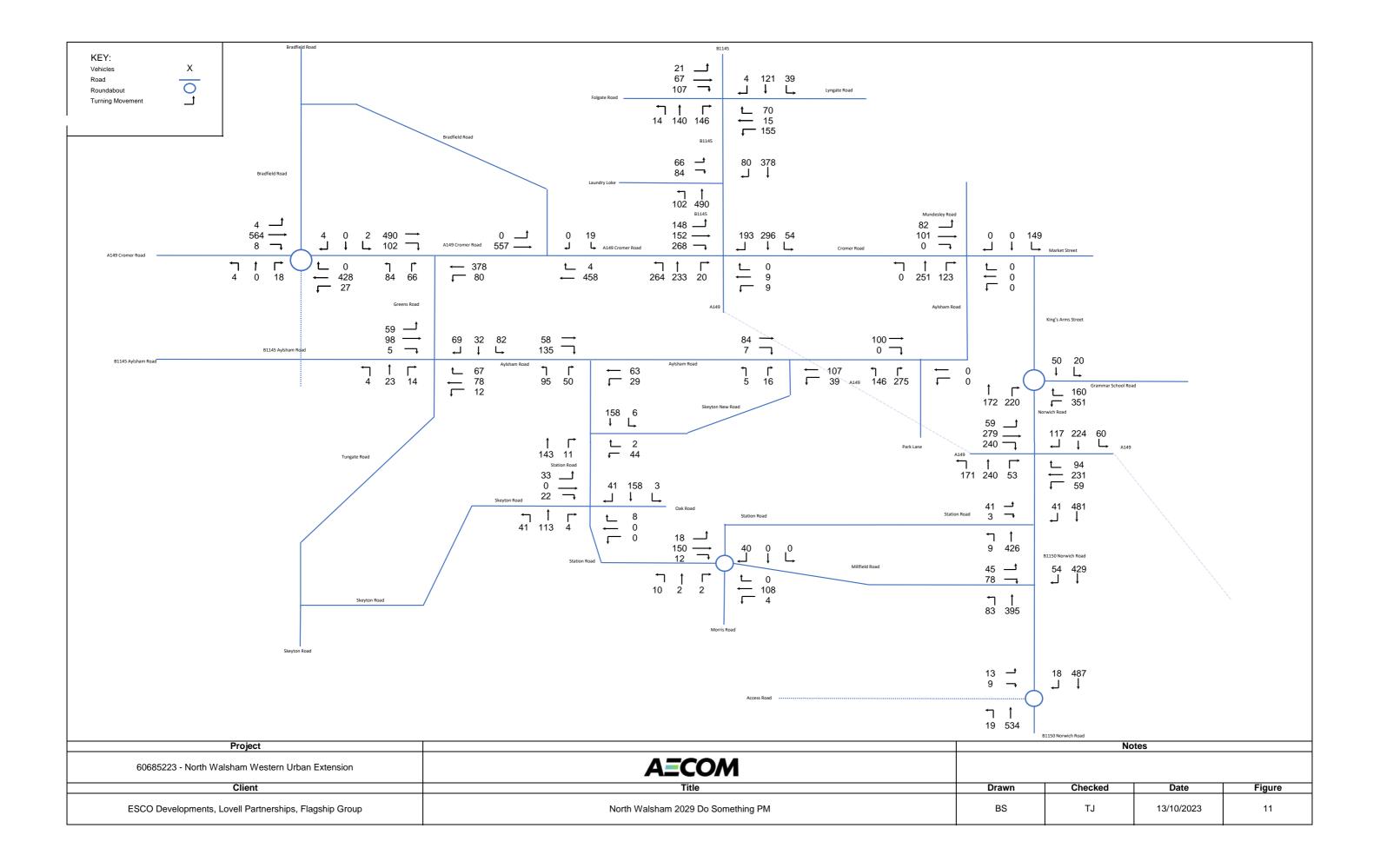


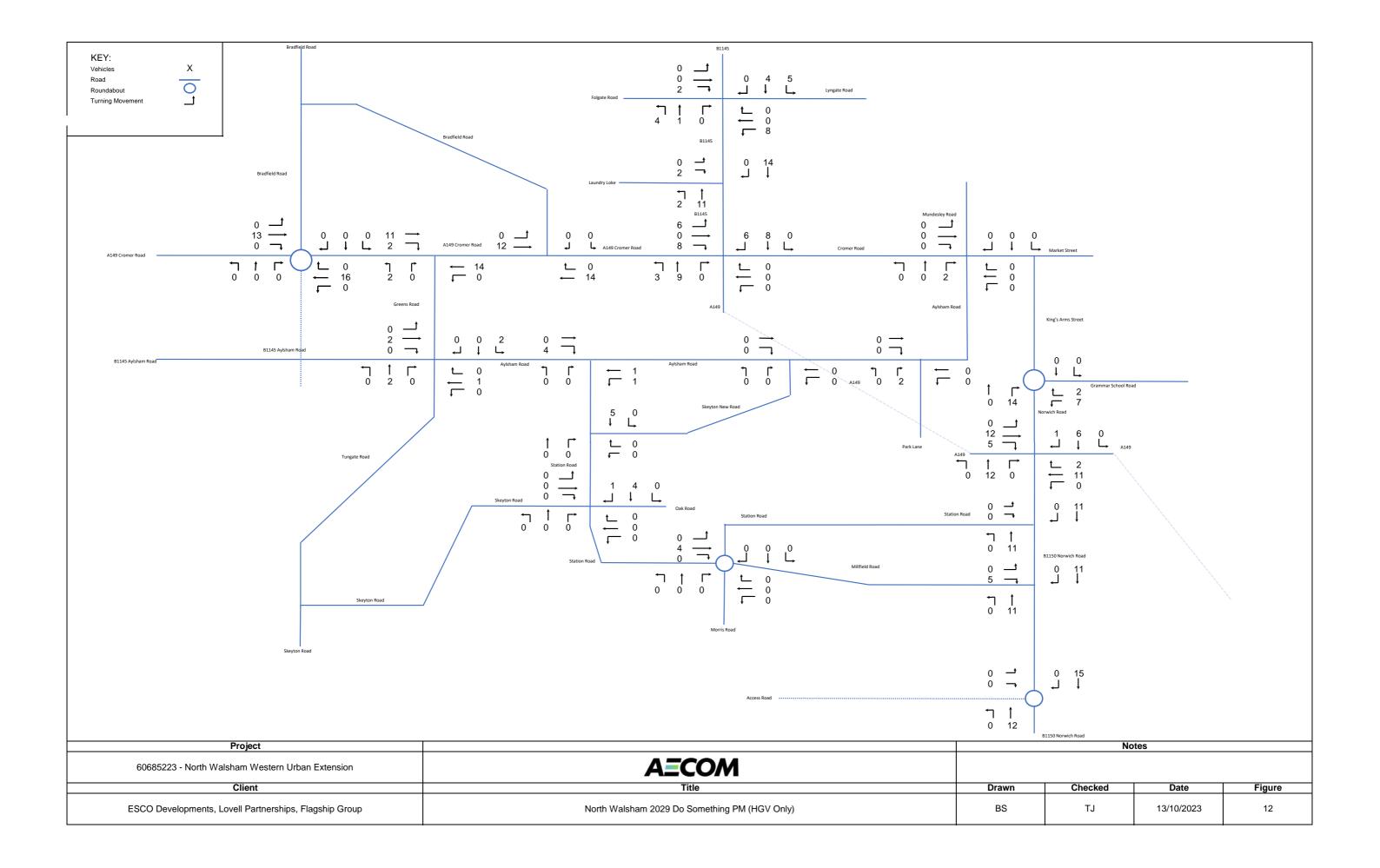


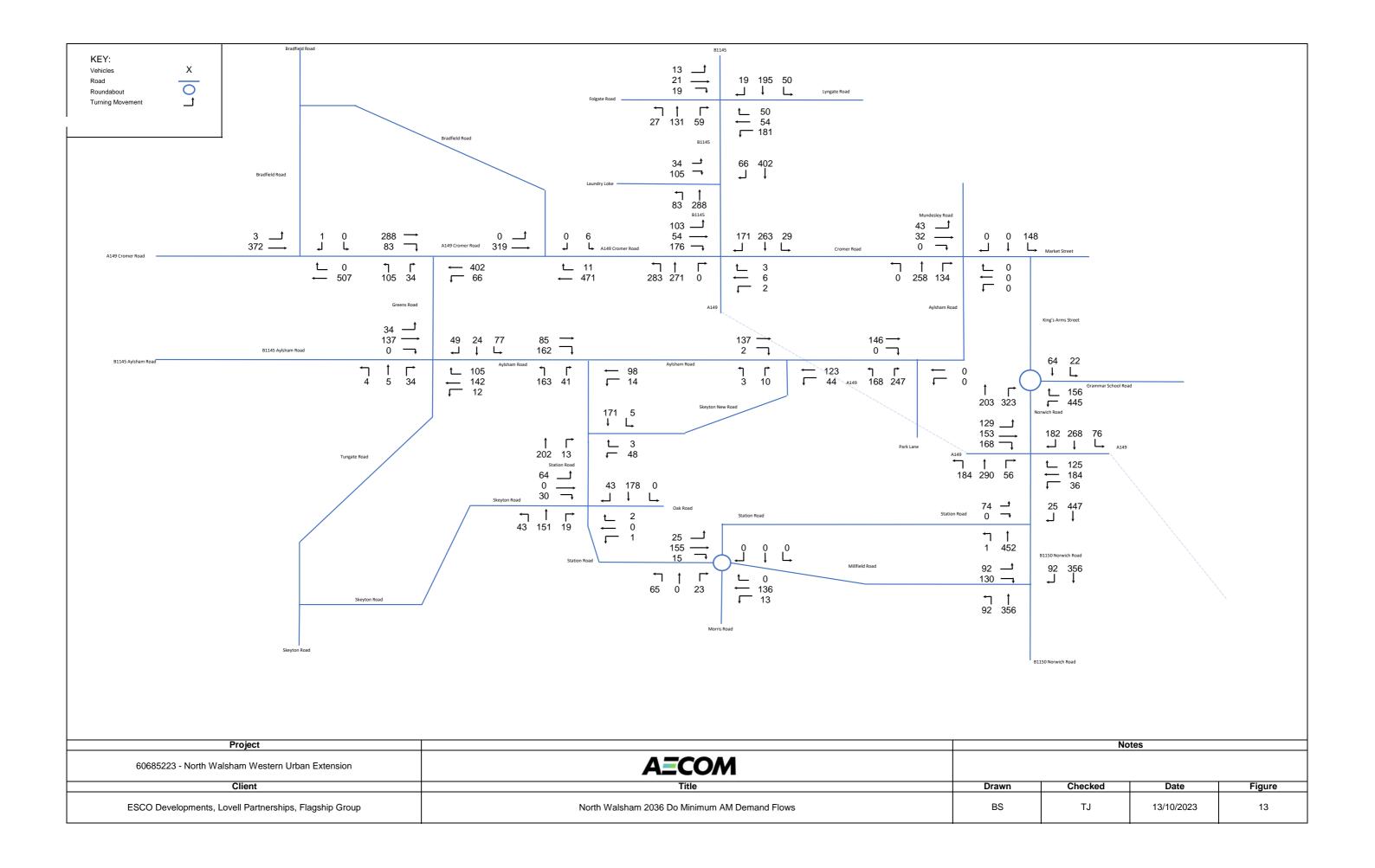


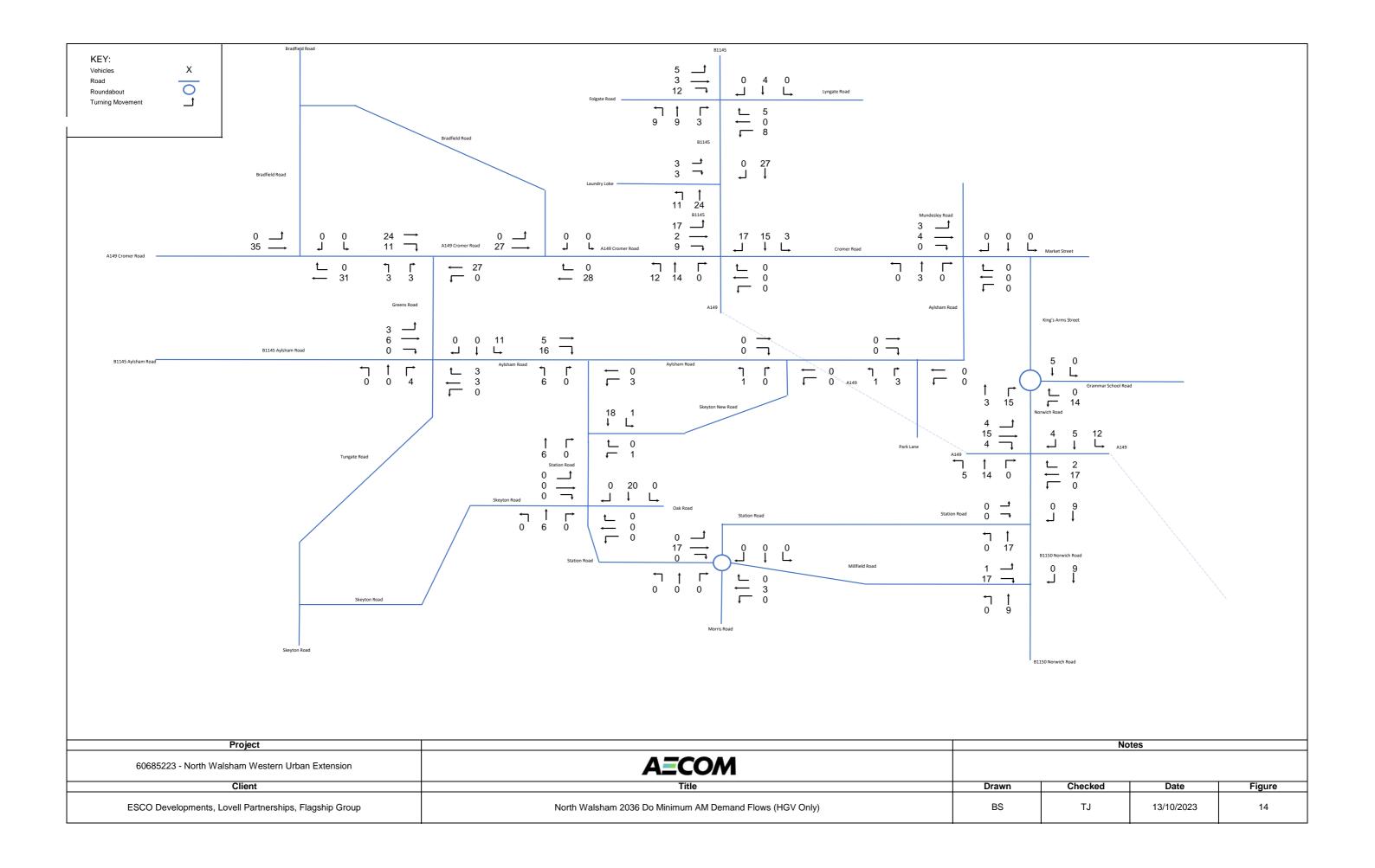


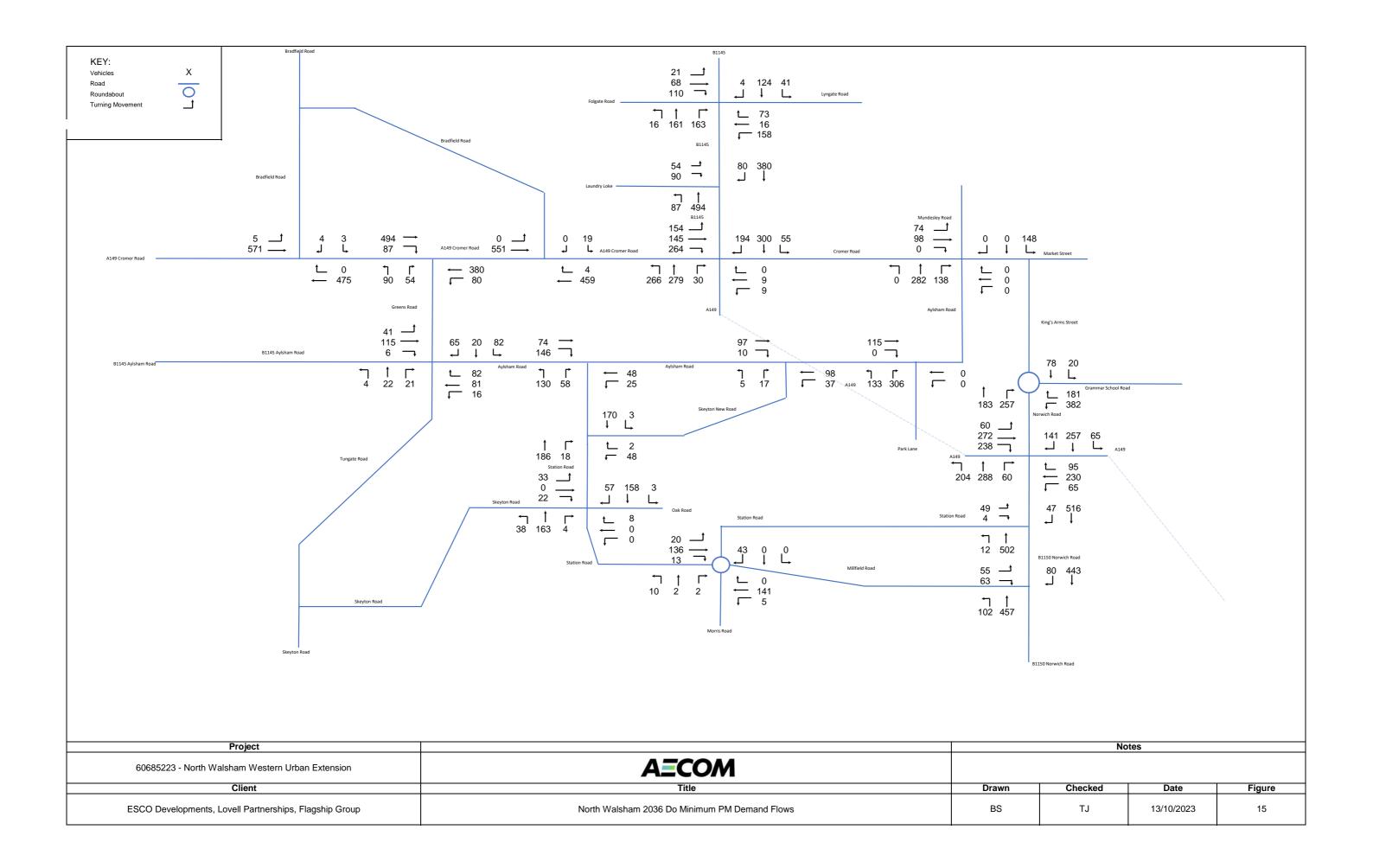


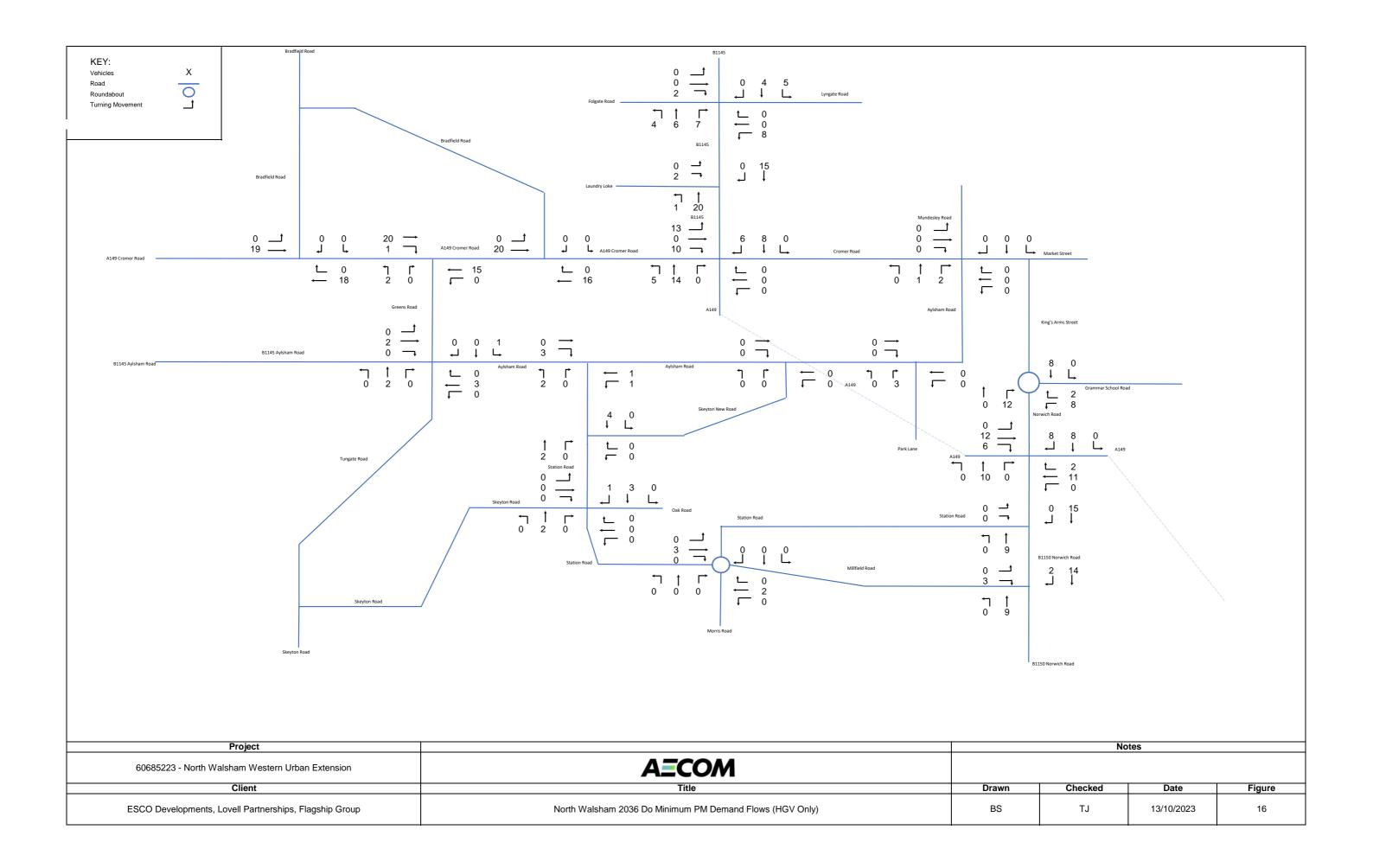


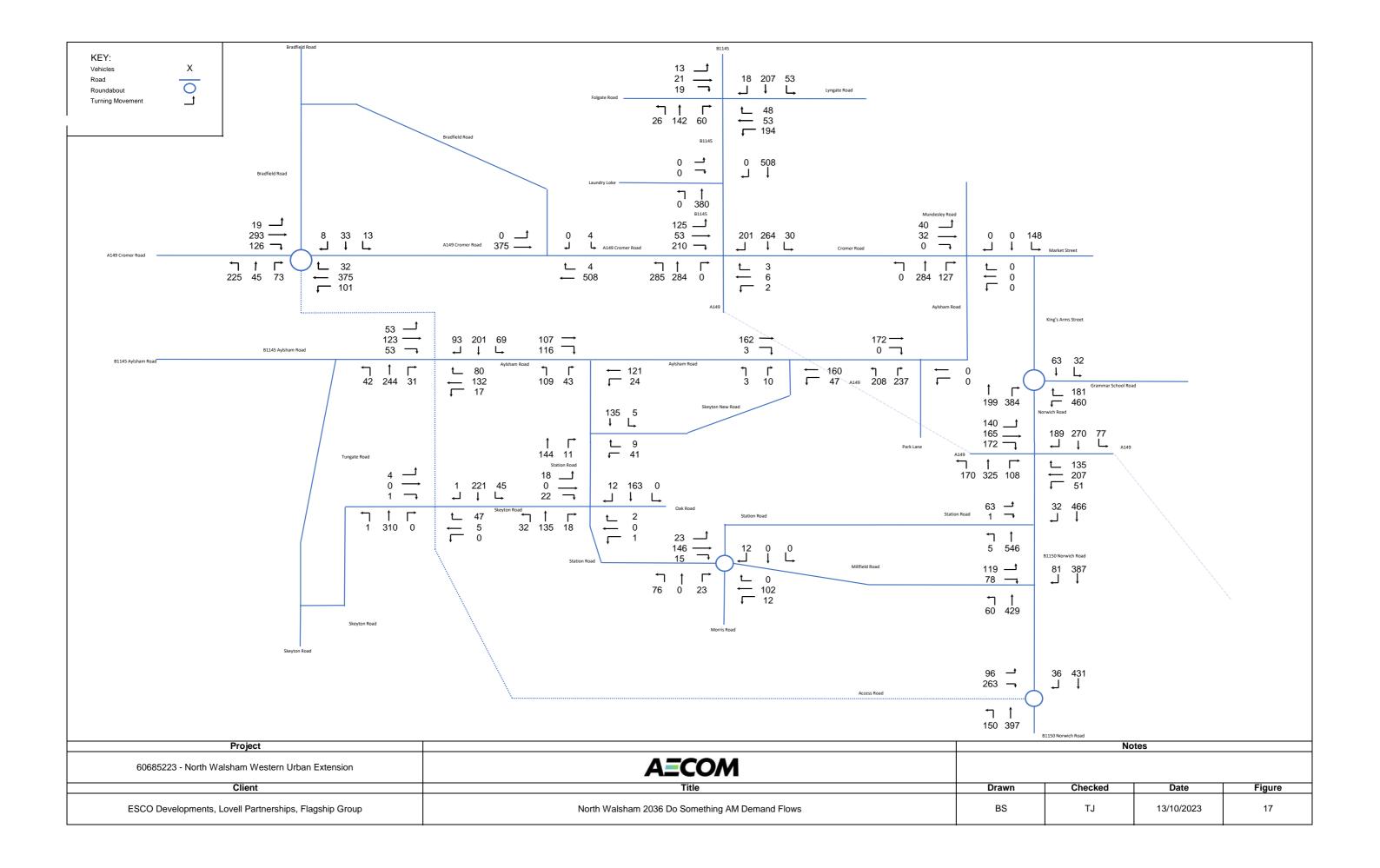


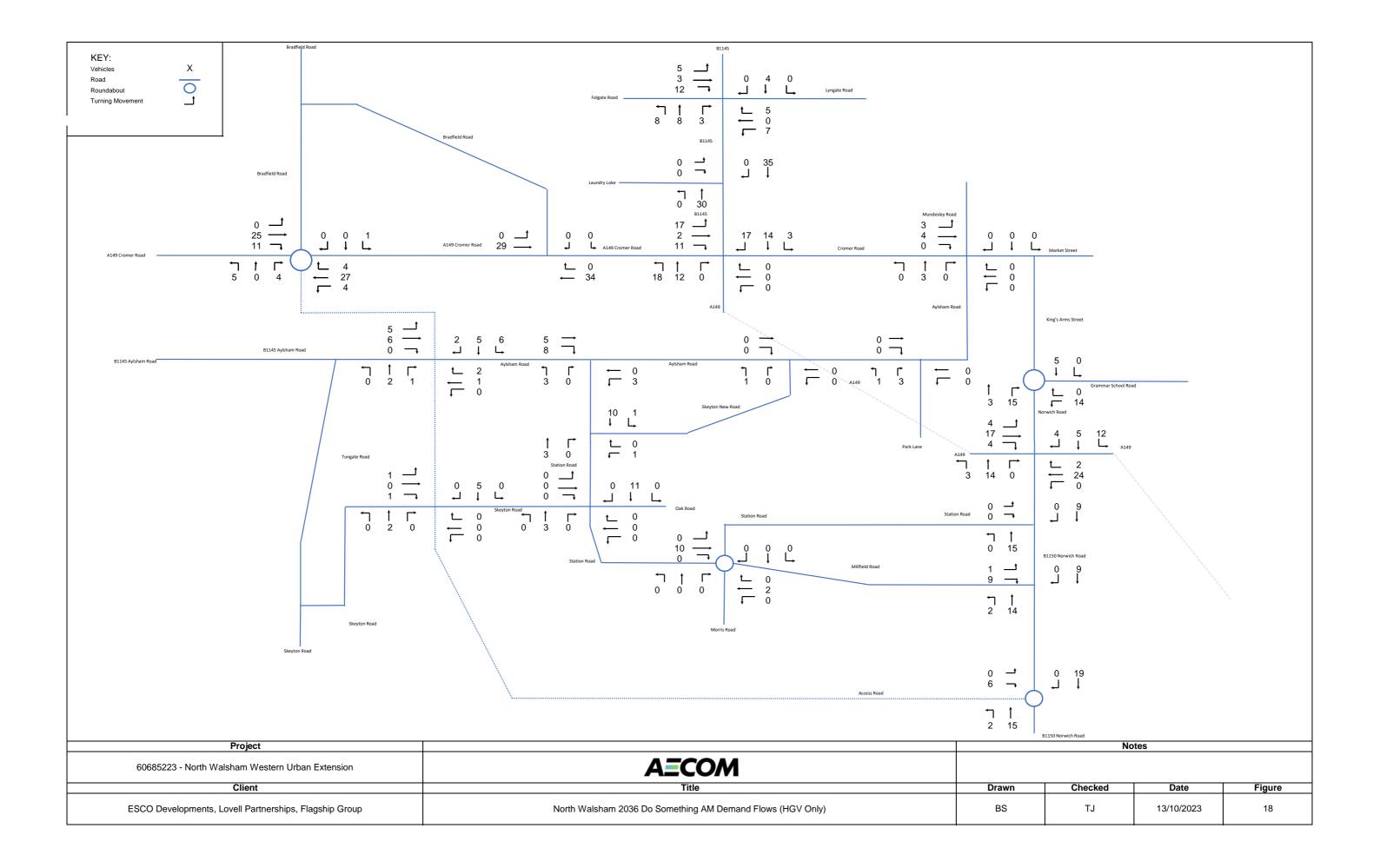


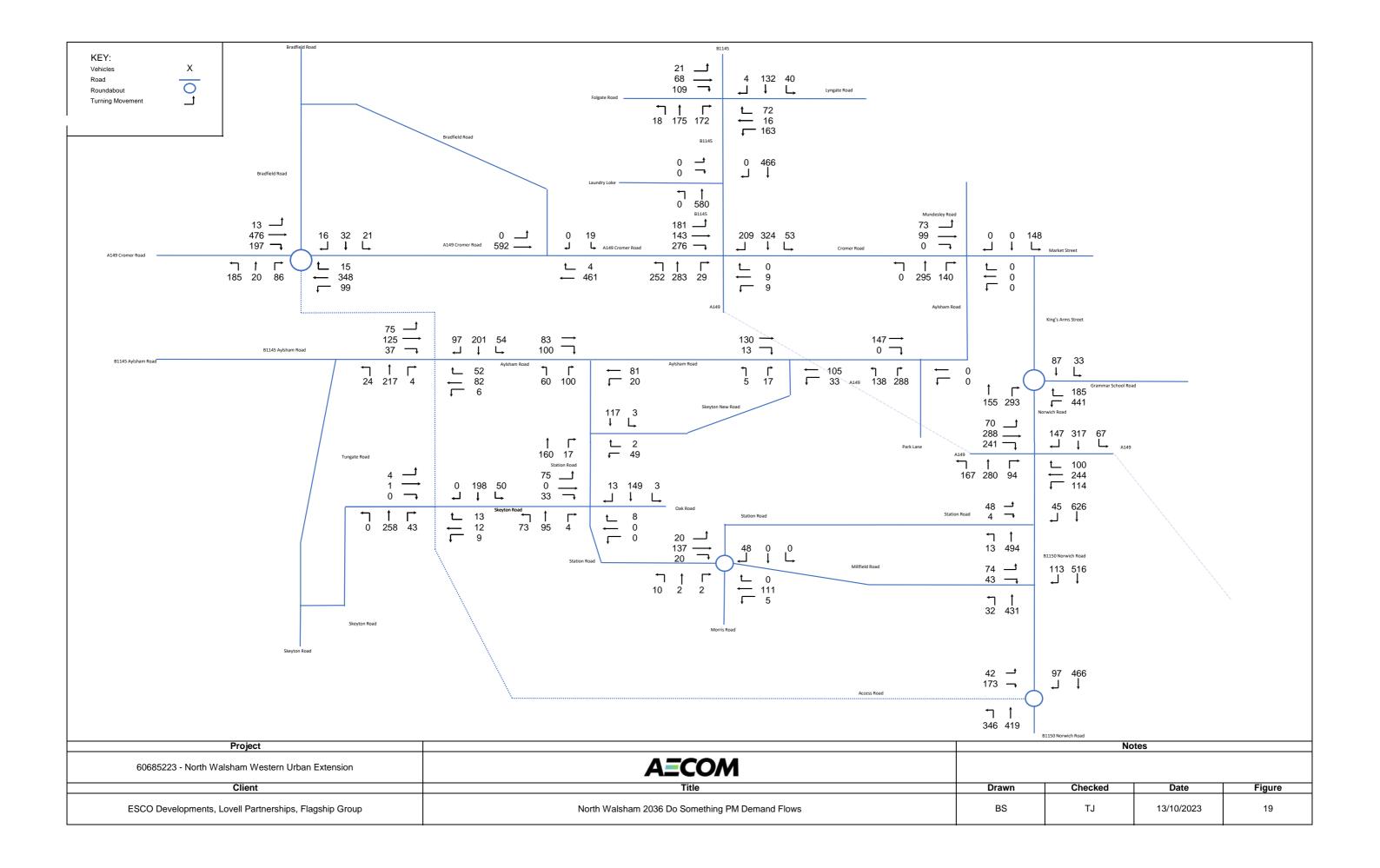


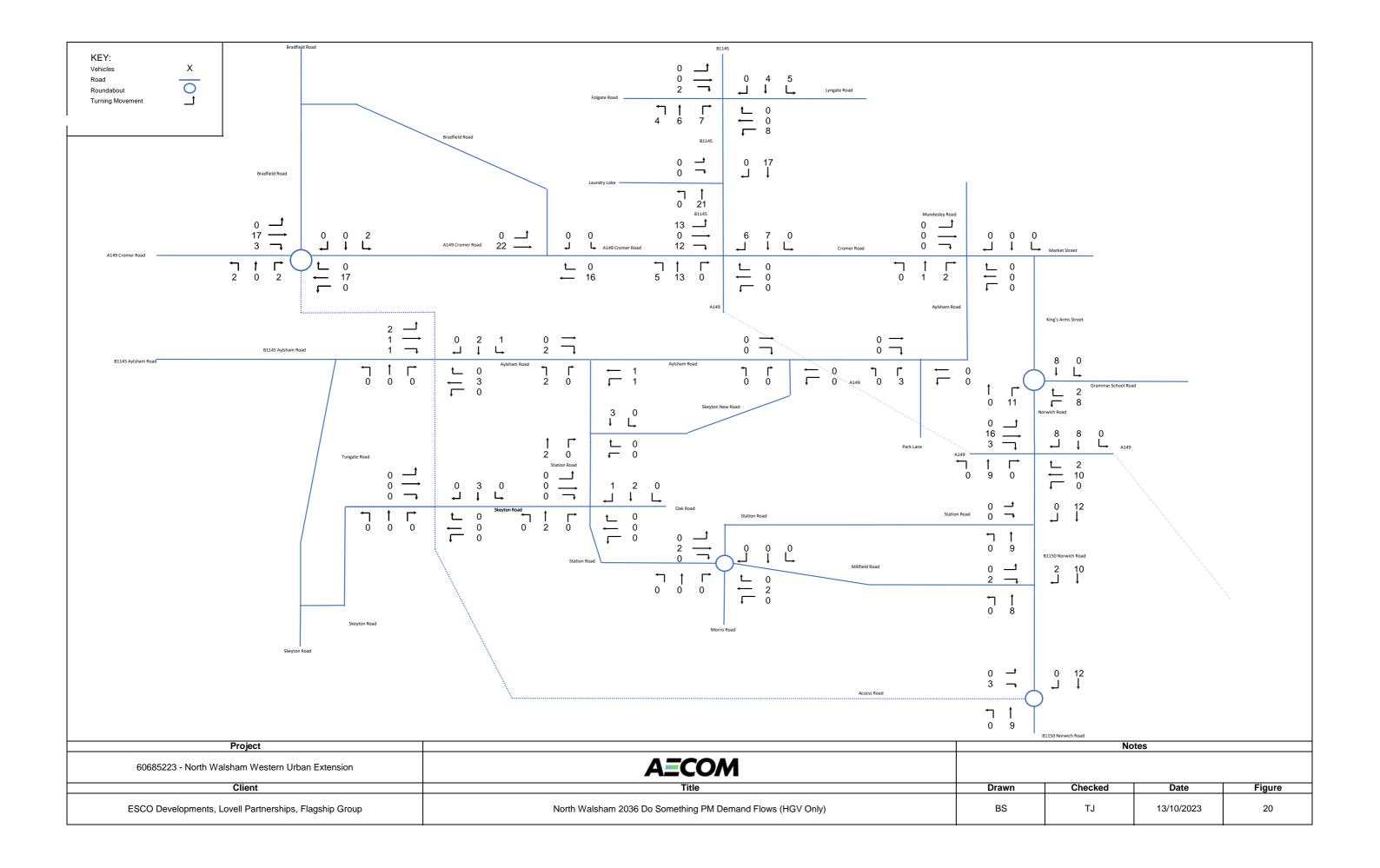


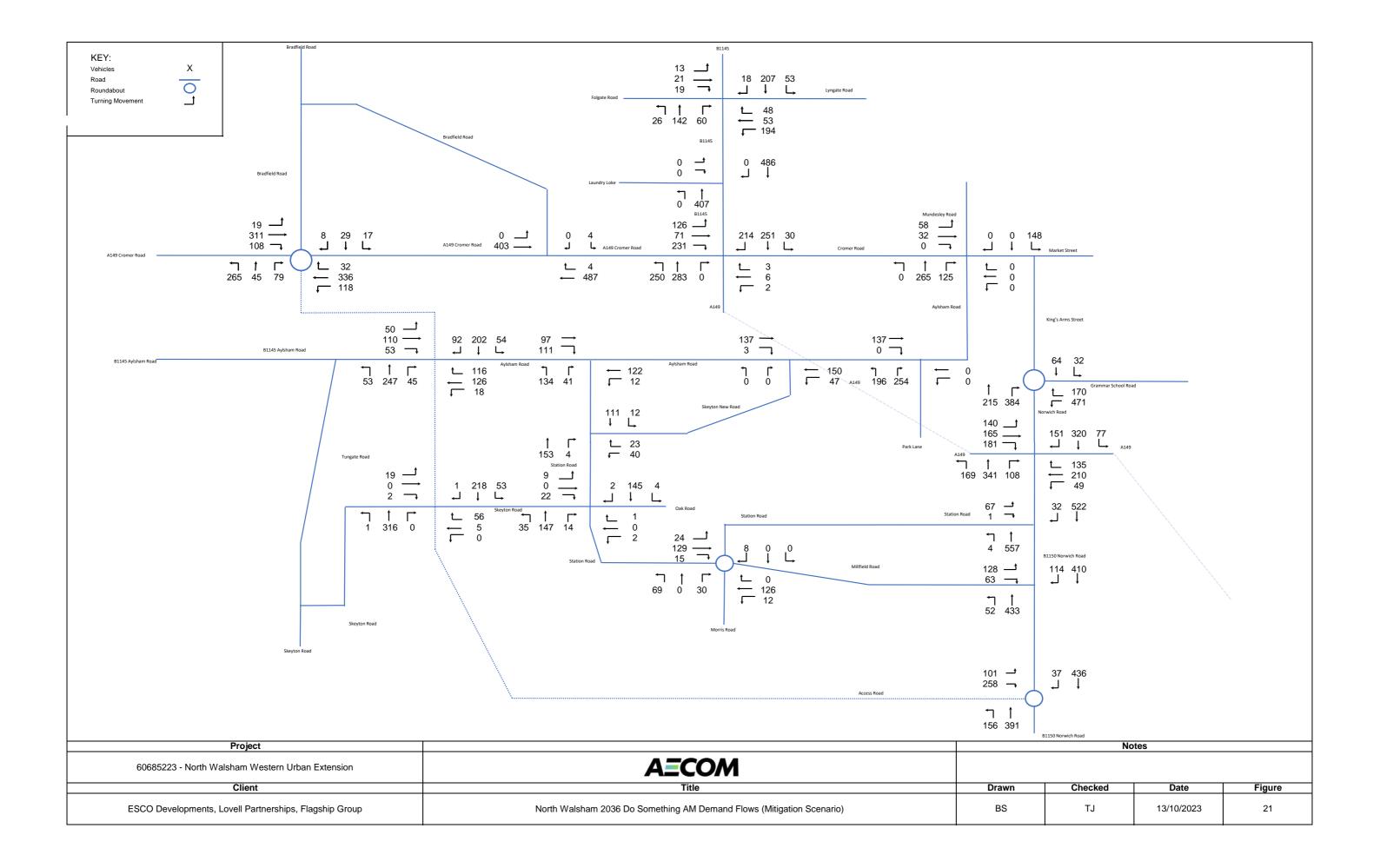


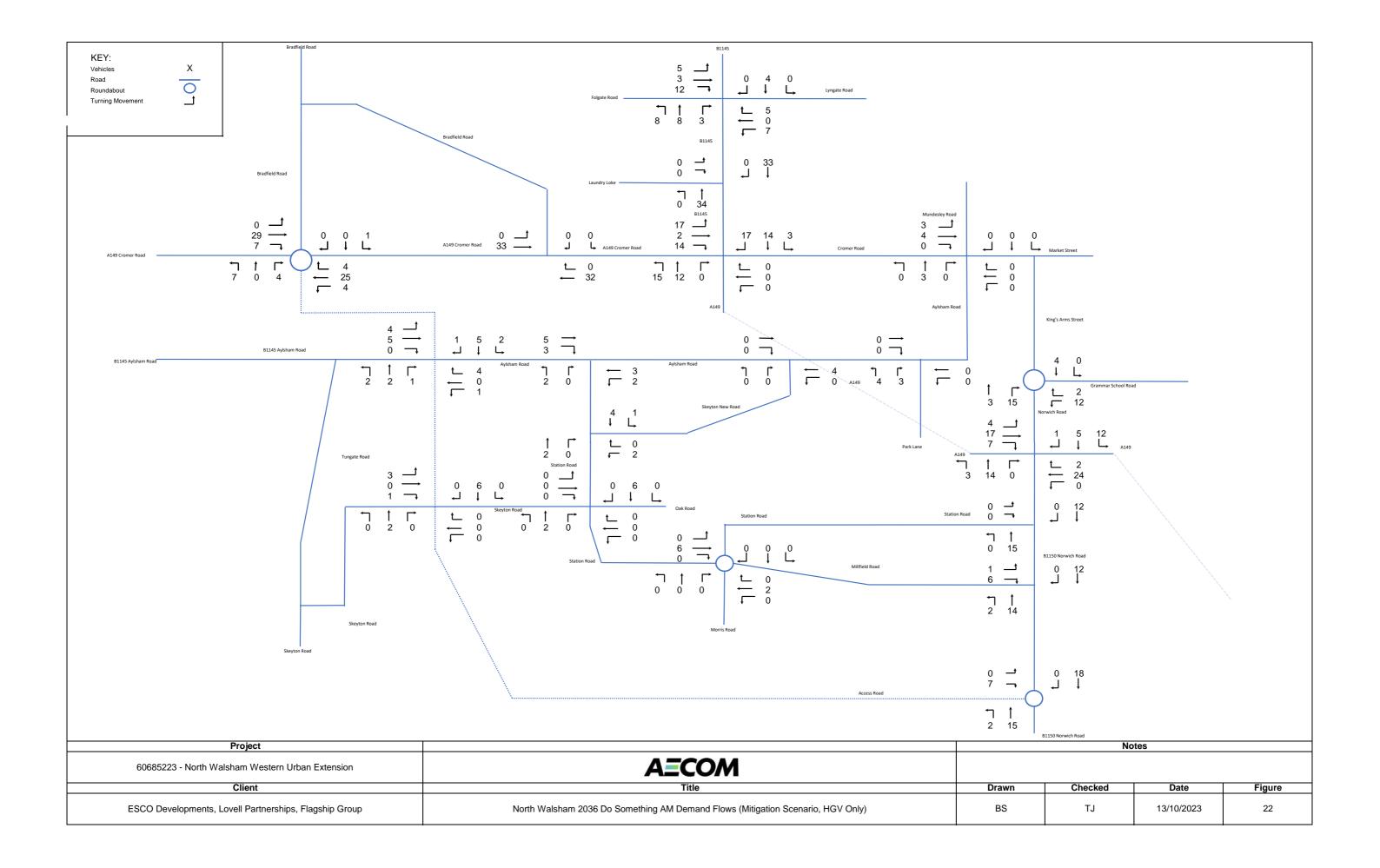


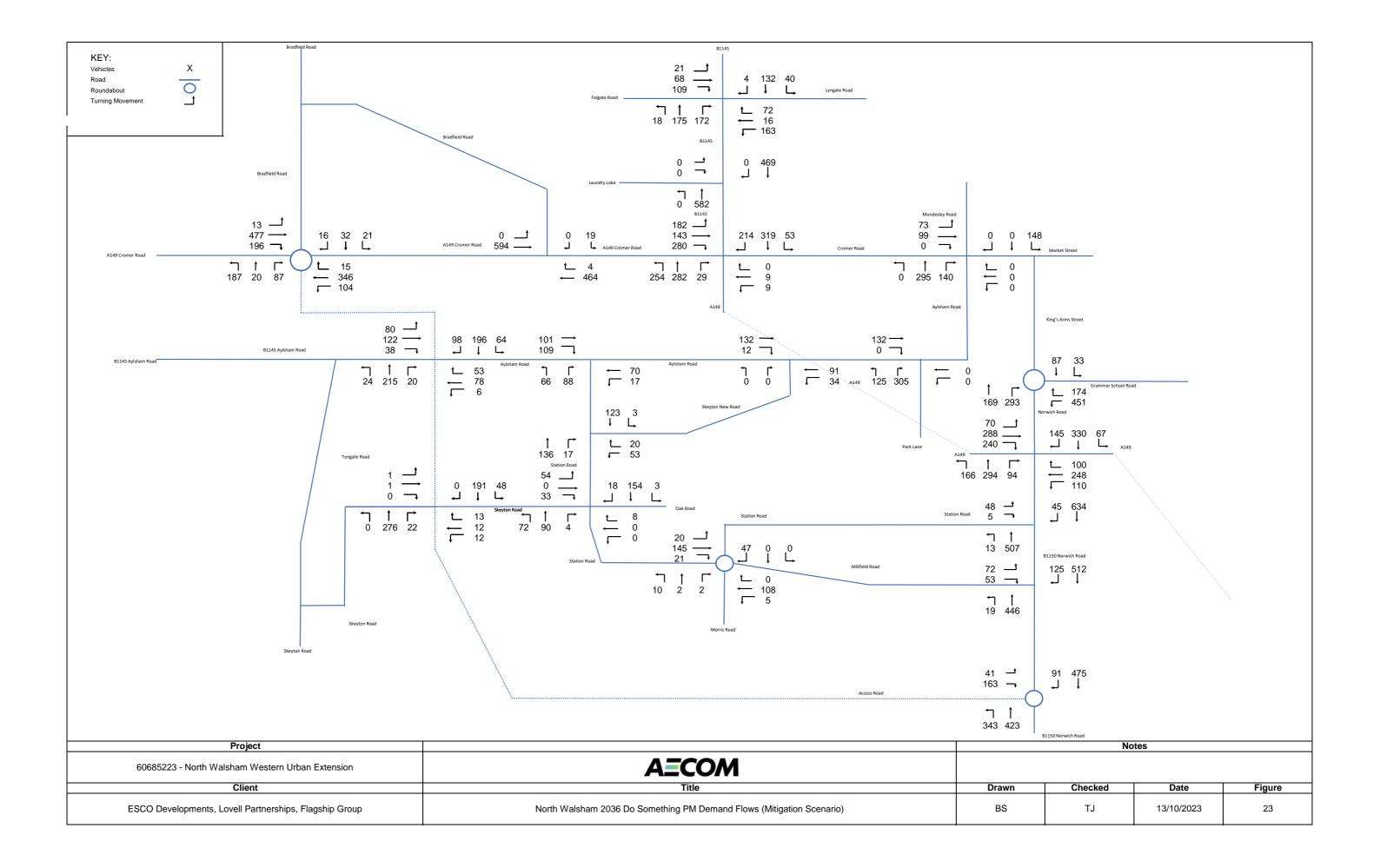


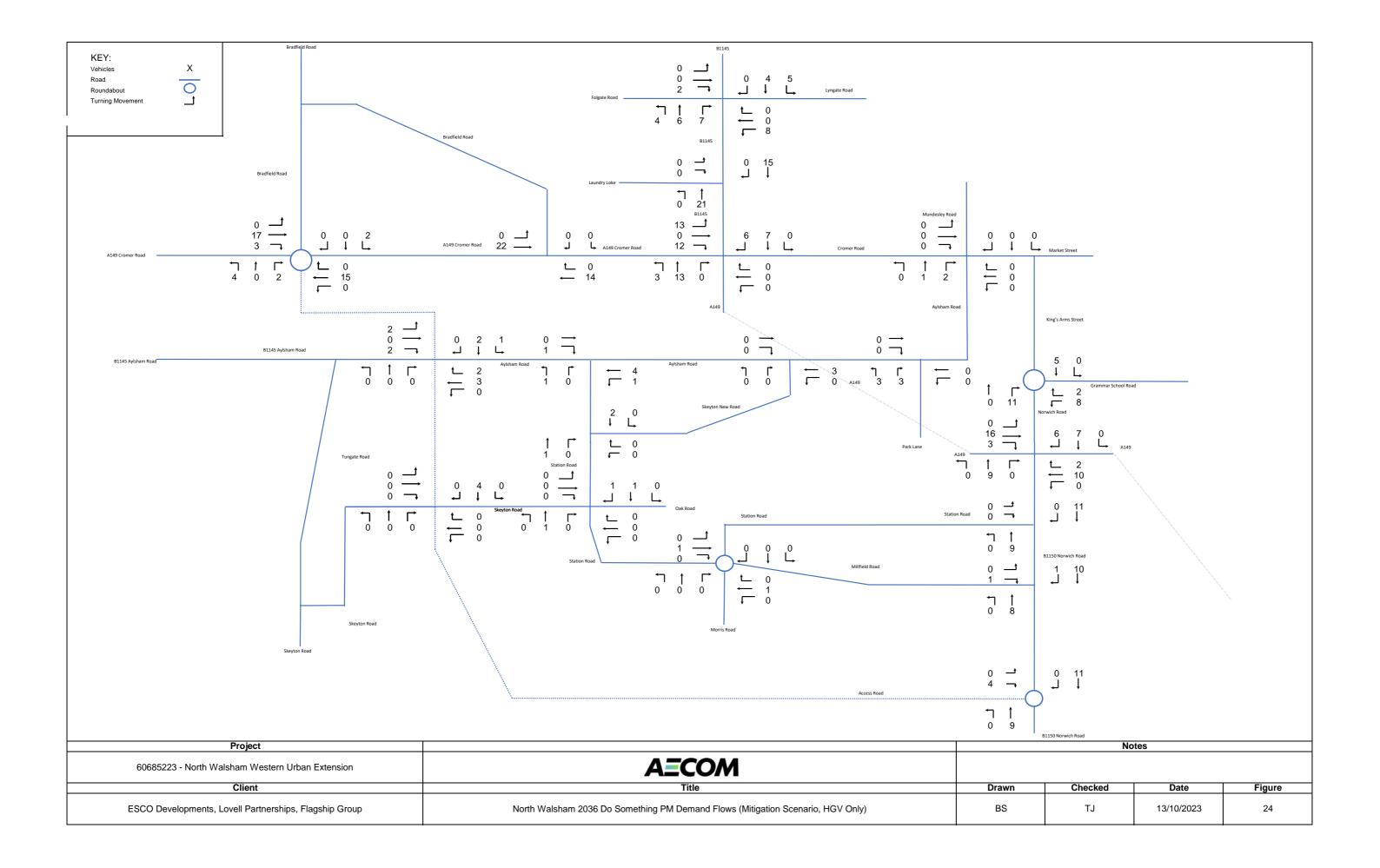


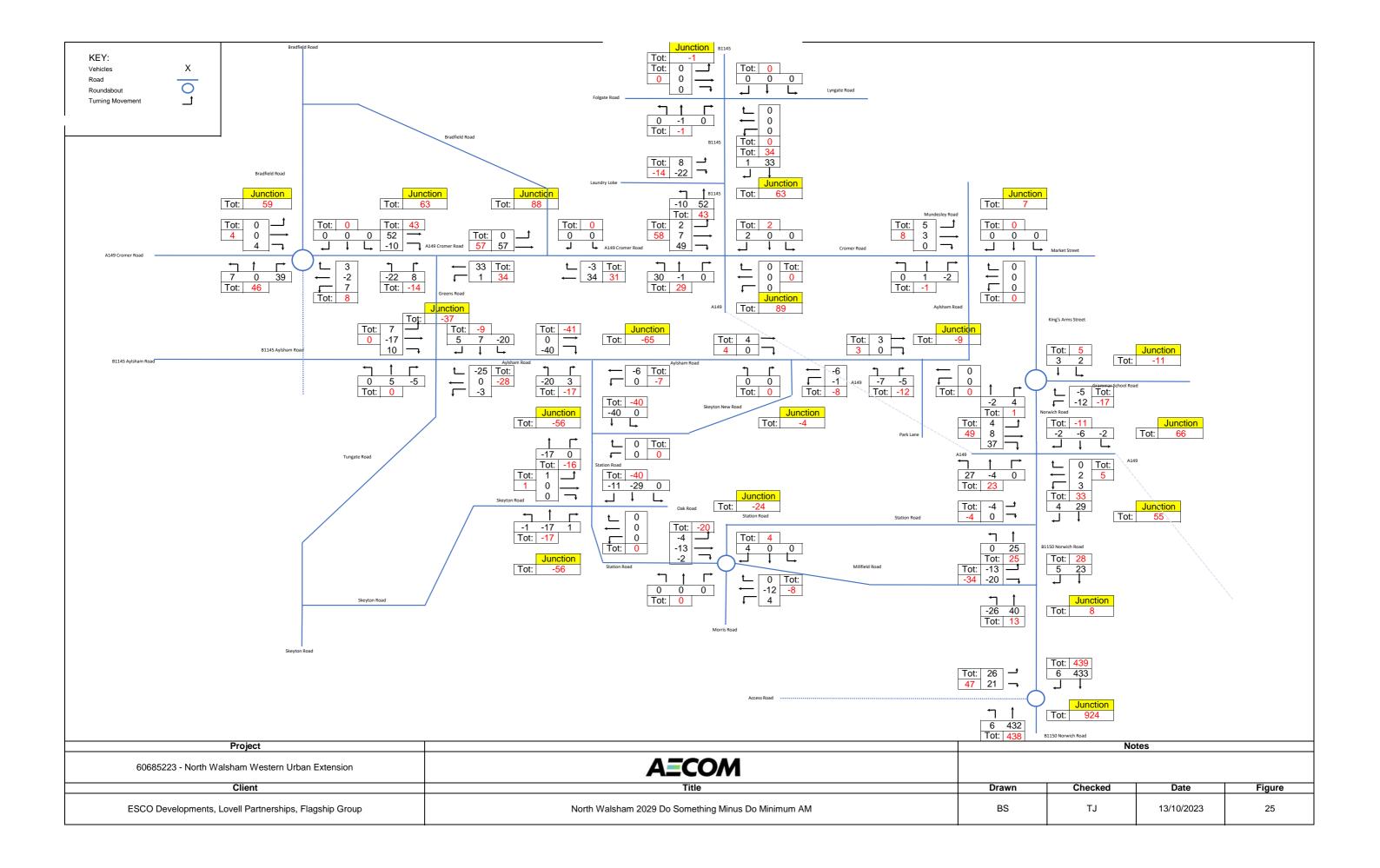


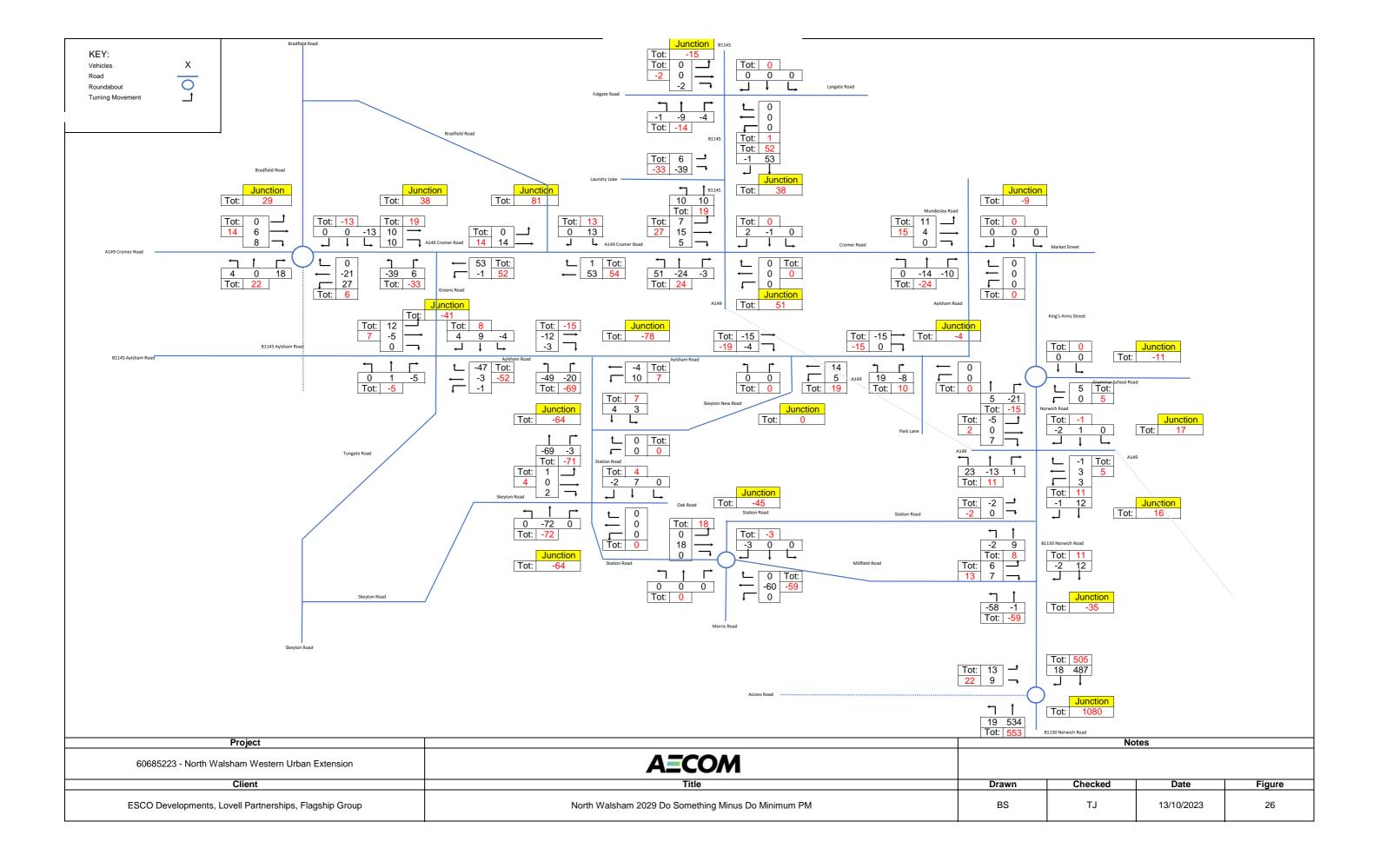


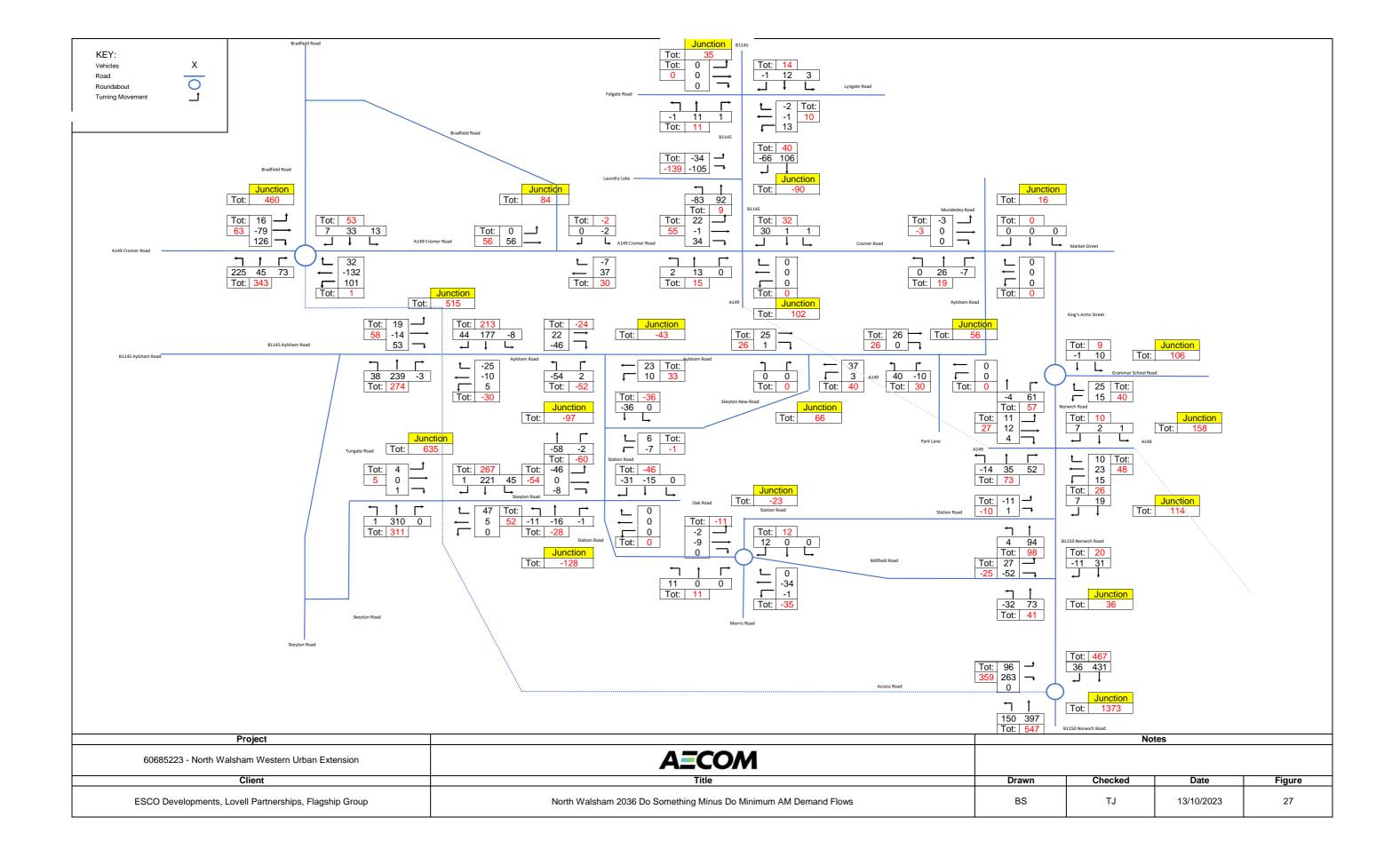


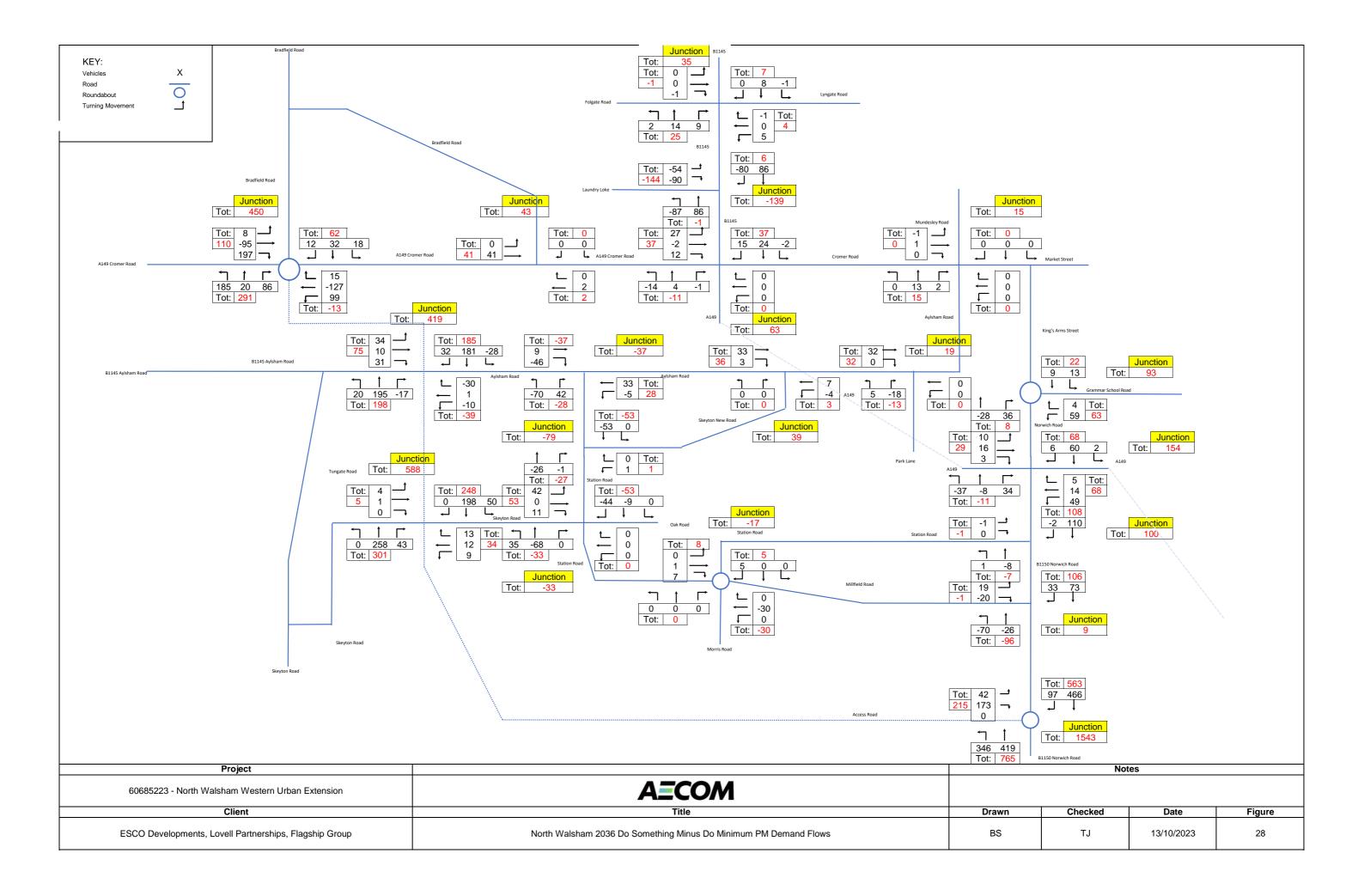


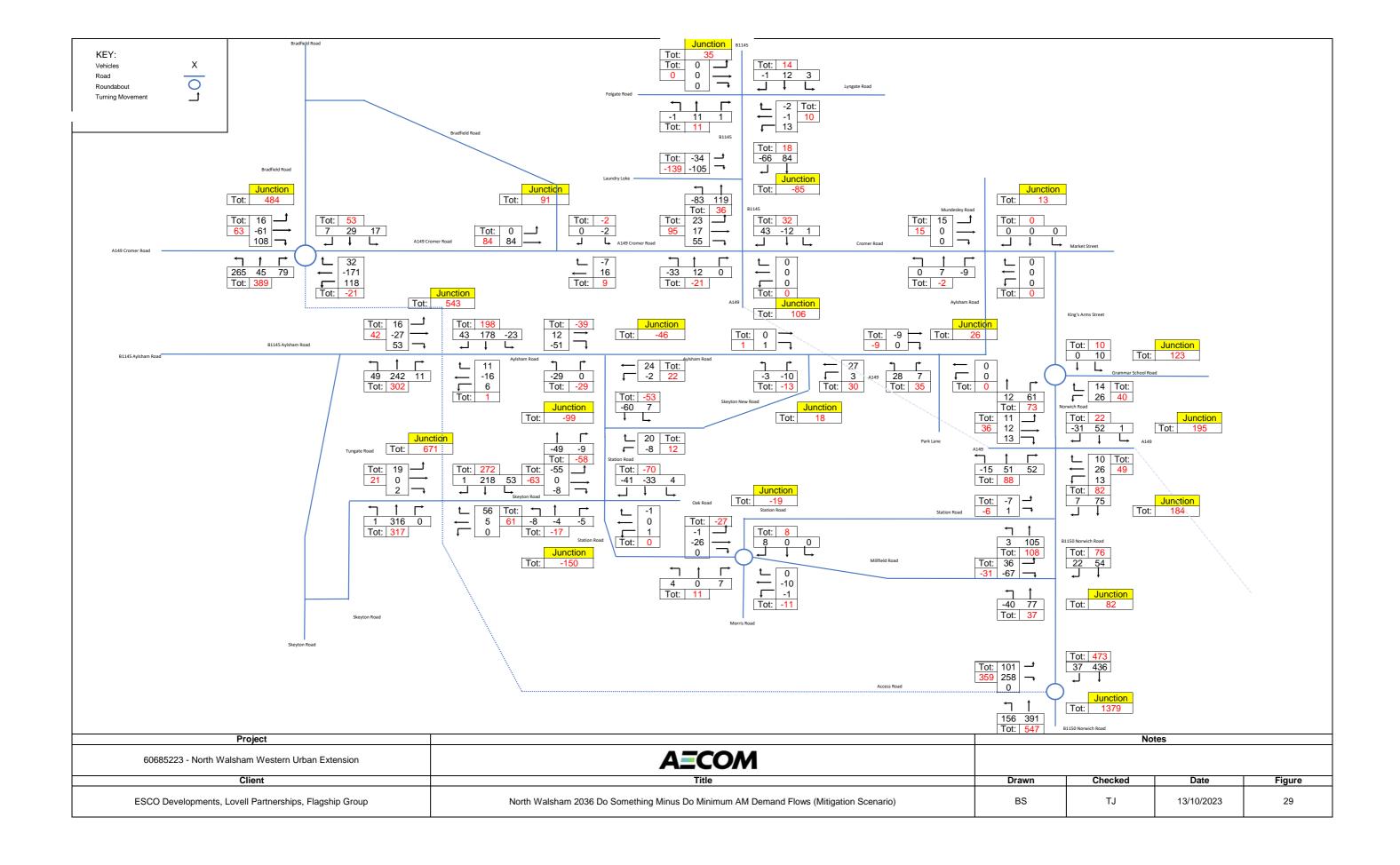


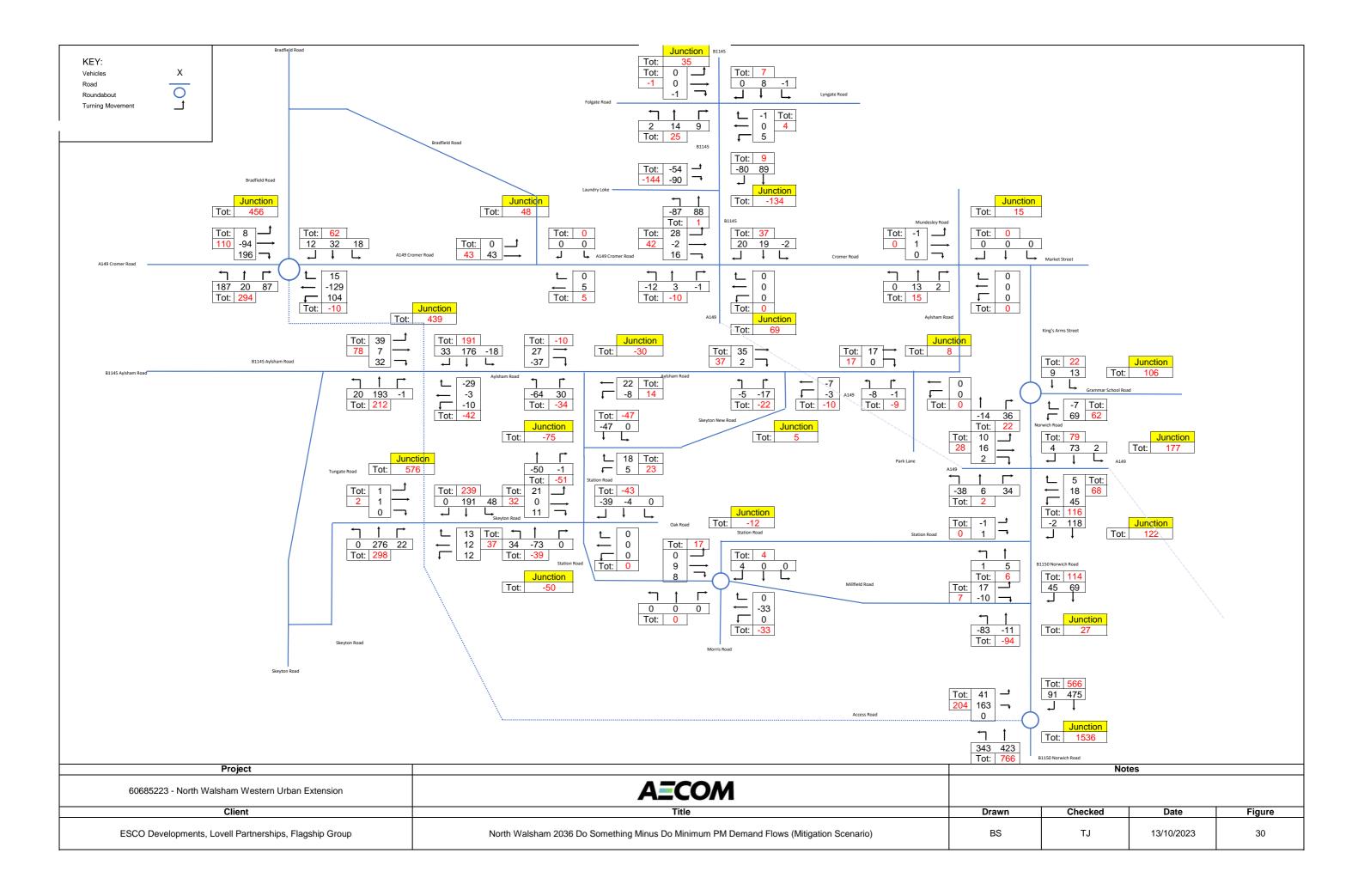


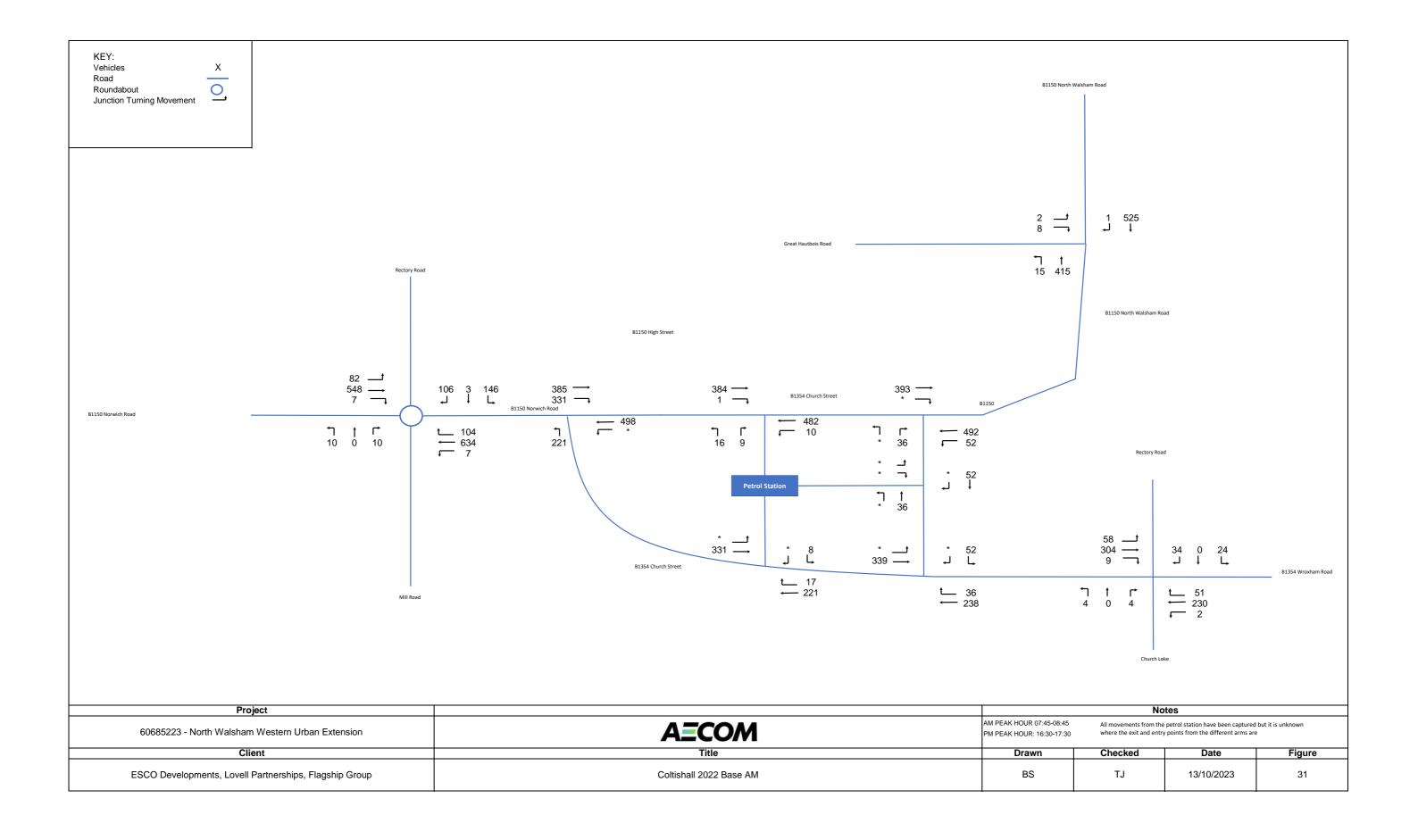


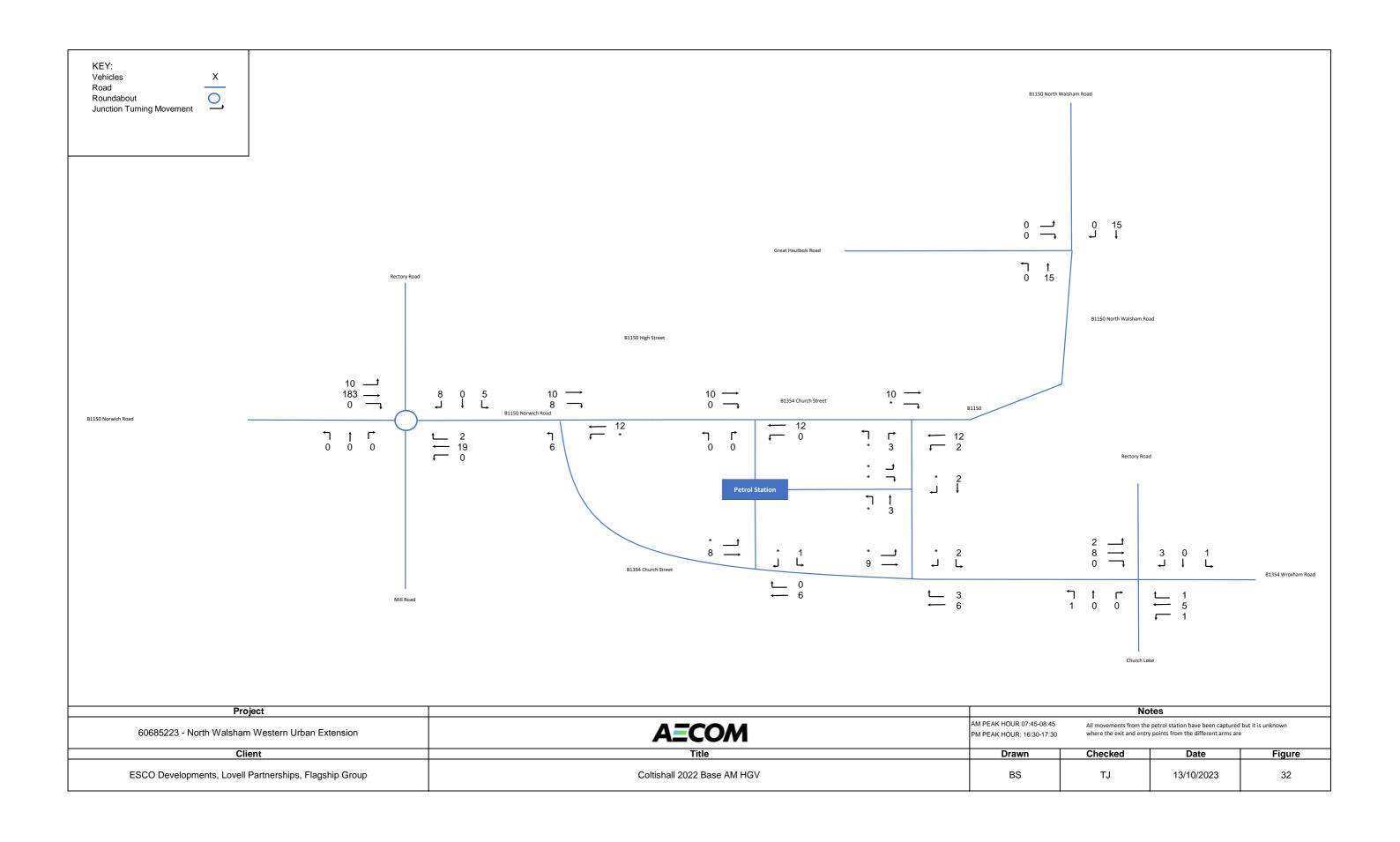


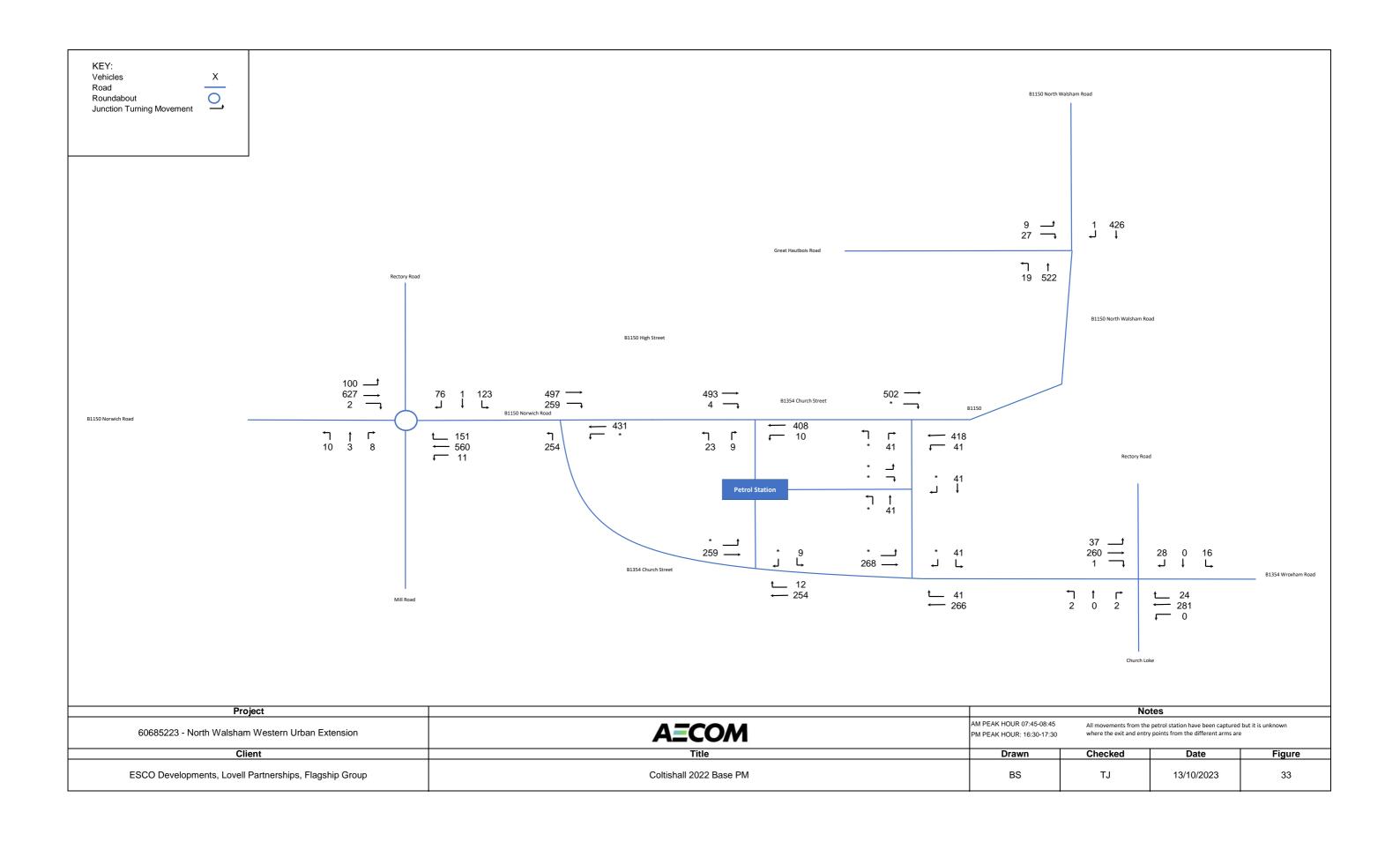


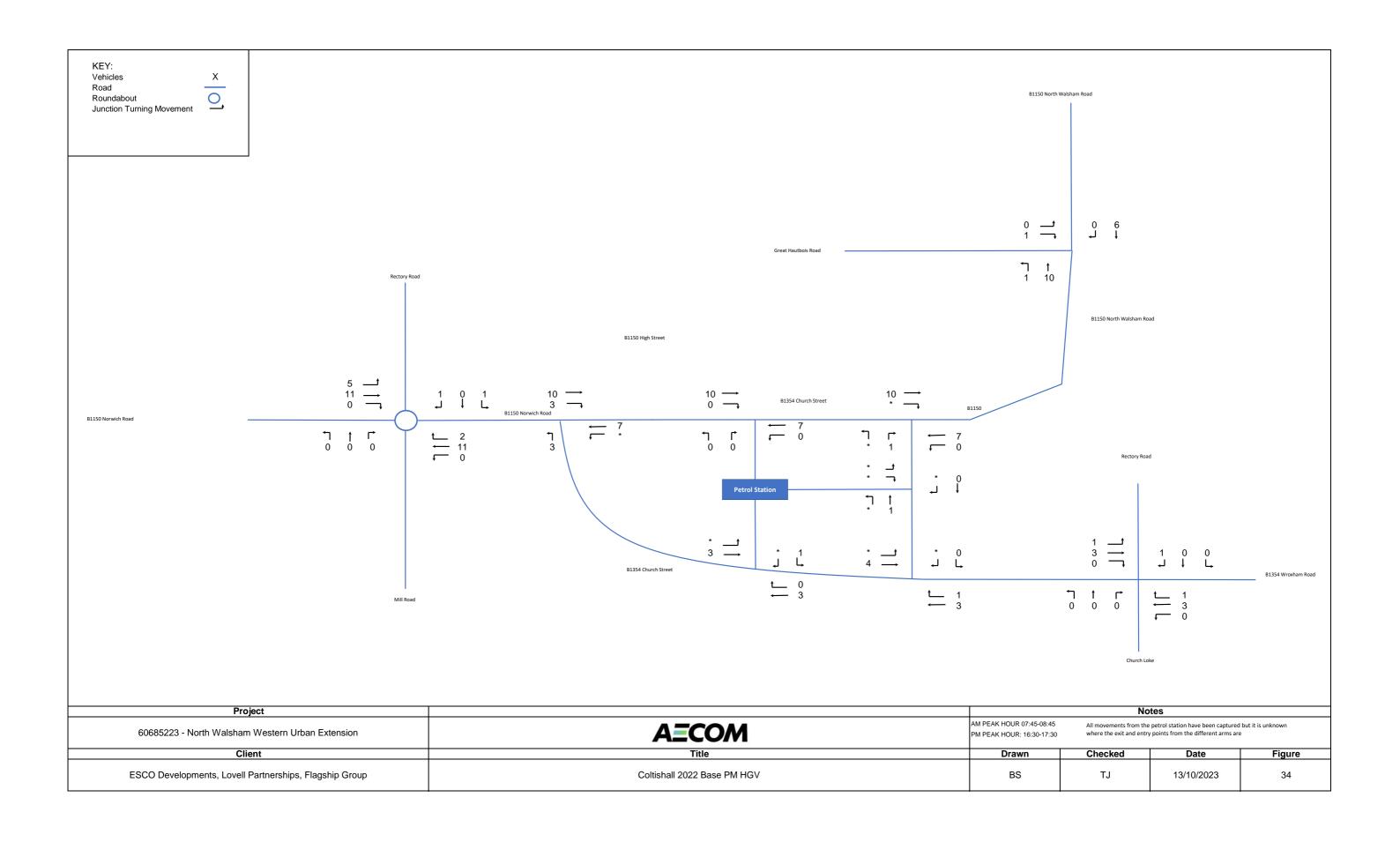


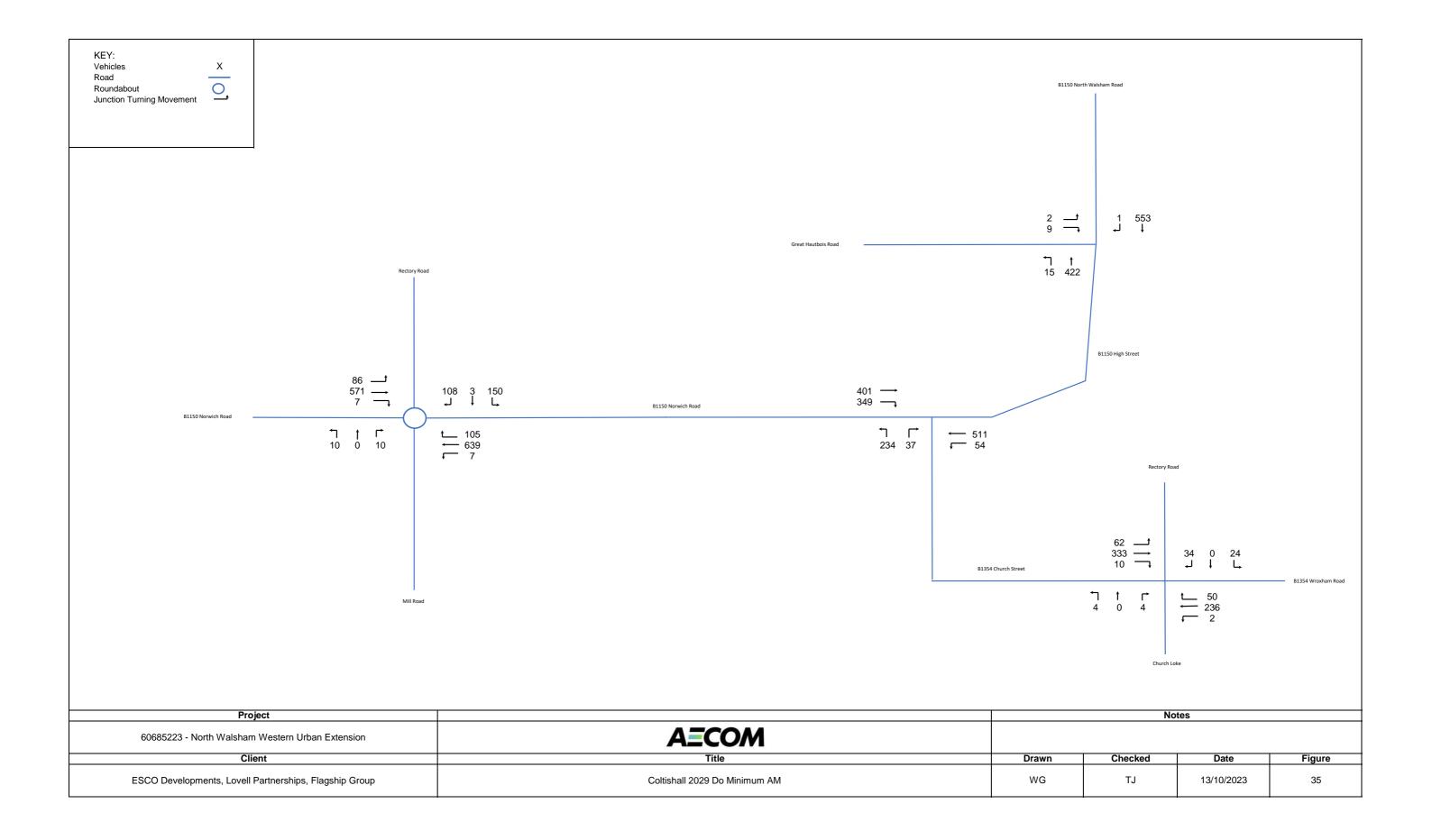


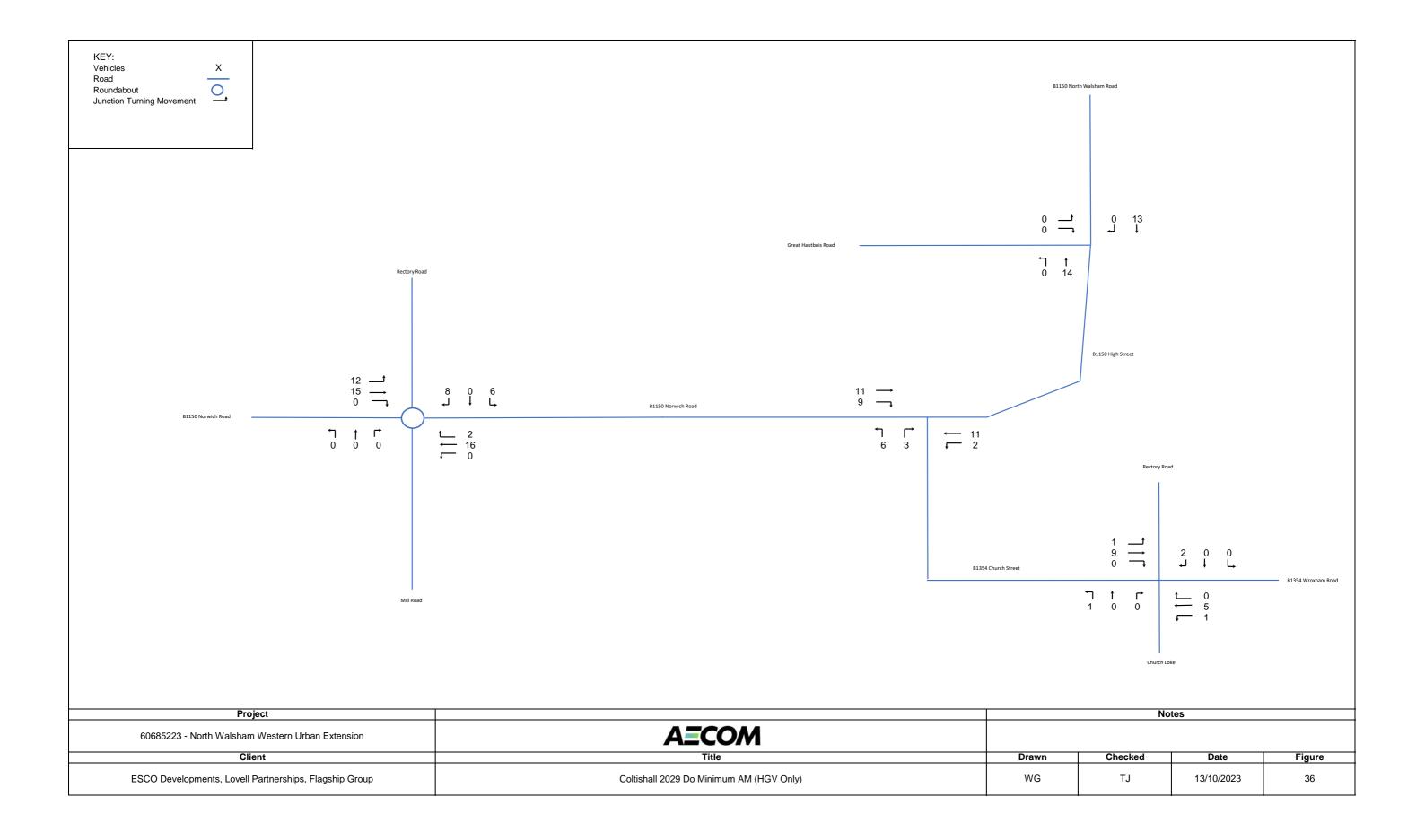


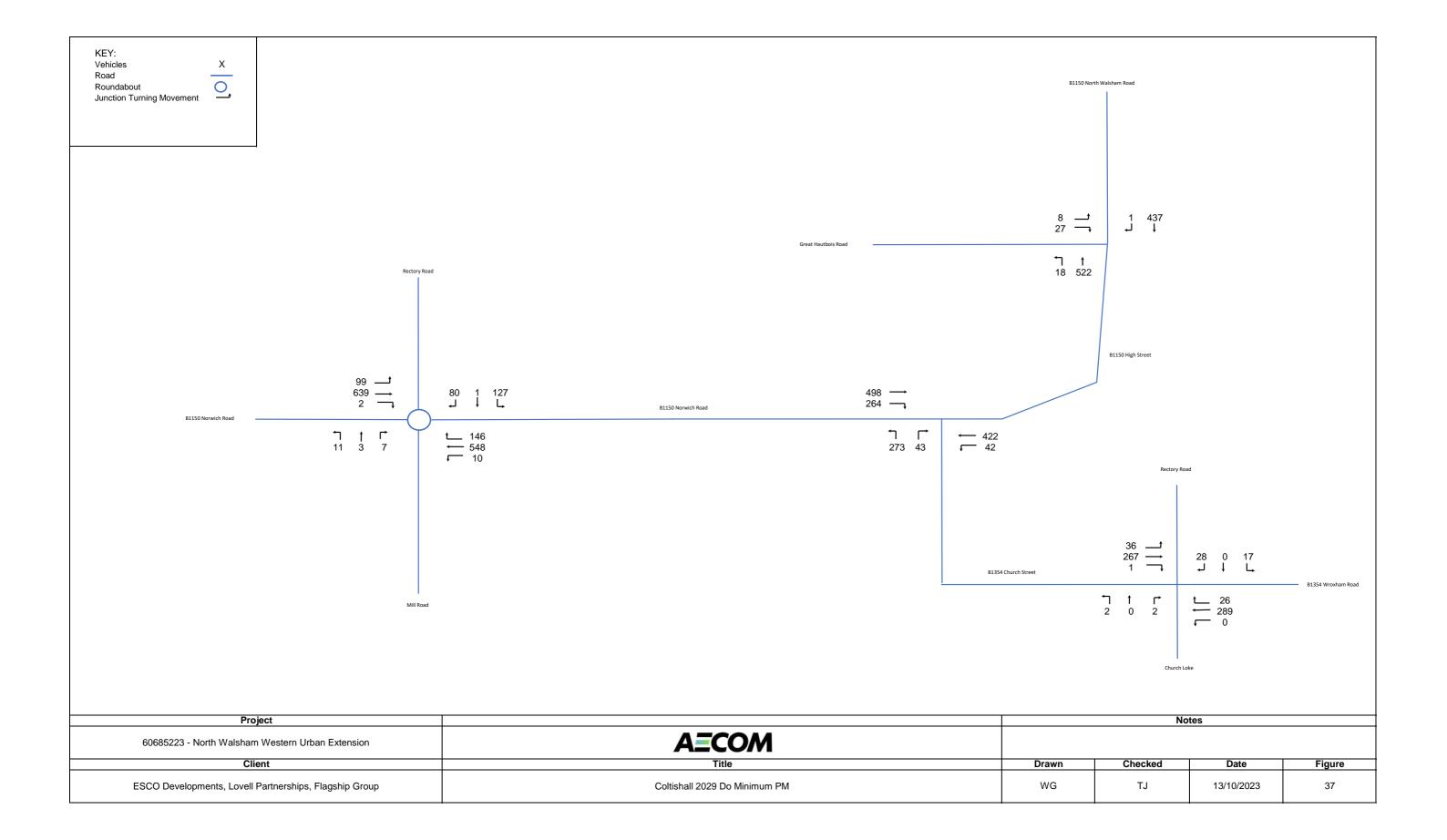


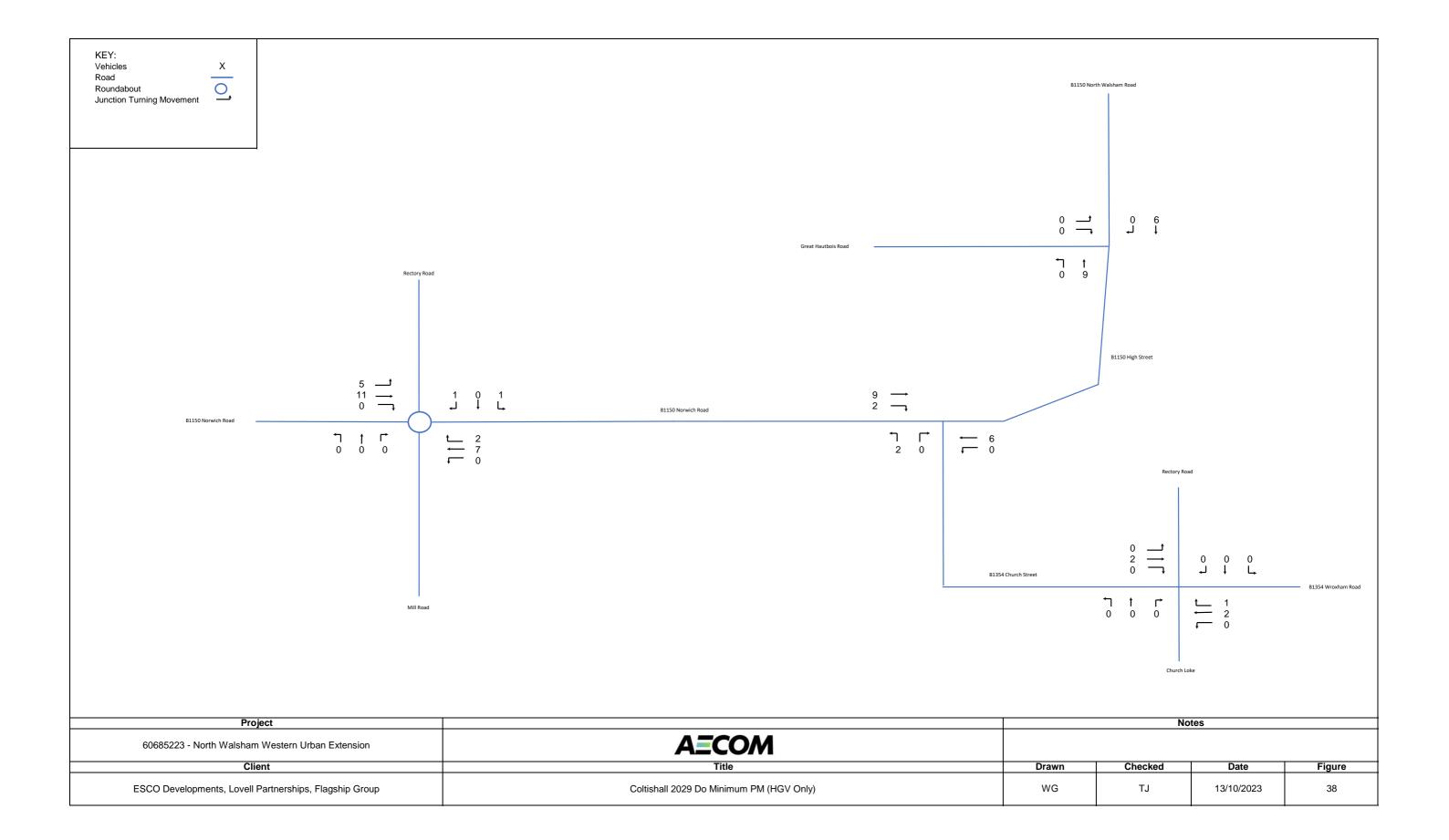


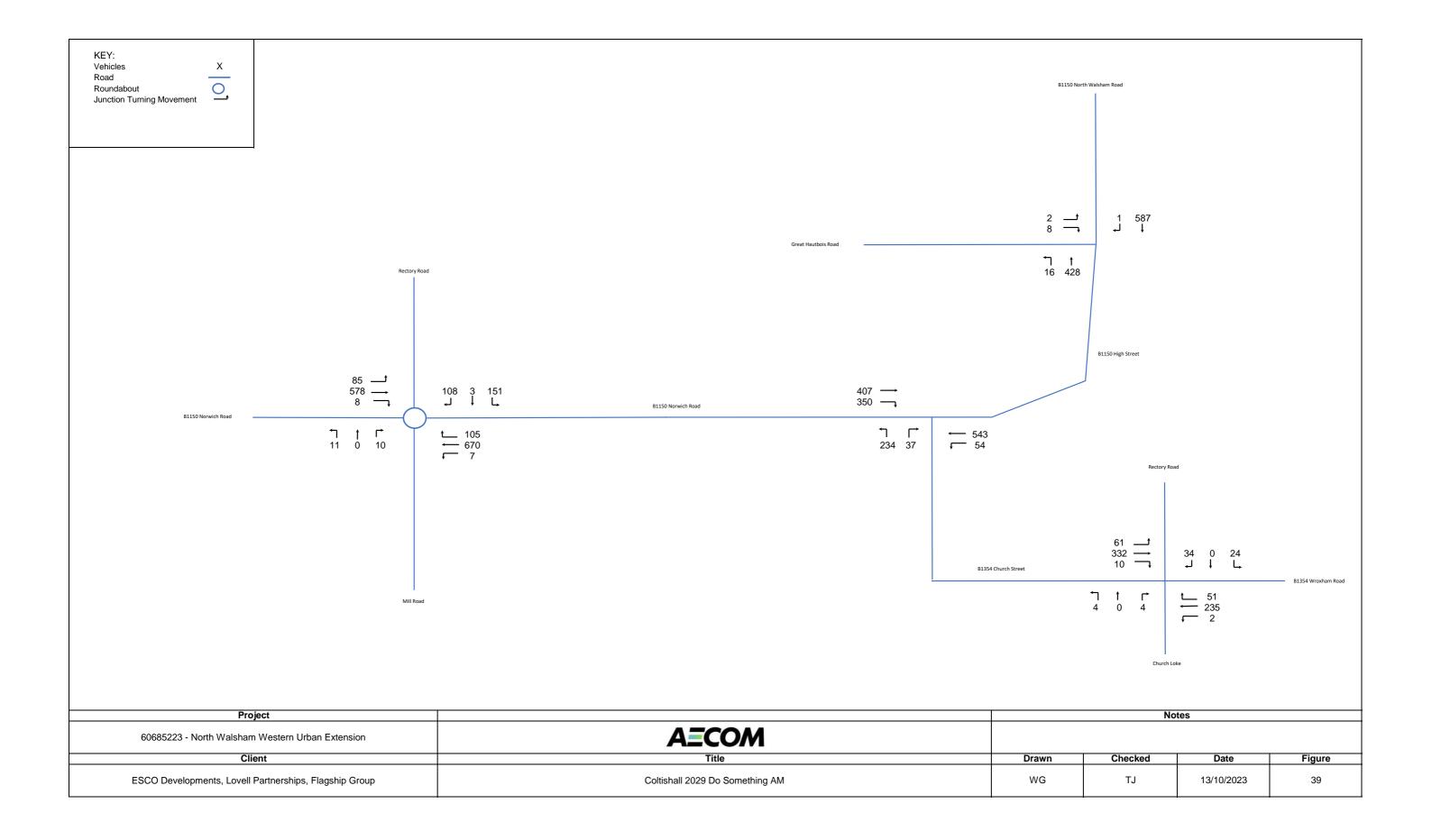


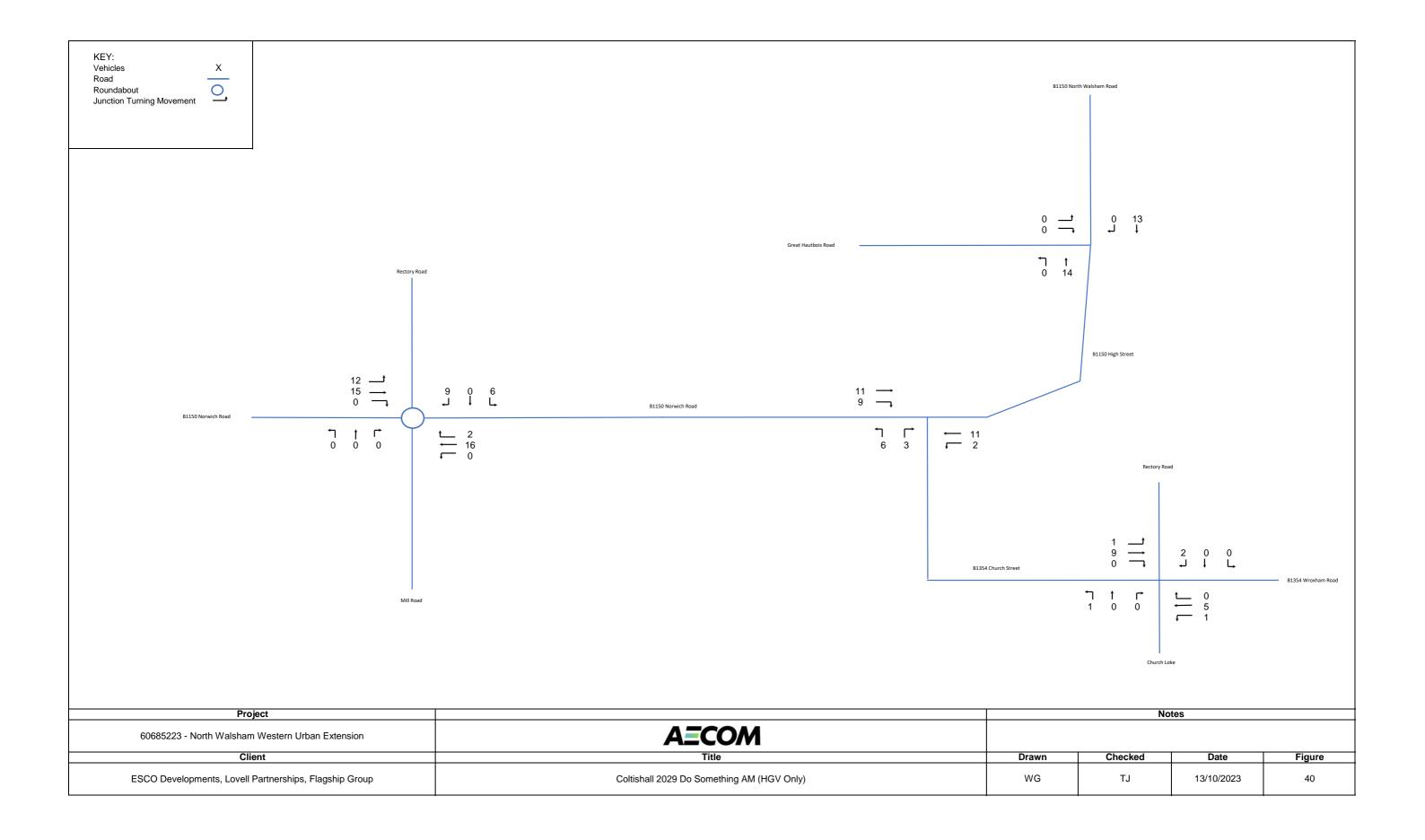


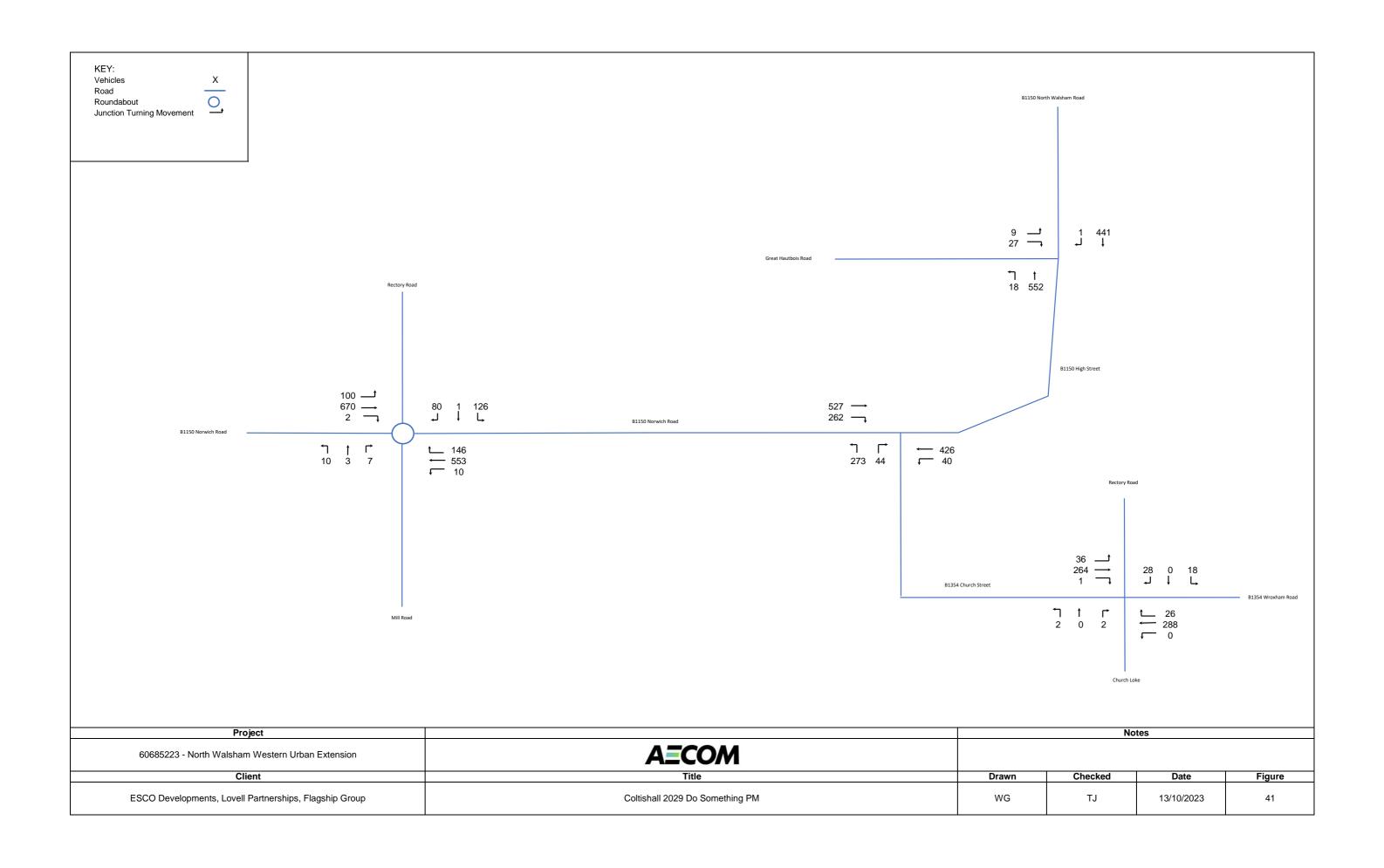


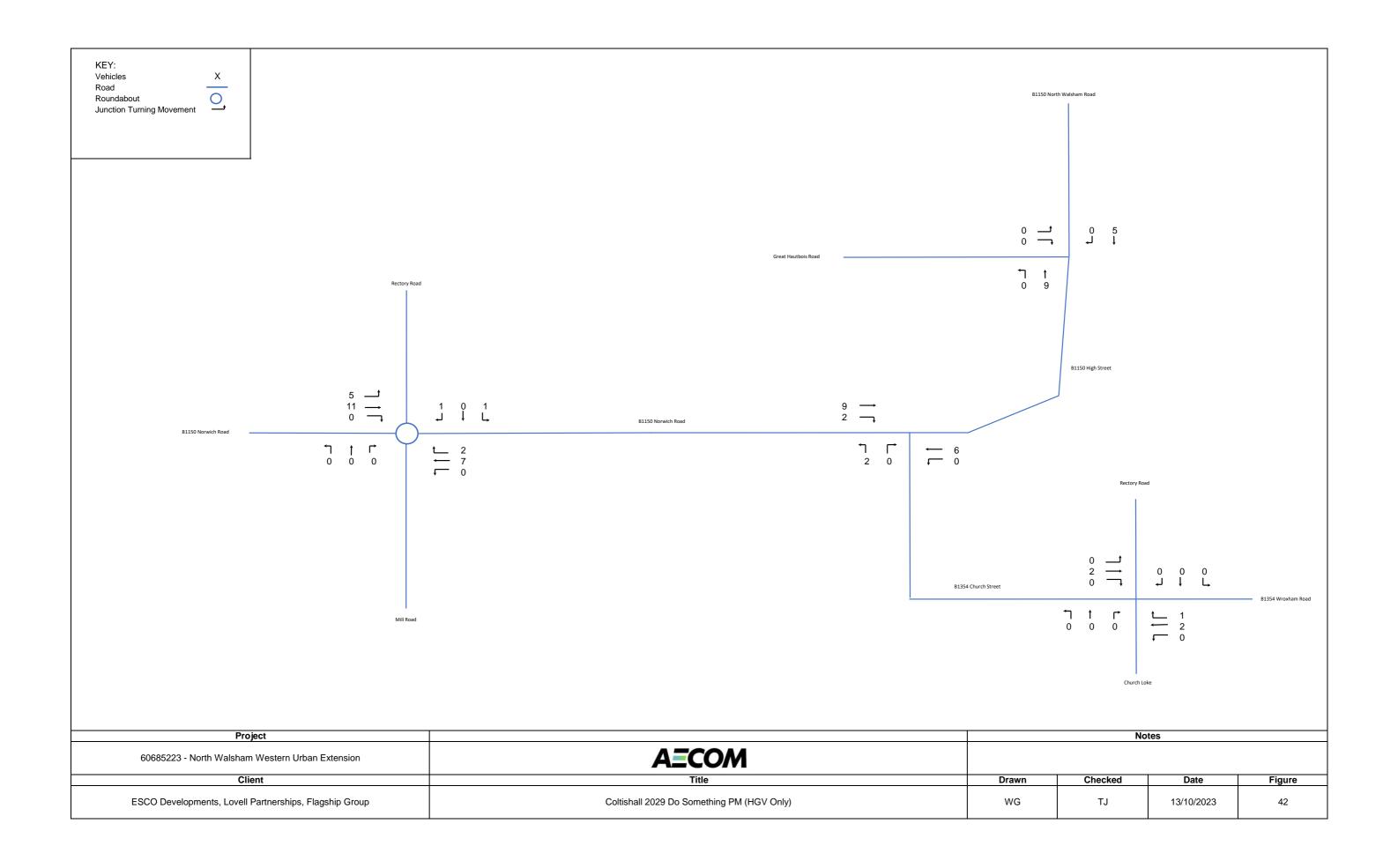


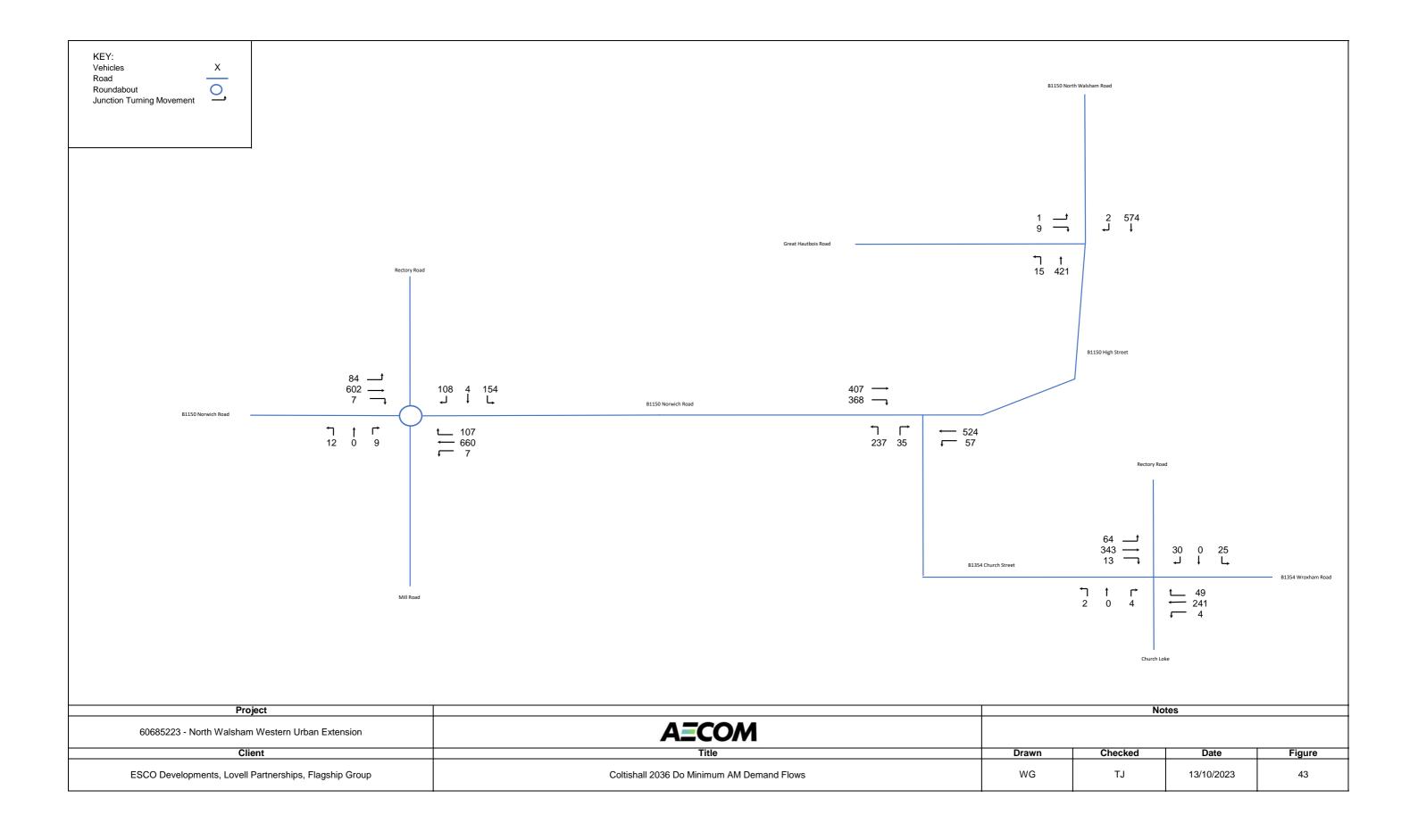


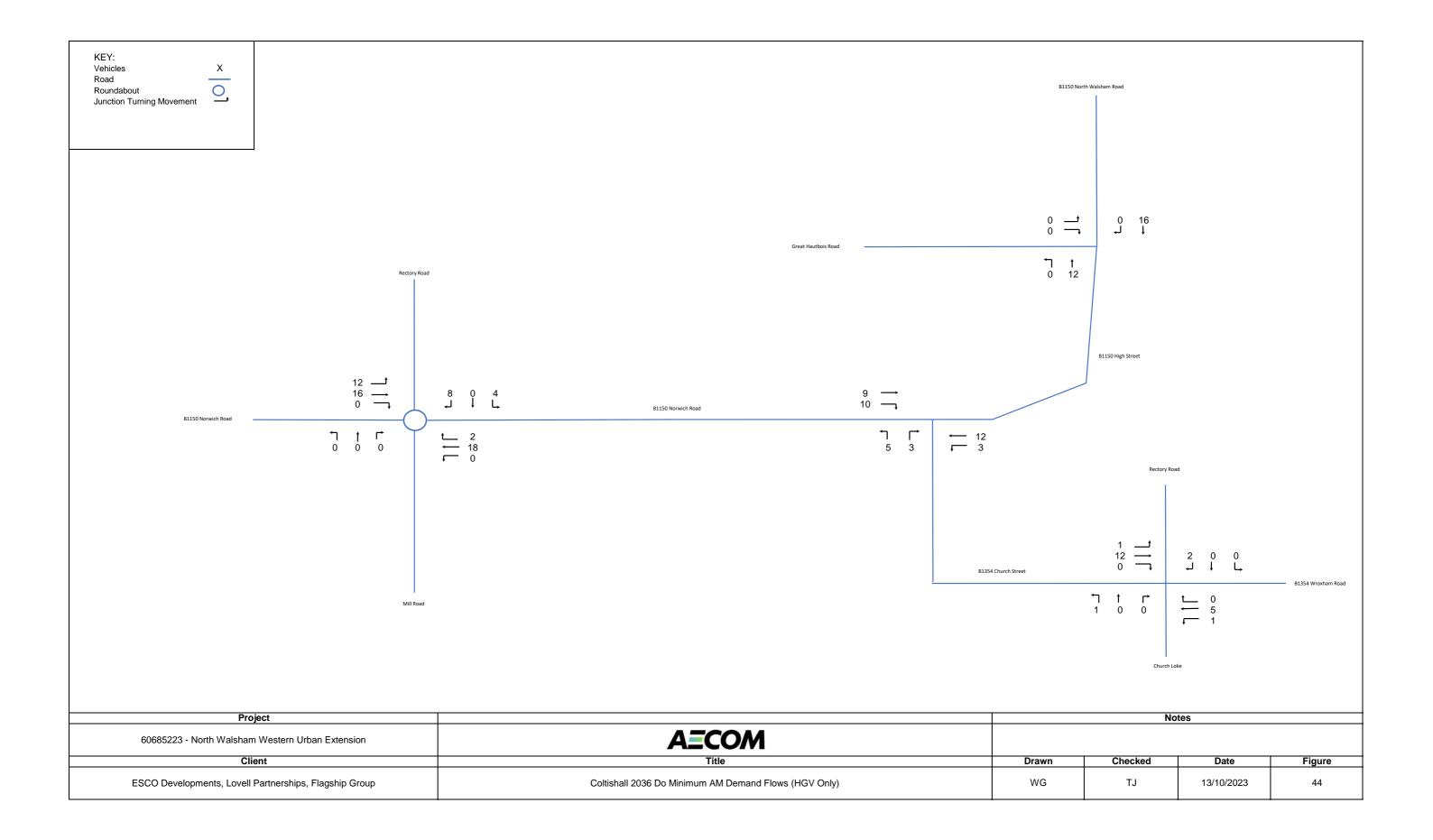


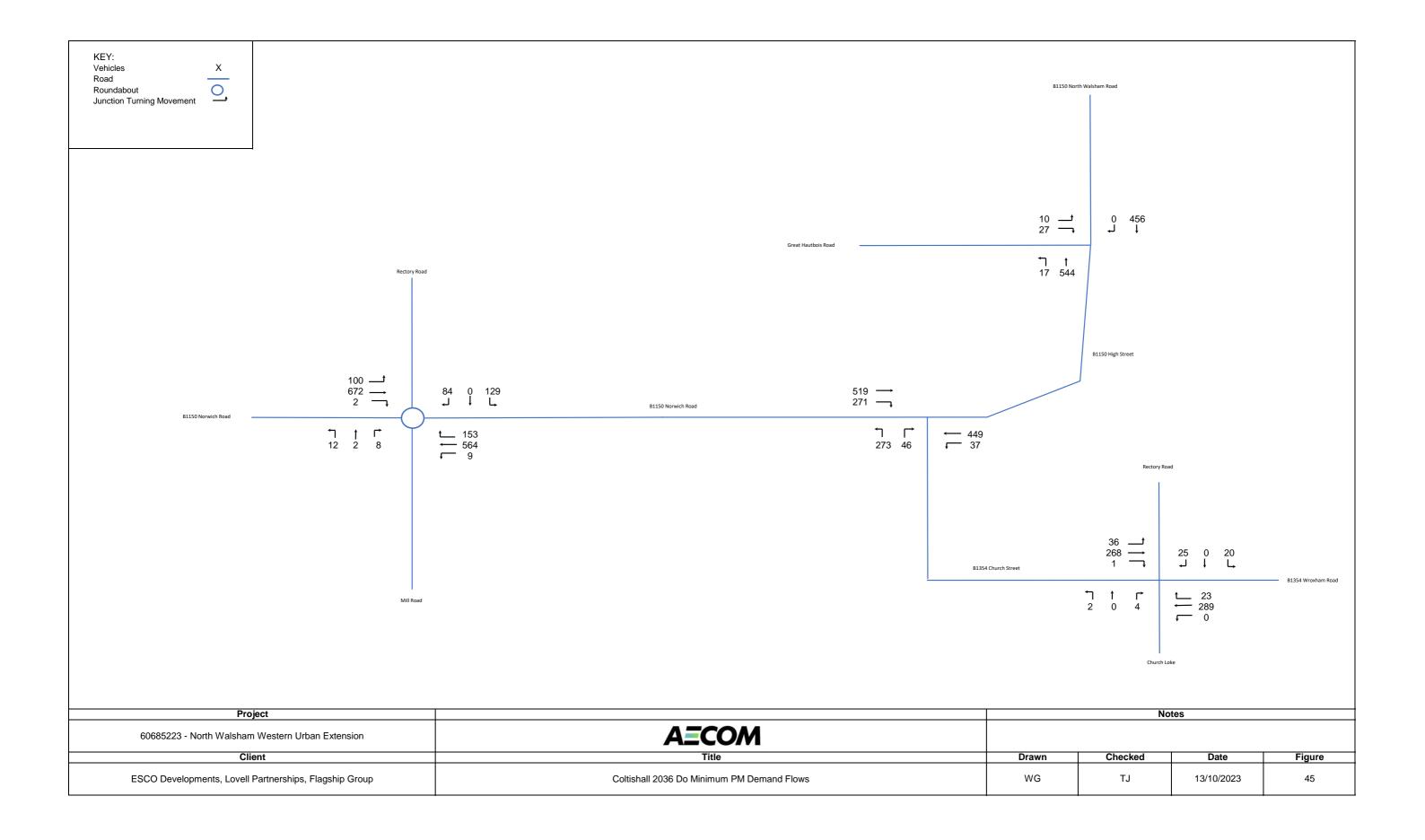


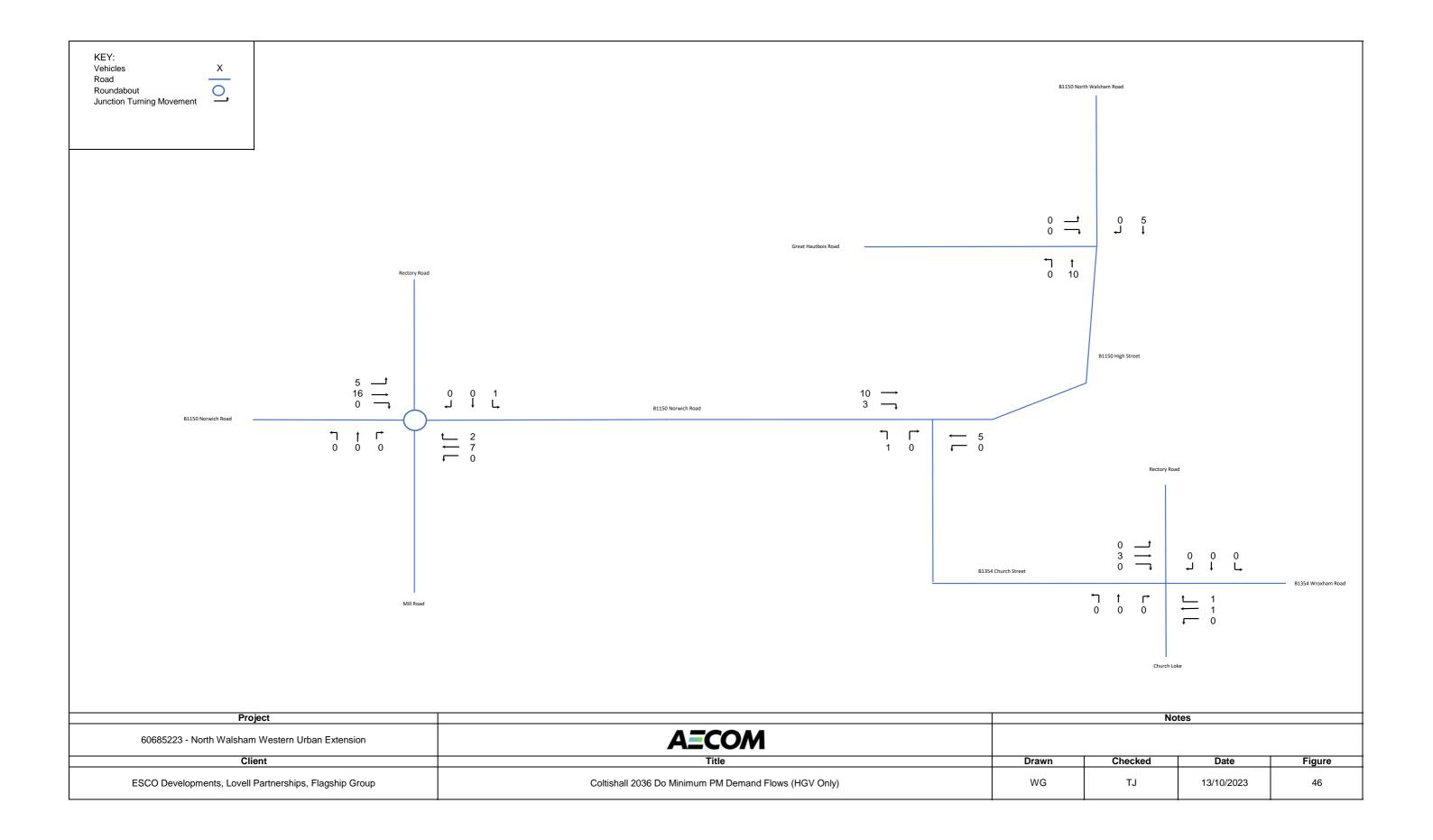


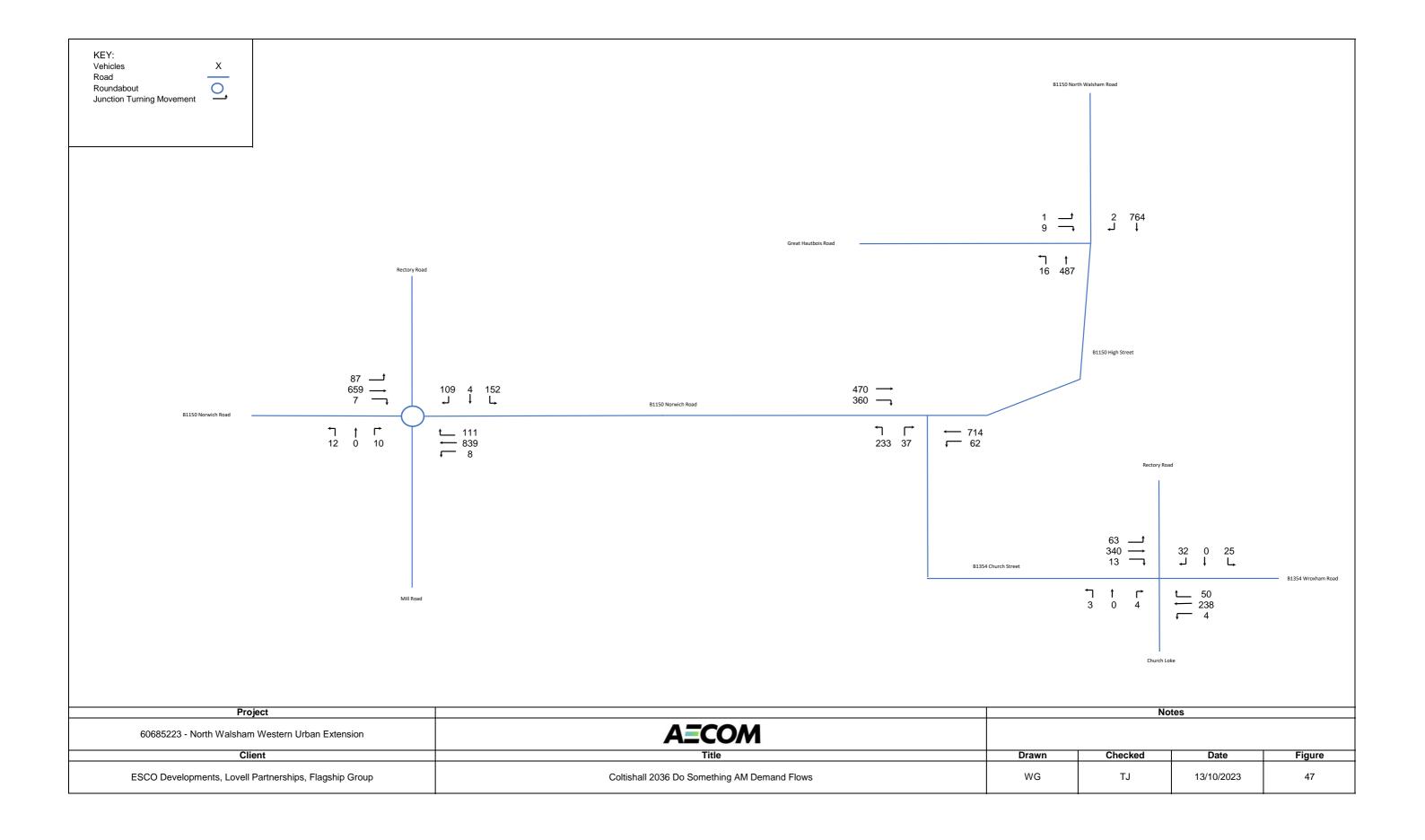


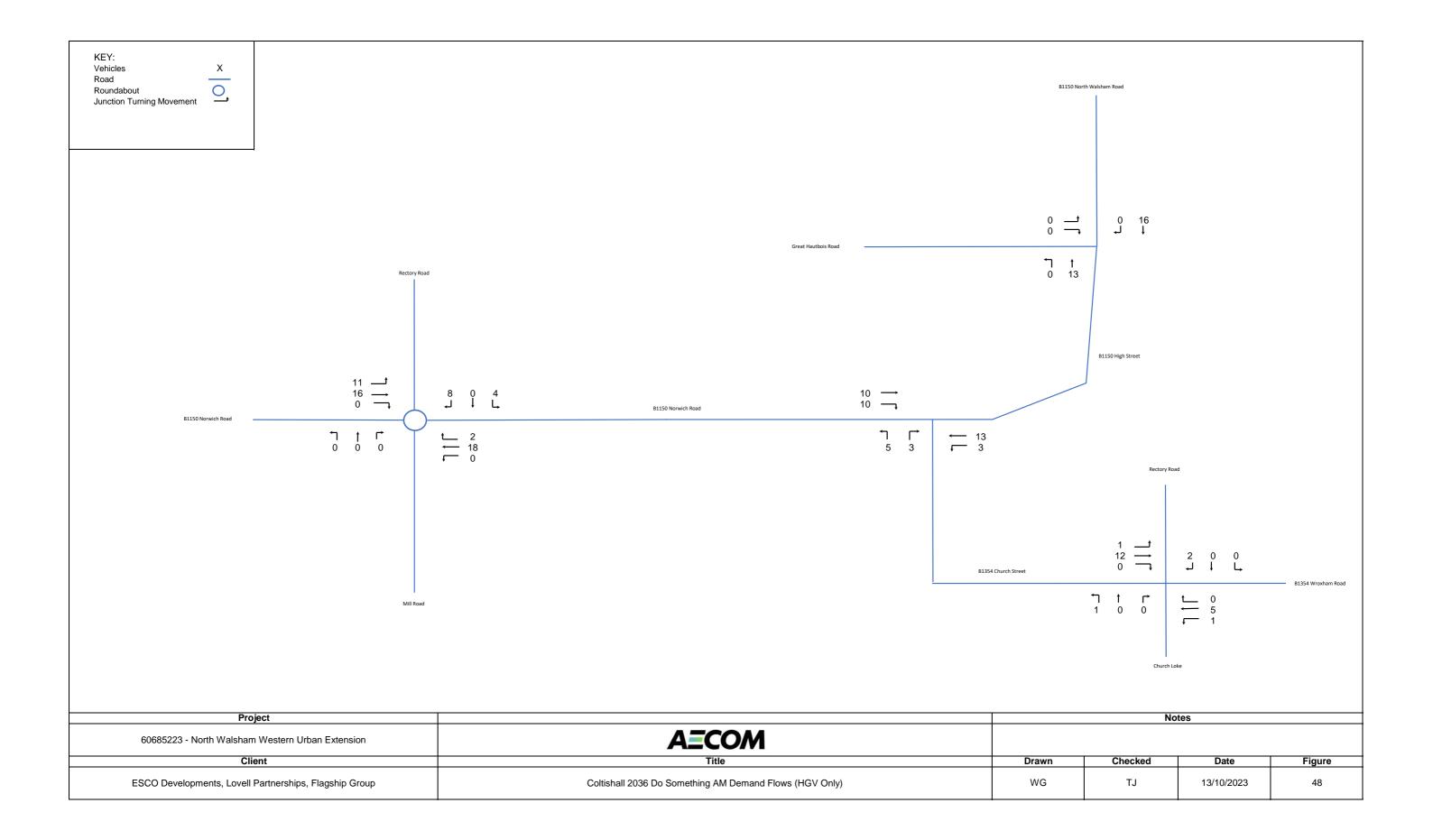


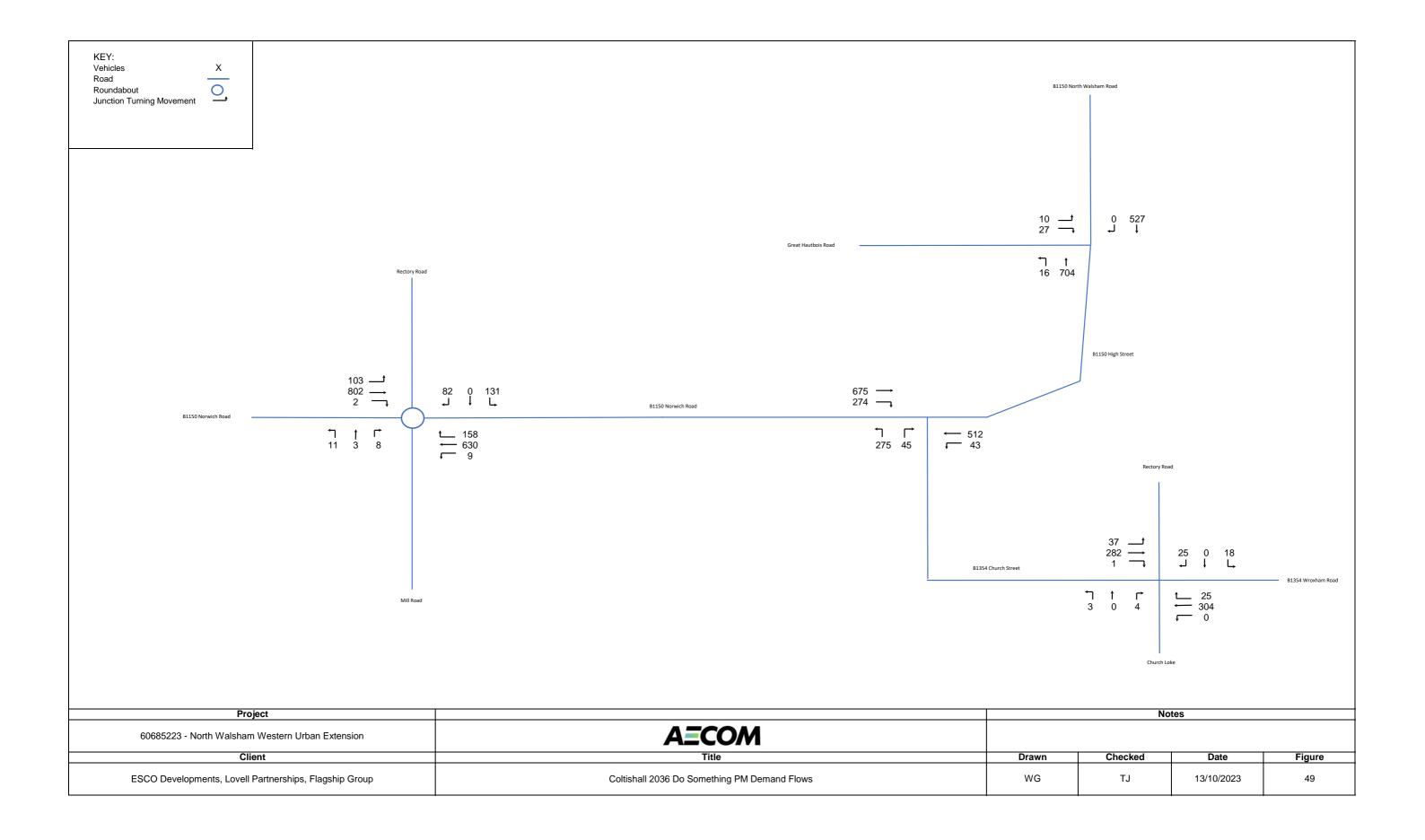


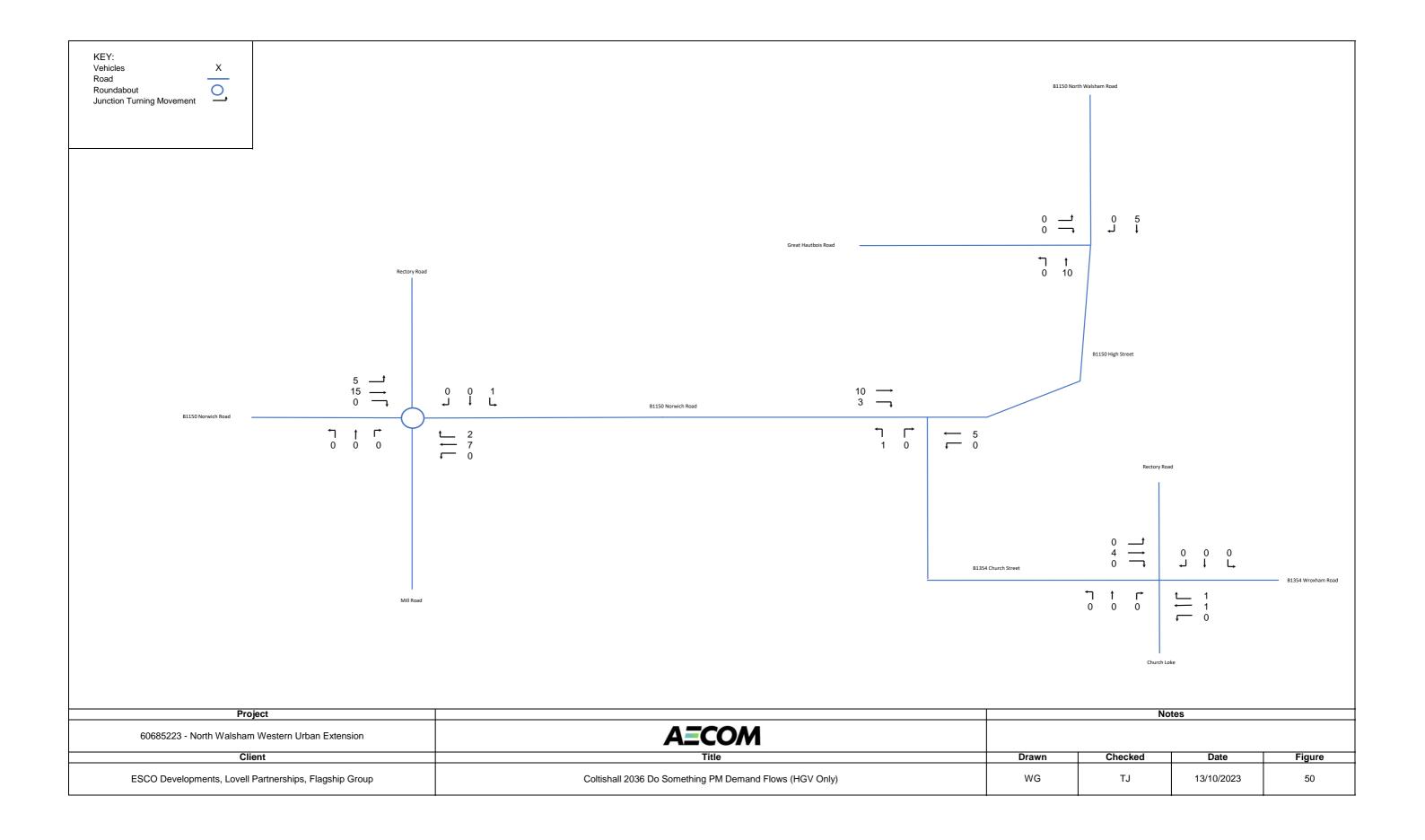


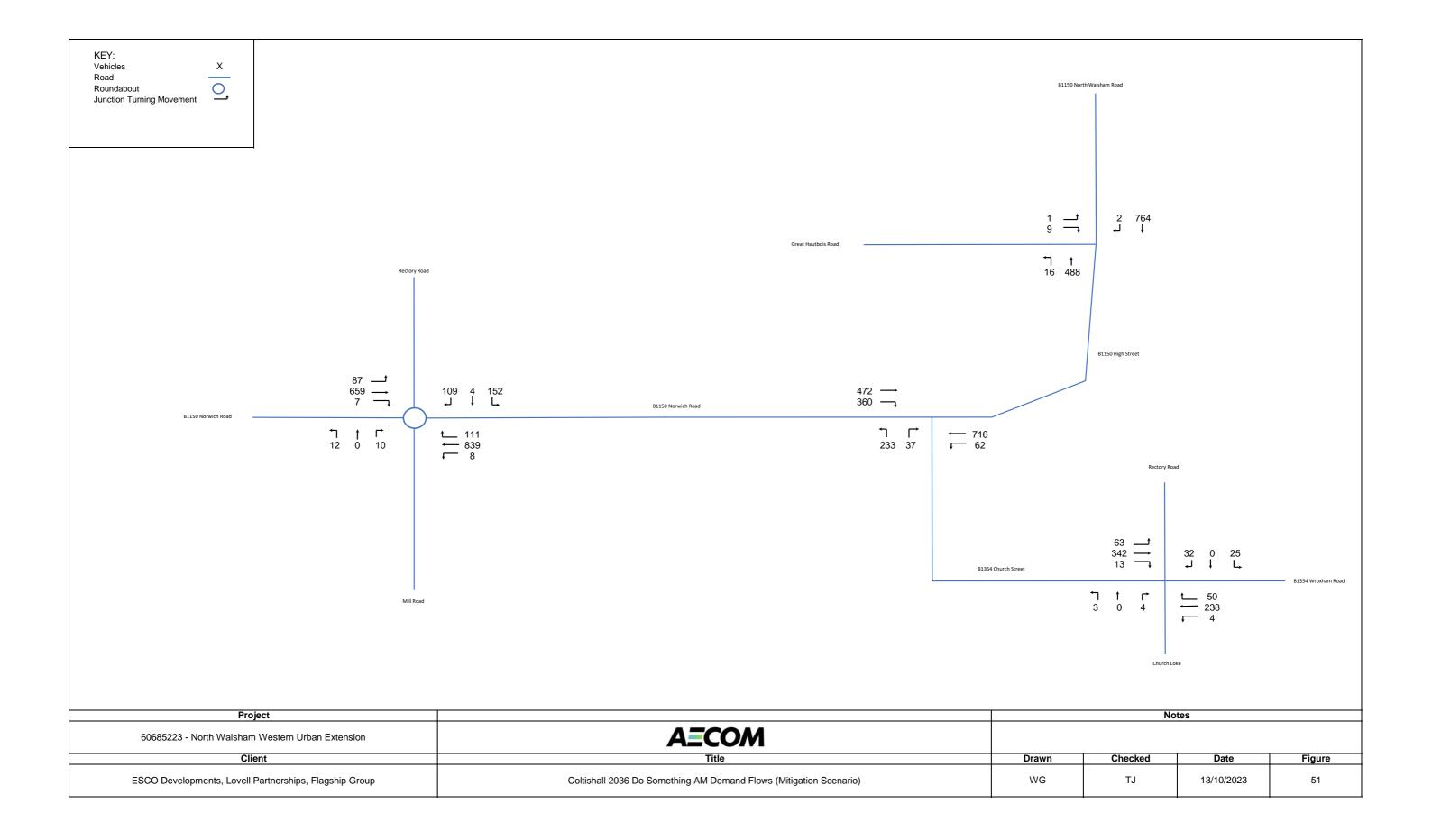


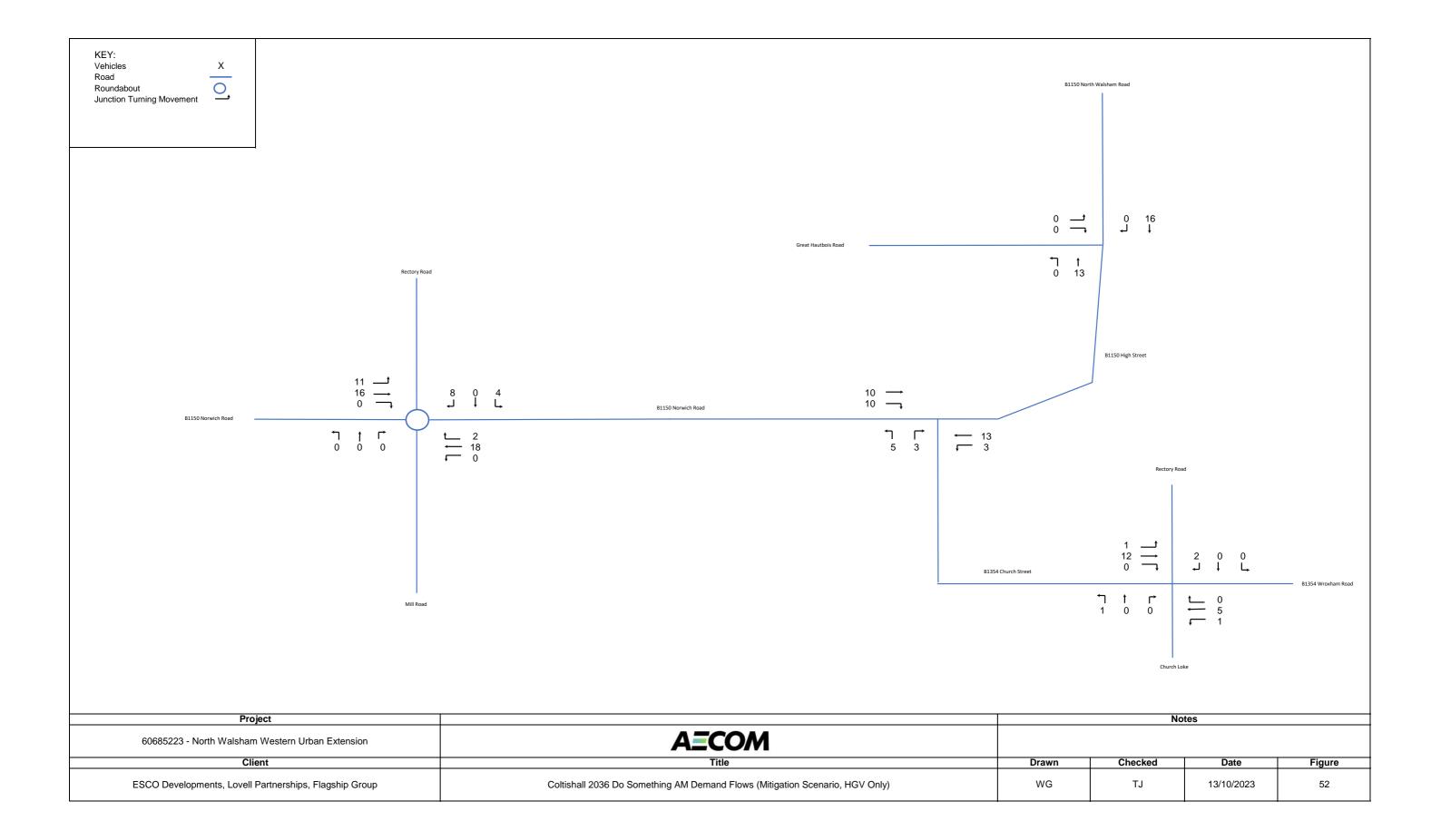


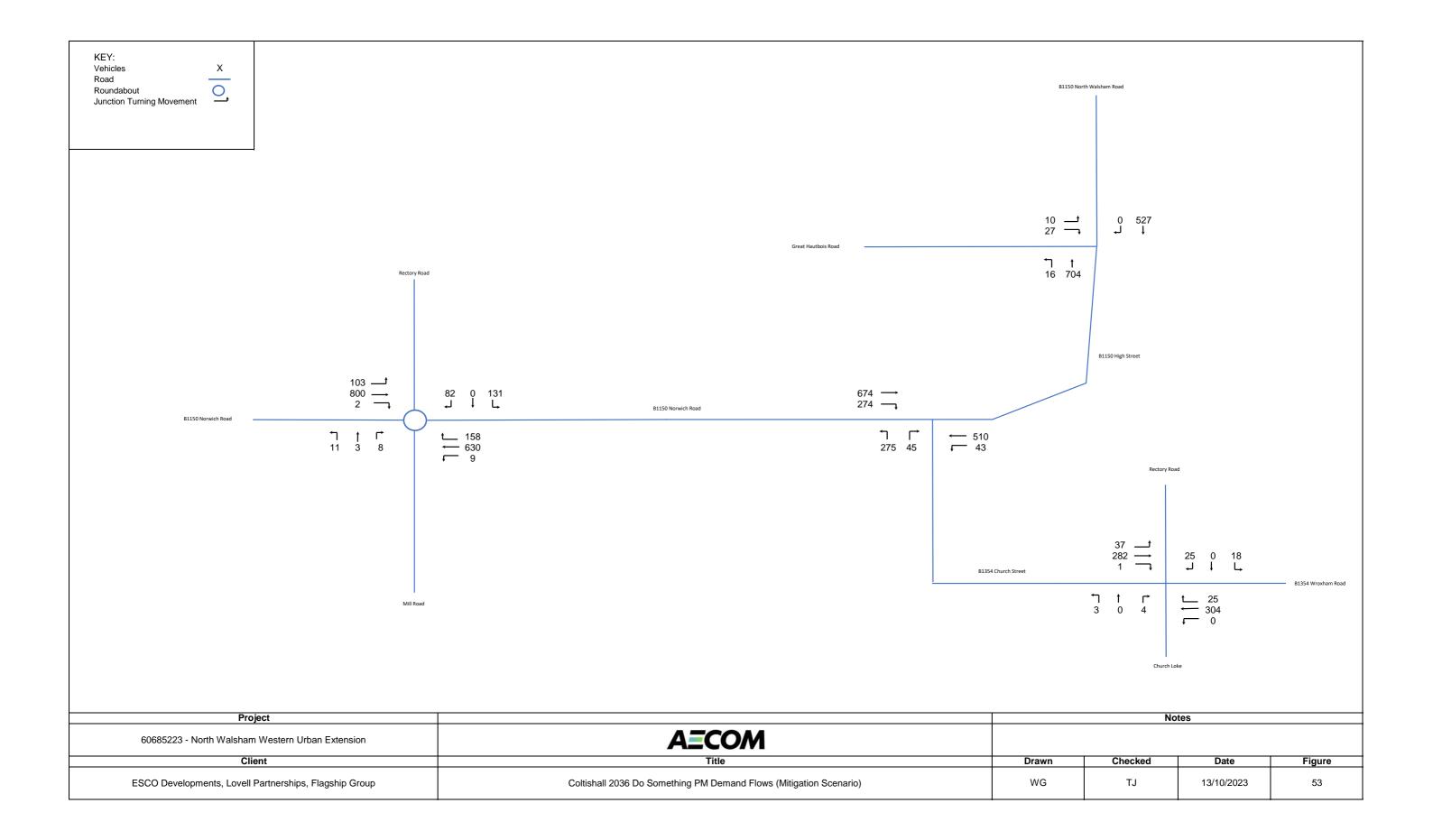


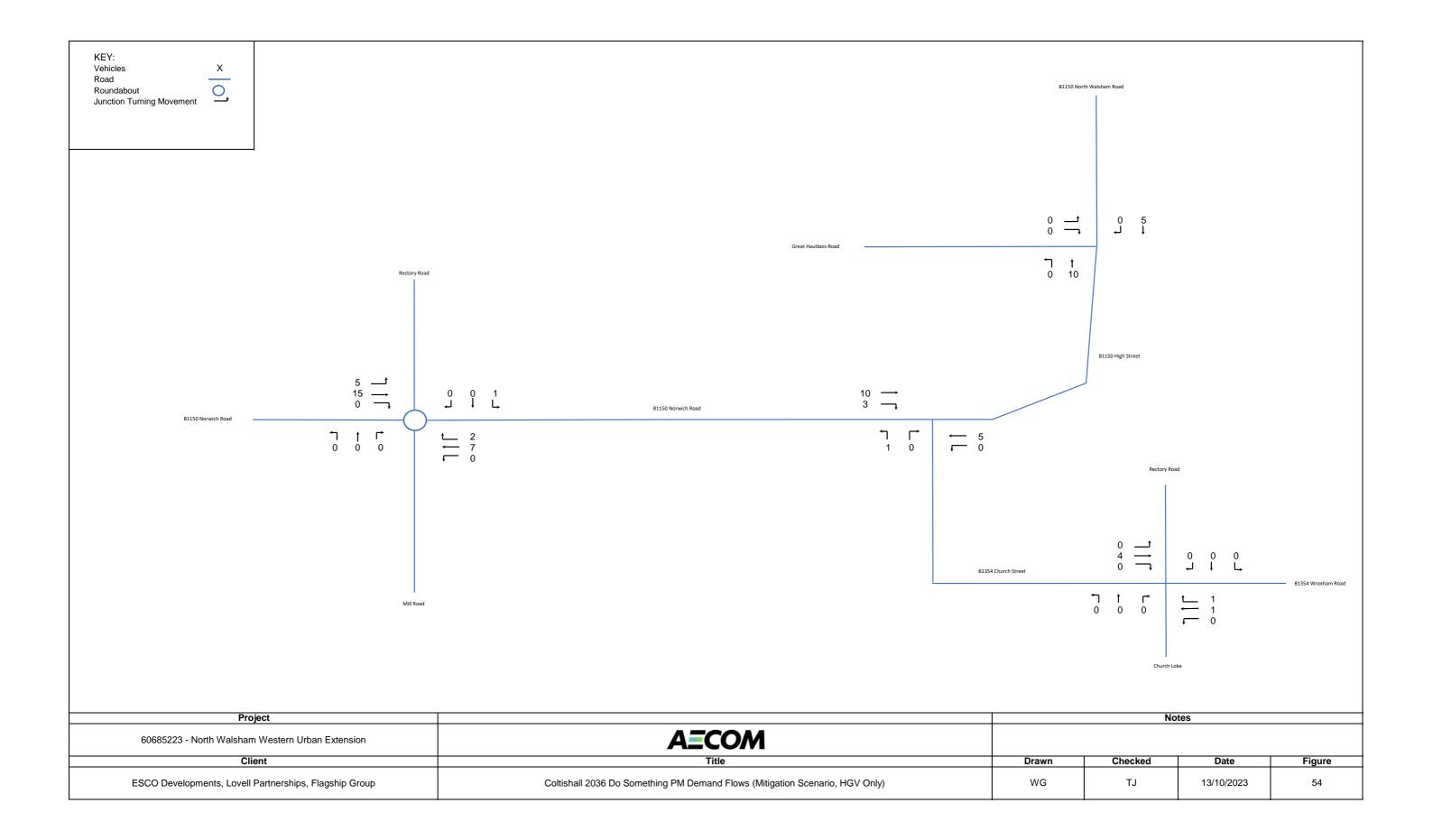


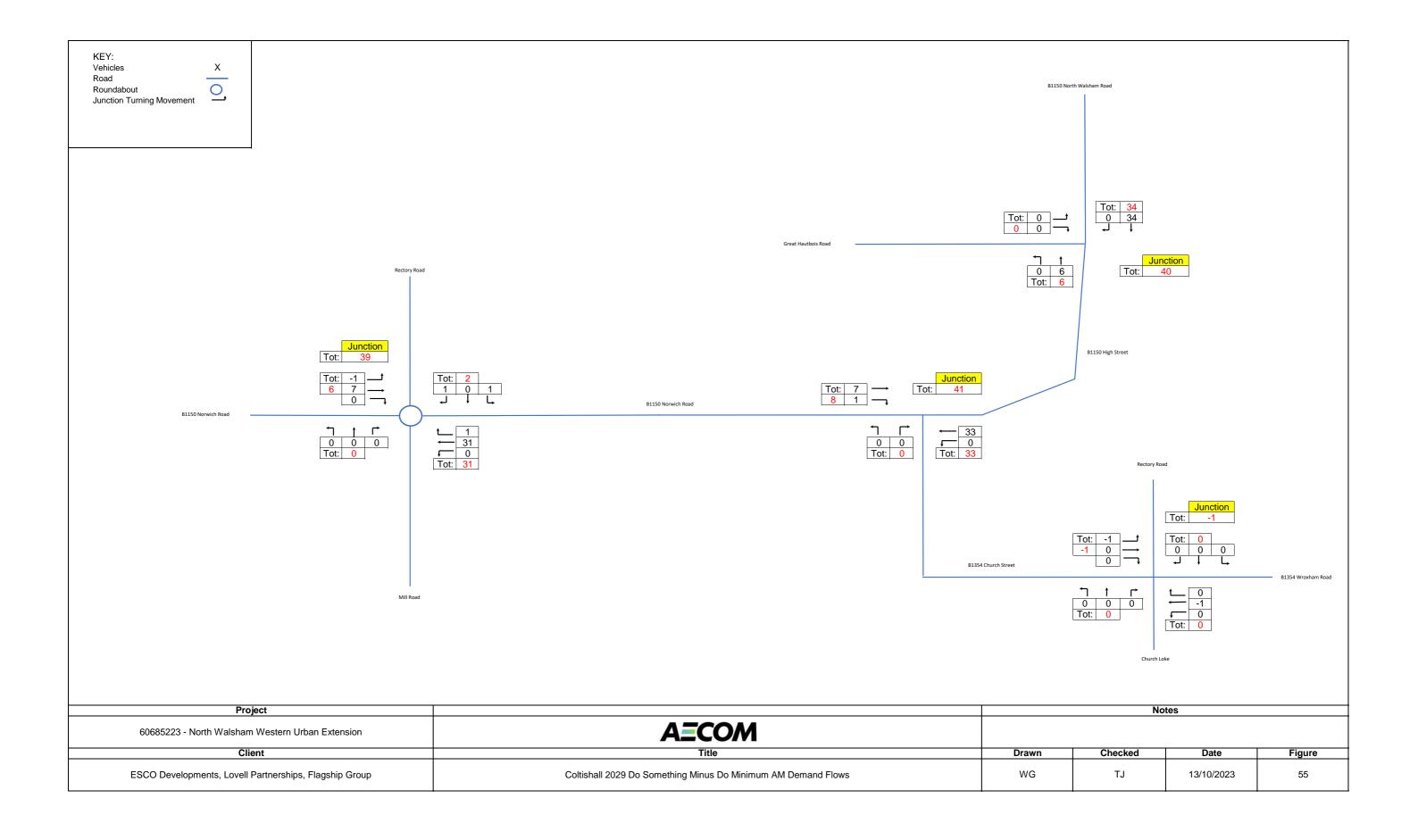


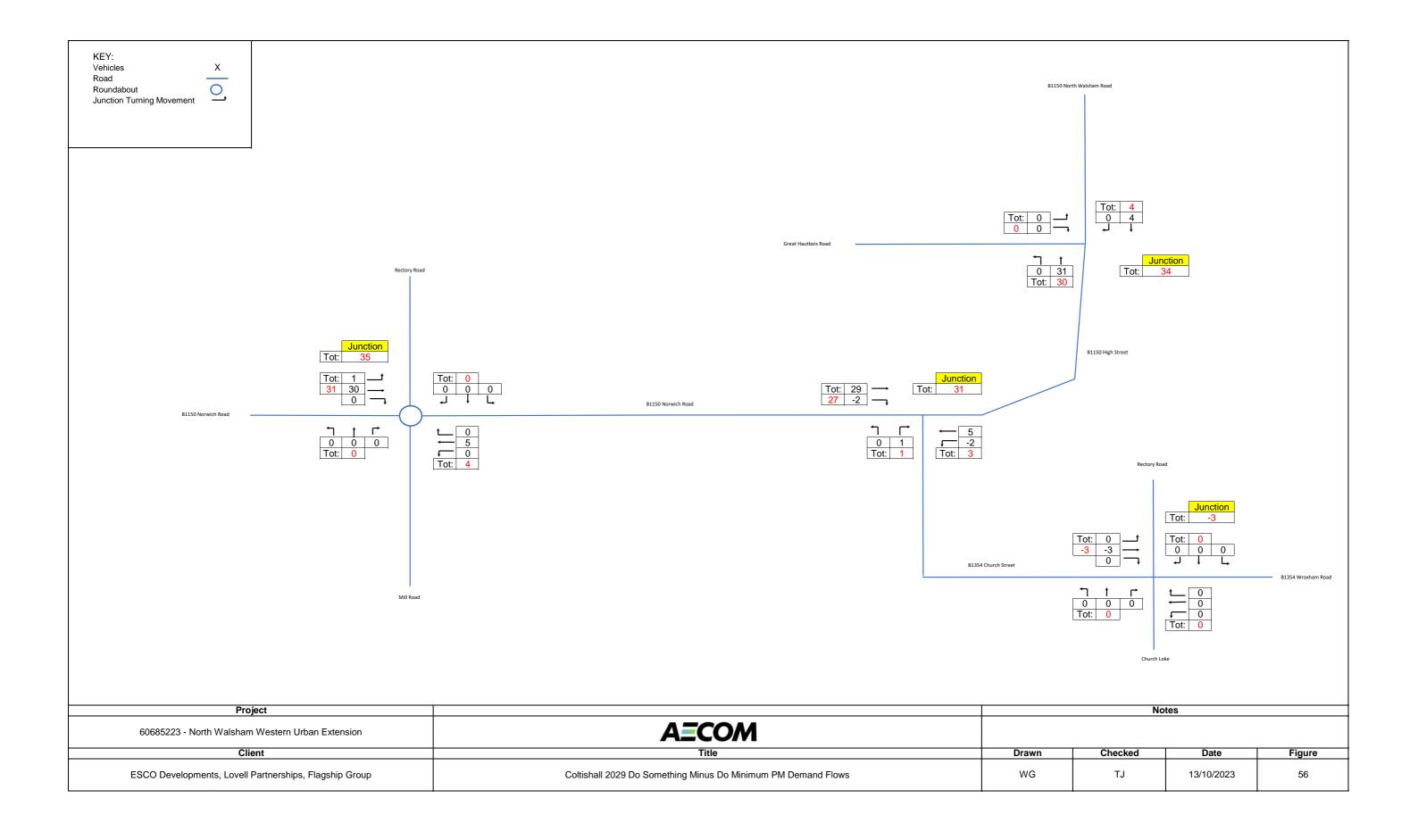


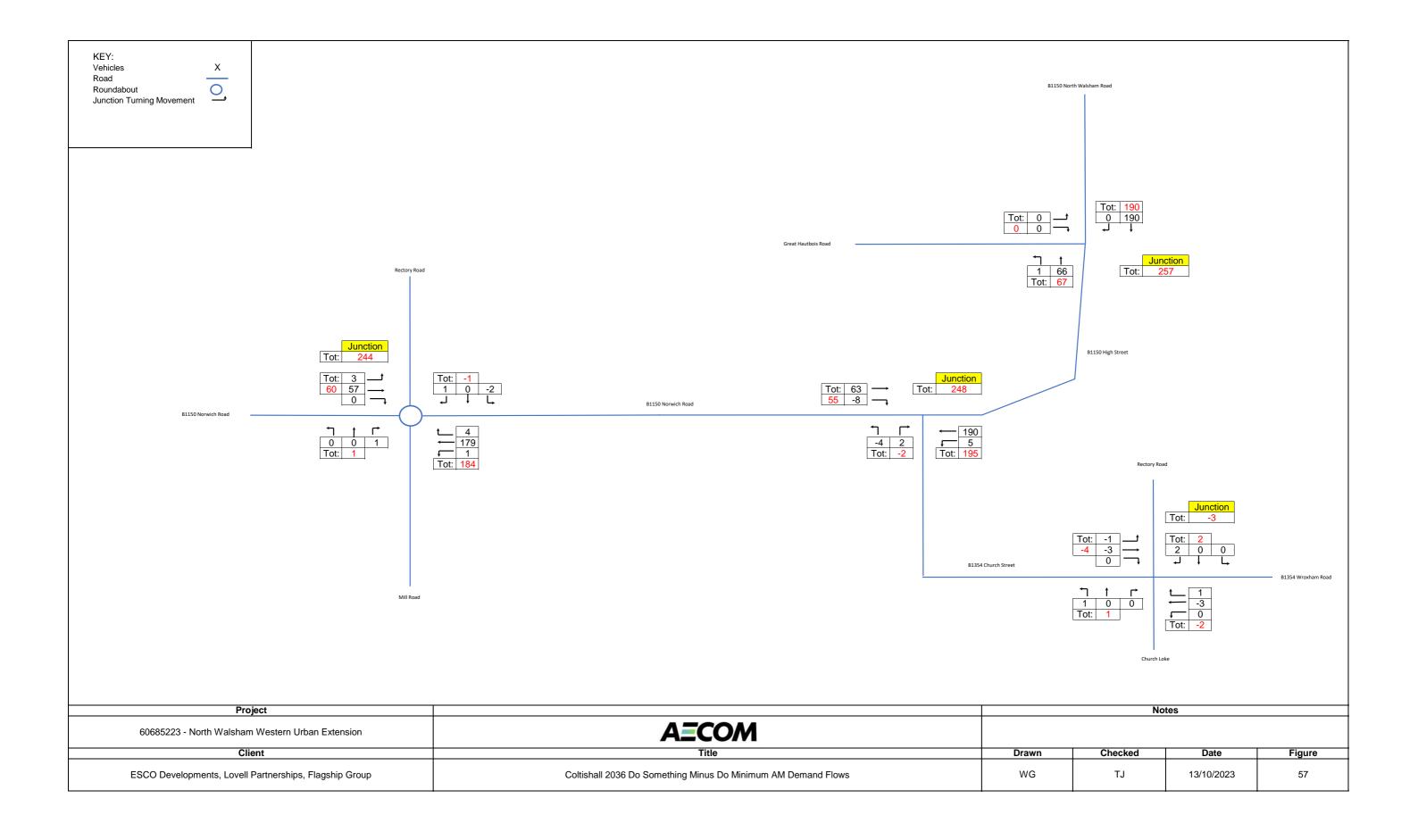


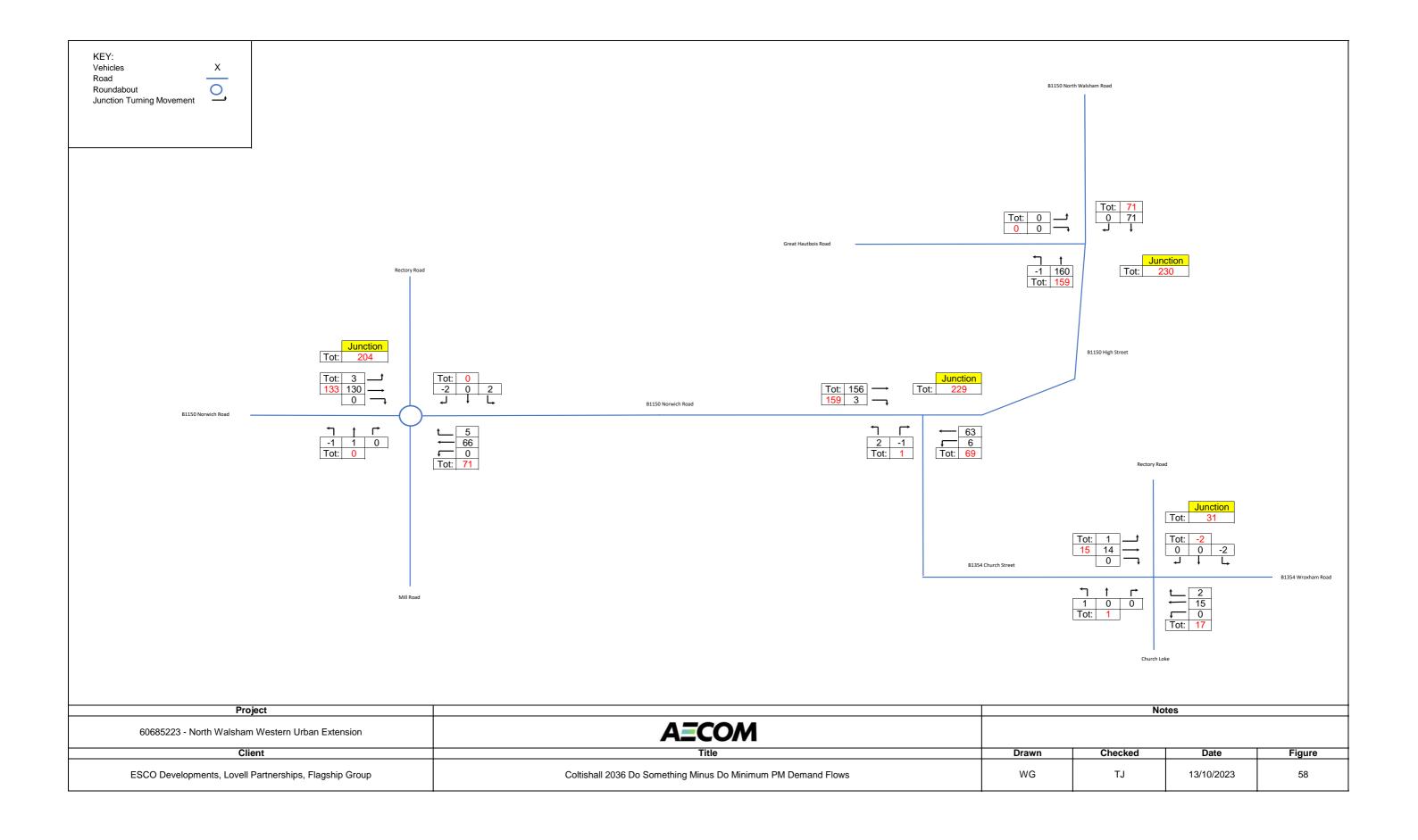


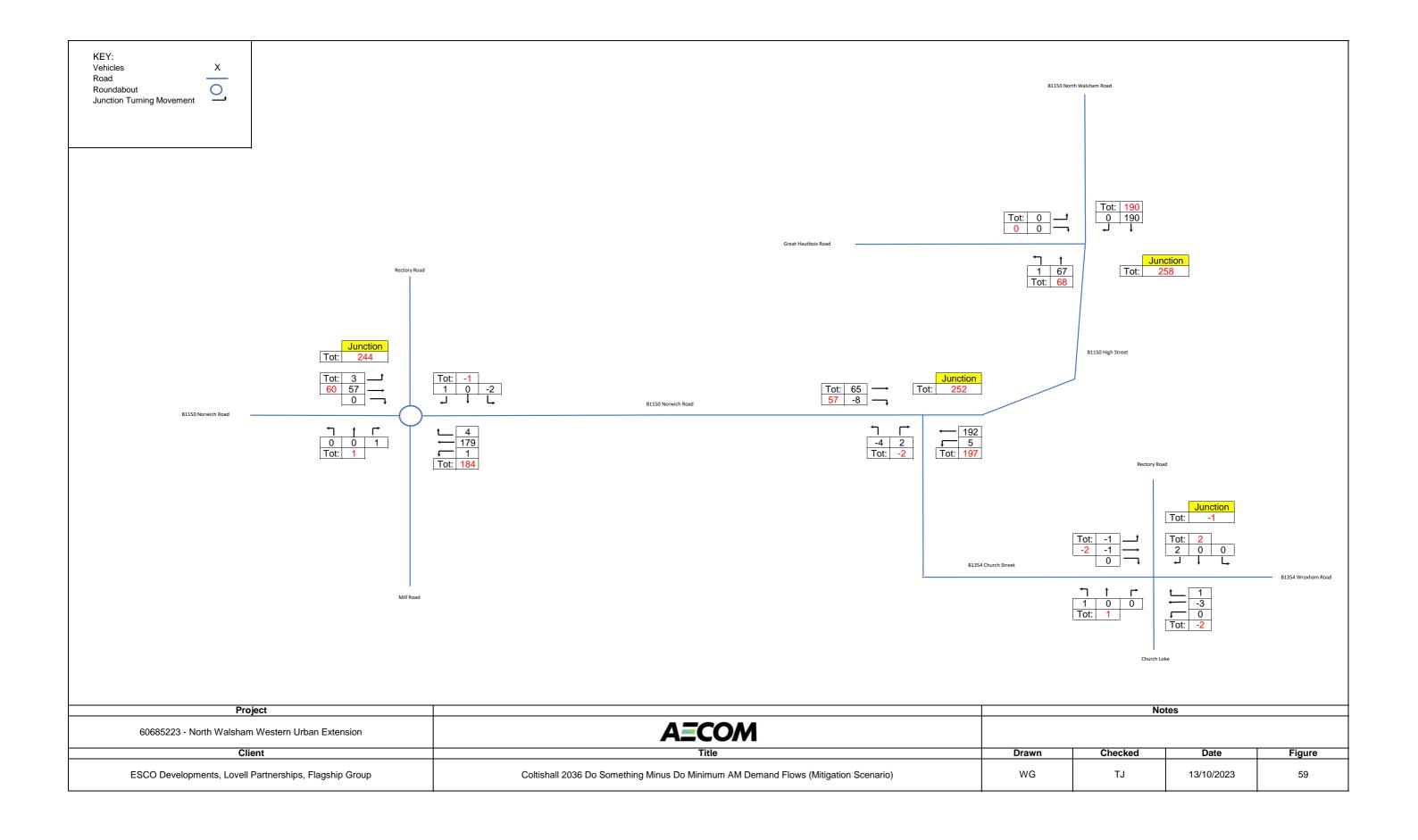


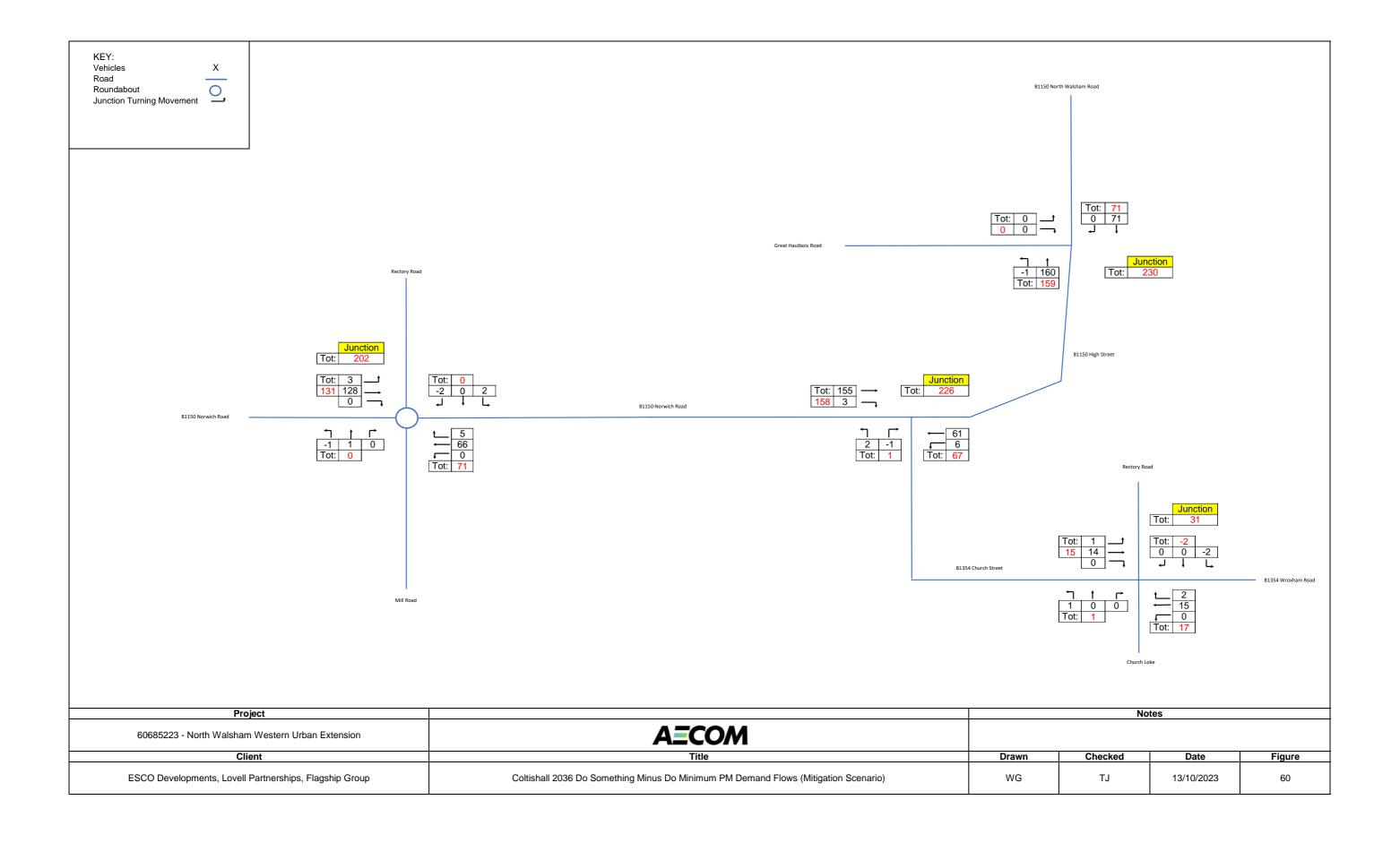












Appendix D – Local Model Validation Reports





North Walsham Vissim Model Validation Report

ESCO Developments, Flagship Housing Group and Lovell Partnership

13 April 2023

Quality Information

Prepared by	Checked by	Verified by	Approved by
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Revision History

Revision	Revision date	Details	Authorized	Name	Position
0.1	17 February 2023	First Draft		Javier Navarro Pardo	Principal Consultant
0.2	13 March 2023	Second Draft		Phil Arnold	Associate Director
1.0	13 April 2023	Draft Issue for Client Comment		Bevin Carey	Regional Director

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Introduction

Background and Report Structure

- ESCO Developments, Flagship Housing Group and Lovell Partnerships have commissioned AECOM to 1.1 develop a Vissim base model of the town of North Walsham to assess the impacts of increased demand in forecast years and the proposed North Walsham Western Urban Extension (NWWUE). The model has been calibrated and validated to replicate the operation of the town based on data collected in July and November
- This report documents the data collection and analysis, the development of the network and base year 1.2 demand, and the calibration/ validation. The report is structured as follows:
 - Data collection and analysis;
 - Demand development;
 - Modelled Network;
 - Calibration results;
 - Validation results; and
 - Conclusions.

Model Scope

1.3 The Vissim model has been developed for the area shown in Figure 1-1. The North Walsham network comprises three signalized junctions and numerous priority-controlled junctions. The Vissim model area includes the A149, which runs through the town with the signalized junctions with the B1150 and B1145.



Figure 1-1 - Modelled Area

- Figure 1-2 below shows the key junctions/ links identified from the survey data/ observations in the model area that are significant to local network operation. The key junctions/ links are as follows:
 - 1 Cromer Road and Bradfield Road;
 - 2 Cromer Road and Greens Road;
 - 3 Cromer Road, A149 and B1145;
 - 4 Cromer Road, Aylsham Road, Mundesley Road and Market Street;

- 5 Aylsham Road underpass;
- 6 B1150 Norwich Road and A149 North Walsham Bypass; and
- 7- B1150 and Millfield Road.
- 1.5 These junctions/ links have been considered when developing the model to replicate the existing operation and driving behaviour observed in the video footage available. It should be noted that the operation at some of these locations is dependent on variable factors such as on-street parking, physical constraints, and courtesy/ give way behaviours, which have been modelled and calibrated to observed queuing patterns/levels of delay.



Figure 1-2 – Junctions in North Walsham Model Area

- 1.6 The Vissim Base models have been developed for the AM and PM peak hours, including 30 minutes warmup and 15 minutes cool-down periods, to make sure the network is saturated at the beginning of the peak hour and to allow vehicles to complete their journeys after the peak hour.
- 1.7 The Base models have been developed in line with modelling requirements and the calibration and validation criteria defined in Transport Analysis Guidance (TAG) and the Guidelines for the Use of Microsimulation Software published in May 2022 by National Highways.

2. Data Collection and Analysis

Introduction

- 2.1 The data collection exercise undertaken by AECOM to inform the Vissim Base model development has been summarised in this section. The data collection comprised the following survey types:
 - Automatic Number Plate Recognition (ANPR) data;
 - Manual Classified Turning Counts (MCTC) Data; and
 - Automatic Traffic Counts (ATC) data.
- 2.2 The data collection took place between the 12th and 14th July. However, upon review, road works were identified on the 12th of July, which resulted in non-standard delays and routing on this day. The data from the 12th of July was therefore not used.
- Further analysis into the survey data, especially on ANPR sample rates showed that there was a noticeably 2.3 lower capture rate on the 14th of July compared to the 13th of July across several cameras including key sites such as Site 11 northbound on the B1150.
- 2.4 An example of the sample rate analysis which was undertaken of the ANPR data can be found in Figure 3.1 for the AM and PM peak hours. The graphs in Figure 3.1 show a large flow difference between the vehicle numbers captured by the ANPR and the total flows along the road on the 14th of July 2022, while the data on the 13th of July show a close match between the two data sets.

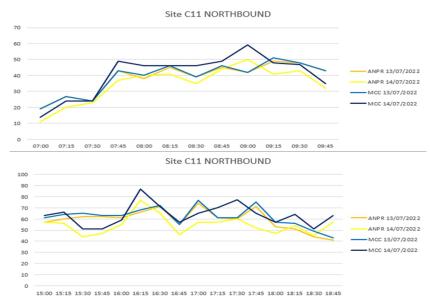


Figure 2-1 – ANPR performance 13th/14th July

2.5 As a result of the initial survey data analysis undertaken it was decided that only the data collected on the 13th of July 2022 will be used to support the VISSIM model development. The ANPR data obtained on the 14th was used to as further verify that origin-destination patterns on the 13th of July were typical.

Automatic Number Plate Recognition (ANPR) data

- The ANPR data collection was categorized into two groups of cameras, Figure 2-2 shows the camera 2.6 locations.
- 2.7 The cordon cameras were defined to capture the origin/destination demand across the area and total journey time through the model area.
 - The internal cameras were defined to capture the internal routing within the model area and split the journey times into sections.

- 2.8 The ANPR data was used to develop the demand matrices and to provide journey times between origins and destinations. The internal cameras were also used to inform the routing through the model area and define the journey time sections used in the model validation.
- 2.9 As shown in Figure 2-2 some of the ANPR cameras lie outside the modelled area. Whilst these cameras were not used as journey origins or destinations, the routing information obtained from them was also used to inform the routing within the model.
- In addition to the routing and journey time information, the ANPR surveys also included Manual Classified Counts (MCCs) associated with each camera to record the capture rate and classify ANPR data.

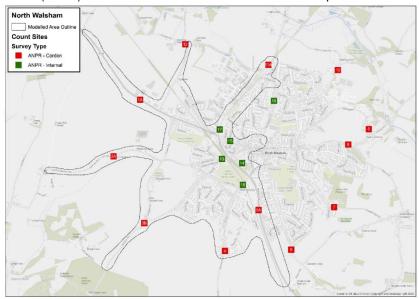


Figure 2-2 - ANPR Cameras

- It should be noted that the ANPR data and routing information is based on the number plates captured successfully during the surveys. Table 2-1 summarizes the captured rate (number of plates that were successfully recognised by the ANPR camera).
- 2.12 The capture and matched rates in Table 2-1 show that most cameras had a very high sample/ match rate, providing a high degree of confidence that the data reflects the demand and routing patterns within the study area.

Table 2-1 – ANPR Cameras Capture and Match Rate

Cita	Sample Rate					
Site	Overall	Inbound	Outbound			
1	99%	100%	99%			
2	99%	99%	99%			
3	98%	98%	98%			
4	98%	99%	97%			
5	99%	99%	99%			
6	99%	99%	98%			
7	94%	94%	94%			
8	98%	98%	97%			
9	86%	88%	84%			
10	99%	99%	99%			
11	98%	98%	98%			
12	94%	90%	98%			

Sample Rate

Site	Sample Rate				
Site	Overall Inbound		Outbound		
13	98%	99%	98%		
14	99%	-	99%		
15	98%	98%	96%		
16	97%	98%	97%		
17	98%	99%	97%		
18	98%	98%	99%		
Total	98%	99%	97%		

^{*} For internal cameras inbound refers to Eastbound or Northbound movement and outbound refers to Westbound or Southbound.

Manually Classified Turning Count (MCTC) data

- 2.13 MCTCs were carried out at the sites indicated in Figure 2-3 on the 12th,13th, and 14th July 2022, between 07:00 and 19:00. The MCTC data was used to refine the base model demand and calibrate the turning flows at each junction shown in Figure 2-3.
- 2.14 Additional MCTC surveys were undertaken on 10th of November 2022 to compare the traffic flow changes from the July 2022 data.

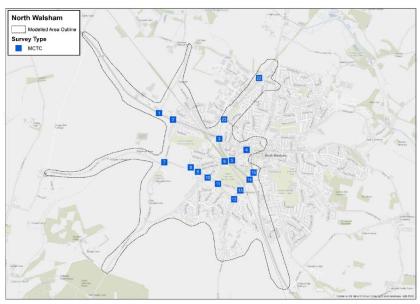


Figure 2-3 – Manual Classified Turning Counts sites

Automatic Traffic Count (ATC) data

- 2.15 The link counts were collected using ATCs. The ATC data was collected over two weeks period including the 12th, 13th, and 14th July 2022.
- 2.16 Seventeen ATC sites were surveyed in total that have been used to inform the total trip ends at the entry/ entry points to the model. Their locations are shown in Figure 2-4.

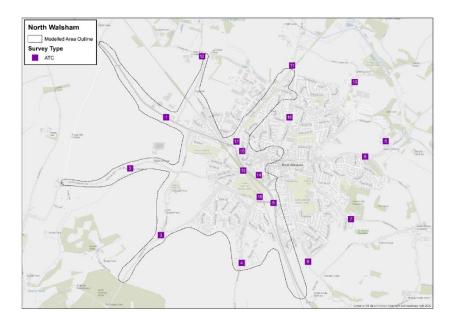


Figure 2-4 – Link counts (Automatic Traffic Counts)

Camera Footage

2.17 Camera footage, which was recorded to produce the MCTC and ANPR data, was obtained to provide the modellers with a more detailed view of the driving behaviour in the area and allow for saturation flow measurements.

3. Data Review and Analysis

Consistency Review

- 3.1 The locations of MCTCs have been labelled approach arms and model entry points to assist with the analysis of the data consistency review and can be found in Appendix A.
- 3.2 The consistency between the different data sets was assessed to understand the reliability of the data and identify any discrepancy that could affect the model development. The key comparisons and findings found during the data analysis have been summarised below. The full details of the consistency checks undertaken can be found in Appendix A.
- 3.3 As a result of consistency checks, it was necessary to include six additional synthetic zones in the model, to balance the flow differences identified between adjacent junctions.
- 3.4 The synthetic zones identified during the survey data analysis represent minor junctions that were not surveyed during the data collection exercise. These junctions are located between surveyed junctions which were calibrated against observed counts. This is the standard modelling approach to infill volumes between surveyed junctions arising due to minor side roads, parking lots etc.
- 3.5 Additional MCTC surveys were carried out on 10th of November 2022 to compare the traffic flows against July 2022 data. The analysis showed a close match between the MCTC data of July and November 2022.

Peak Hour Analysis

- 3.6 The survey data available was processed to identify the morning and evening peak hours by analysing the profile of traffic volumes during the surveyed period. For this calculation, all vehicle movements have been considered as well as calculations of the inbound flows to the model area.
- 3.7 MCTC and ATC/ MCC data were analysed to determine the peak hour, by totalling all movements and by totalling only entries in the model area. In the AM period, the peak hour was calculated to be 08.00-09.00, both when considering entries into the modelled area and when using all available data. In the PM period calculations similarly returned a consistent peak hour of 16.30-17.30 using both methods. The ATC/MCC data was also analysed and showed the same peak hours as the analysis of the MCTC data.
- 3.8 Figure 2-4 shows the profile of the rolling hour calculated from the ATC data, which was used for calculating the peak hour.

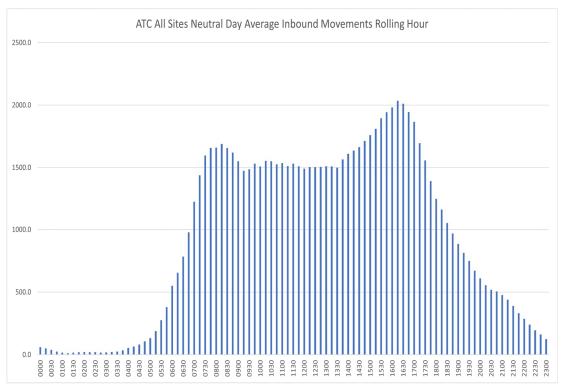


Figure 3-1 - ATC Peak Hour Analysis

3.9 This analysis has identified the following peak hours:

AM peak hour: 08:00 - 09:00; and

PM peak hour: 16:30 - 17:30

3.10 The modelled simulation periods include a 30-minute warm-up period to fully saturate the network before the simulated peak hour and a 15-minute cool-down period to allow vehicles to complete their journeys. The modelled periods are, therefore:

AM modelled period: 07:30 - 09:15; and

PM modelled period: 16:00 - 17:45.

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4. Demand Development

Overview

- 4.1 This section describes the demand methodology and the routing analysis undertaken to develop and calibrate the traffic demand in the Vissim Base model.
- 4.2 The model was developed using the dynamic assignment module, as it would allow the model to predict future changes in routing which result from the demand growth, committed schemes or proposed mitigation measures in the area.
- 4.3 The ANPR data was used to develop the prior demand, which was then adjusted using the MCTC data to calibrate the demand to individual junction turning flows, resulting in the hourly Origin Destination (OD) matrices used in the Vissim model.
- 4.4 The traffic demand has been calculated for each vehicle type included in the model (Car, Light Goods Vehicle (LGV) and Heavy Goods Vehicle (HGV)) for the modelled peak hours. The available survey data has been used to develop the hourly Origin-destination matrices and the 15-minute profiles for each origin zone.

Demand Development

- 4.5 ANPR captures number plates at each of the camera locations providing a trip chain report documenting when and where the number plate was captured. This information has been used to develop demand matrices for the Vissim model.
- 4.6 The ANPR data has been factored up to represent all the vehicles in the network, by expanding the matched vehicles based on the capture rate at each ANPR site. However, the capture rates are not consistent between all the cameras, resulting in small discrepancies between these ANPR demand matrices and the MCTC data.
- 4.7 To minimise these discrepancies and refine the modelled demand, the ANPR matrix has been manually adjusted to match the MCTC data, allowing for a closer representation of the MCTC counts demand in the area while maintaining a direct correspondence between the VISSIM demand and the original ANPR data, preserving the observed routing data. The process followed is outlined in Figure 4-1.

Manual **VISSIM**

New Zones

Initial Matrix

Define zone Correspondence between the ANPR cameras and the Model zones.

ANPR Matrix

2. Uplift the demand matrices per origin according to their capture rate

1. Furness the ANPR matrix to match the trip end target from the Link Counts (ATC and Manual Counts)

Prior Matrix

- 1. Identify zones not captured by the ANPR cordon and add them to the matrix.
- 2. Identify a suitable parent zone from which to copy the destination distribution.
- 3. Combine the trip distribution from the parent zone with the MCTC data to generate the New Zone Matrices

Analyse the turning count comparison between the MCTC and Initial Matrix to identify the manual adjustments required

Adjustment

Matrices

- 2. Combine all the manual adjustments in a matrix format to form the Manual Adjustment Matrices
- Final Vissim matrix is the sum of the prior matrix and the adjustment matrix.

Demand

Figure 4-1 – Demand Development Methodology

- 4.8 To ensure the best possible correlation between the observed data and the Vissim model demand, the vehicle inputs and origin/destination routing have been developed by combining three different components:
 - Initial Matrix reflecting the routing patterns in the ANPR matrix and the link counts at entries and exits
 of the model;
 - New Zones Matrix additional zones required in Vissim but not directly captured by the ANPR; and
 - Manual Adjustment Matrix adjustments required to address routing and discrepancies between the Initial Matrix and MCTC data.
- 4.9 The process outline below was followed:
 - The ANPR cameras and the Vissim model zones have been consistently referenced to define a correspondence between them e.g., Camera 5 is representative of Zone 5. The OD matrix extracted from the ANPR data has then been uplifted to reflect the number of vehicles at each origin, since the ANPR capture rate is less than 100%.
 - The imperfect capture rate, with different number plates missed at each camera, means that the resulting
 matrix requires uplifting to outbound observed flows. The entry and exit link counts were used to furness
 the matrix. The last iteration has been set up to match the origin trip ends, to ensure that the demand
 matrix represents the traffic volumes entering the model area. This process results in an hourly OD
 matrix for each vehicle type: Cars, HGVs, Taxis, and LGVs.
 - Once the matrix derived from ANPR and link counts was in a usable OD matrix format, the entries to the
 model where ANPR data is unavailable were reviewed. The total origin and destination demand for each
 additional zone was derived from the differences between adjacent turning counts and the trip
 distribution was assumed to be the same as another zone with similar characteristics. In this way, a New
 Zones Matrix was developed, which will infill the Initial Matrix to include zones not covered by ANPR
 cameras.
 - The Initial matrix and the New Zones Matrix were combined and assigned in Vissim the modelled turning flows and observed turning counts were compared to identify manual adjustments required to meet the flow calibration criteria. This was an iterative process, and several adjustments were needed before adequate match between observed and modelled turning counts was achieved.
 - The manual adjustments identified from the comparison between the modelled and observed turning flows are implemented in a separate Manual Adjustments Matrix for each vehicle class; this is then combined with the Initial Matrix and New Zones Matrix developed previously to obtain the final Vissim demand.

Convergence and routing analysis

- 4.10 The Vissim dynamic assignment module assigns the vehicles on the different paths based on the journey time cost and distance, assigning most of the vehicles to the shorter or faster paths, depending on the convergence parameters.
- 4.11 The journey time and routing data obtained from the ANPR was used to analyse the routing patterns in the model area and calculate the parameters required to support the convergence process.
- 4.12 The results of the convergence process and dynamic assignment were then checked against the routing information obtained from the ANPR data to ensure the model provides a suitable representation of the routing patterns in the area for the OD pairs with multiple route choice.
- 4.13 An example of the routing checks is shown in Figure 4-2 below, for two possible routes between Zone 1 and Zone 4 in both directions. The routing analysis compared the flows along each route against the observed data from ANPR surveys. This analysis provided further reassurance that the observed routing patterns were replicated in the model for the main OD pairs with multiple route options.
- 4.14 It should be noted that these routing checks were undertaken to identify and address any potential routing issues in the assignment that may affect the operation of the model. However, these checks are not part of the TAG validation criteria required for microsimulation models.

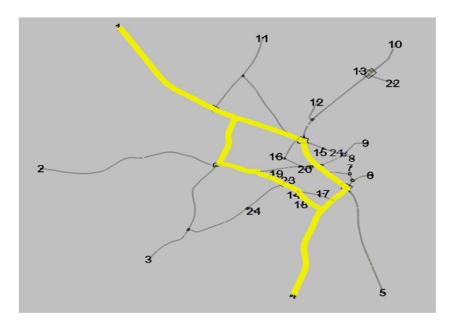


Figure 4-2 - VISSIM Dynamic Assignment with Two Possible Routes

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5. Network Development

Network coding

- 5.1 Scaled Bing maps within Vissim have been used to code the network geometry and structure, such as number of lanes and flare lengths. Reference was also made to Google Maps and Street view to ensure the network reflects conditions on the ground.
- 5.2 Observation from the video footage available have also been used to inform the network coding and replicate the operation of the existing layout.

Desired Speed Decisions & Reduced Speed Areas

- 5.3 Desired Speed Decisions, defining the speed distribution that vehicles follow at each point of the network, have been updated to represent the posted speed limits for each link. Reduced Speed Areas have been included to replicate driving behaviours such as bends curves, narrow road sections or pedestrian crossings, but also, to calibrate saturation flows and replicate behaviour at signalised junctions.
- 5.4 The speed distributions used in the model have been obtained from two different sources. The Guidelines for the Use of Microsimulation Software from National Highways provide distributions for 50 mph and 70 mph, while 30 mph and 60 mph have been obtained from the SPE0111 Vehicle Speed Compliance by road type and vehicle type in Great Britain from Department for Transport (DfT).
- 5.5 On some links, the speed limits do not provide a realistic representation of the average speeds. For example, Bradfield Road is a country lane with the national speed limit of 60 mph, However, the average speed for a narrow unlit road is significantly lower according to the ANPR data. The speed limits coded on such links have been derived from observed ANPR data.
- 5.6 Similar behaviour has been observed in Tungate Road and Skeyton Road, where the journey time data suggests that vehicles travel at lower speeds. A 30 mph speed limit has been coded on Tungate Road since this is a single-track road, and vehicles will slow down at narrow sections or when a vehicle in the opposite direction approaches. Due to the unpredictable/ variable behaviour along these links, and fact that vehicle may need to pass each other/ stop at any point along the link, this can only be replicated by Reduced Speed Areas (RSAs) representing average delay along the link.
- 5.7 Closer to the town centre on the section of Aylsham Road between Cherry Tree Lane and Station Road the road narrows with residential property walls and fences at either side of the road. A lower speed limit (15mph) was introduced in the model to represent the observed behaviour along this section, where vehicles slow-down below the speed limit (20 mph).

Route Closures

- 5.8 The routing analysis undertaken during the convergence and assignment was also used to identify certain routes with negligible traffic flows. These routes have been removed from the model to avoid rat-running and improve the model stability.
- 5.9 The following route closures were implemented in the model to prohibit certain routes which are not practical, due to the conditions of the roads, and this was confirmed by ANPR and MCTC data:
 - A route closure has been coded on Skeyton Road, banning the through movement from the south, so
 the road is only used for access to and from Zone 24 (Brookes Drive). This assumption was supported
 by the ANPR and MCTC data in the area showing less than 15 vehicles per hour along this route in both
 directions:
 - Secondly, a route closure was applied to avoid vehicles accessing Cromer Road to and from Cherry Tree Lane, as the road is narrow and on-street parking makes this route highly unattractive; and,
 - A route closure was also added to Bradfield Road allowing vehicles to only use Cromer Road for Eastbound and Westbound movements.

Priority Rules and Conflict Areas

- 5.10 Priority Rules and Conflict Areas have been coded and calibrated based on observed network conditions and driving behaviour at roundabouts, priority junctions and other give way situations.
- 5.11 Priority Rules have also been used to replicate specific behaviours such as the operation of the underpass on Aylsham Road shown in Figure 5-1 where large vehicles use the centre of the road to go through the underpass due to the height of the bridge.



Figure 5-1 – Eastbound Road view on Aylsham Road at A149 underpass

- 5.12 In addition to the underpass on Aylsham Road there are height restrictions in place for HGVs at the B1150 Norwich Road and A149 Cromer Road. The traffic data collected at the nearby junctions suggests that the constraints created by the height restrictions do not affect all the HGVs as the data and the video footage shows OGV1 and OGV2 going through the underpass.
- 5.13 The Vissim model has been calibrated to match the number of Cars, LGVs and HGVs observed in the area. However, vehicle classification used to develop the Vissim demand (DfT vehicle classification) which defines the vehicle characteristics, such as vehicle length, acceleration or speed profile does not include any reference to vehicle height as this parameter is not linked to the vehicle type.



Figure 5-2 - Height restriction on N Walsham Rd

Buses

5.14 All bus services in the model were coded based on information available online. For all bus stops in the model a standard dwell time of 20 seconds was assumed.

Signal Information

- 5.15 The signalised junctions included in the model area have the capability to operate on MOVA (Microprocessor Optimised Vehicle Actuation). However, MOVA logs, and operational files were not collected on the day of the surveys, so it was not possible to model this operation explicitly in the model. This requires use of PCMOVA, an add-on to Vissim, which adds additional time/cost to the model development and increases run-times, so this is typically only used in complex strategic junctions where it is proportionate.
- 5.16 The signal data provided by Norfolk County Council (NCC), including the specification of the existing controller, and the average green times at the junction were used to develop a variable signal logic file included in the model using VisVAP. The Vehicle Actuated (VA) signal operation allows the model to extend or reduce the green time allocated to each arm of the junction depending on the traffic demand, which is monitored through detectors (representing loops in the road).
- 5.17 The minimum and maximum green times as well as signal patterns defining the priority of each arm have been calibrated to observed signal operation and signal information, to provide a realistic approximation of the operation of MOVA.

Differences between AM and PM Networks

5.18 Some elements of the models are expected to be different in different time periods. The demand, routing, and signal controllers represent the different flow patterns/ routeing and signal timings in the AM and the PM model. However, there are no differences between AM and PM networks to report.

6. Model Calibration

Introduction

6.1 The purpose of the model calibration process is to ensure that the model represents existing traffic conditions. Calibration is an iterative process in which the model is revised to replicate observed traffic volumes, traffic conditions and vehicle behaviour as closely as possible.

Saturation Flow Calibration

- 6.2 The saturation flow is the maximum number of vehicles that are able to pass across a lane at a signal stopline in an hour.
- 6.3 The modelled saturation flows on each signalized stop line have been compared to estimated saturation flows calculated using the RR67 formula. The measurements required for the RR67 formula (lane-width, radius, etc.) have been measured using Google Maps.
- 6.4 The modelled saturation flows were extracted from Vissim using a saturation flow script developed by AECOM. Modelled values have been compared to the RR67 values to ensure that they are within an acceptable range. The saturation flow results have been presented, below in Table 6-1.

Table 6-1 - Saturation Flows

Junction	Approach	Modelled	RR67	Difference
	Mundesley Road	1761.25	1865	-6%
Cromer Road / Aylsham Road	Aylsham Road	1761.25	1865	-6%
	Cromer Road	1761.25	1915	-8%
	A149 Northbound	1731.16	1808	-4%
	A149 Northbound	1818.8	1915	-5%
Cromer Road / B1150 / A149	B1150 Southbound	1979.0	1915	3%
Cromer Road / 61150 / A149	B1150 Southbound	1717.74	1808	-5%
	Cromer Road	1672.69	1785	-6%
	Cromer Road	1717.74	1808	-5%
	A149 Southbound	1781.58	1915	-7%
	A149 Northbound	1780.27	1915	-7%
A149 / Norwich Road / Grammar School Road	A149 Southbound	1723.09	1808	-5%
A1497 NOIWICH ROAU / GIAIIIIIIAI SCHOOL ROAU	Norwich Road	1720.85	1783	-3%
	A149 Northbound	1727.75	1808	-4%
	Norwich Road	1935.75	1859	4%

Flow Calibration Criteria

- 6.5 This section presents the traffic flow calibration which was undertaken and compares modelled and observed traffic flows using the criteria provided in TAG Unit M3-1.
- 6.6 The observed and modelled turning flows were compared for each of the junctions for the AM and PM peak hours, using the TAG criteria (Unit M3.1) for flow calibration as shown in Table 6-2.

Table 6-2 - TAG Calibration Criteria

Туре	Criteria	Acceptability Guidelines
1 - % Flows	 a. Individual flows within 15% for flows 700-2700 vph b. Individual flows within 100 vph for flows < 700 vph C. Individual flows within 400 vph for flows > 2700 vph 	> 85% of all cases
2 – GEH Criteria	GEH Statistic - Individual flows: GEH < 5	

- 6.7 The differences between modelled and observed flows were calculated and the TAG criteria, both for absolute differences and for GEH statistic, were used to determine if these differences were acceptable. The GEH statistic incorporates both relative and the absolute differences and provides a better indication of the significance of differences, compared to using percentage differences which can be misleading.
- 6.8 The GEH statistic is defined as:

GEH=
$$\sqrt{\frac{(M-C)^2}{(M+C)/2}}$$
, where M and C are different datasets to be compared.

Flow Calibration Results

- 6.9 The modelled turning flows were compared against the surveyed turning flows to calibrate the demand inputs and model assignment. The models were run twenty times using different random seeds to produce a set of average turning count results for comparison with the survey data.
- 6.10 The AM calibration results in Table 5-3 show the calibration results for each vehicle type. The results demonstrate that the AM peak hour flows are also calibrated closely against the observed turning counts when analysed vehicle class, and all exceed the thresholds set out in TAG. The structure of the junctions and turning count references included in the AM calibration results can be found in Appendix B.

Table 6-3 - AM Calibration Results - Peak Hour by Vehicle Class

Vehicle Class	Tag Criteria	Within	Total Counts	Percentage Passing
Car	% Counts within GEH <5	150	151	99%
	% Flows within Individual Flow	151	151	100%
HGV	% Counts within GEH <5	151	151	100%
	% Flows within Individual Flow	151	151	100%
LGV	% Counts within GEH <5	151	151	100%
	% Flows within Individual Flow	151	151	100%
Total	% Counts within GEH <5	145	151	96%
	% Flows within Individual Flow	150	151	99%

- 6.11 The AM calibration results in Table 5.4 shows the calibration results for total vehicles entering the model. Although not required in TAG, explicitly matching the observed number of vehicles entering the network is a key metric to validate the capacity and delays of the microsimulation models.
- 6.12 The results demonstrate that modelled flows at all entries to the model are calibrated closely with observed data as all the inputs are below GEH 5 as required in TAG guidance.

Table 6-4 - AM Calibration results - Model Entries

Entry Road	Observed	Modelled	GEH
Bradfield Road Joining Cromer Road	7	2	2.36
Cromer Road Eastbound	346	344	0.11
Mundesley Road Southbound	136	135	0.09
Market Street Westbound	0	0	0.00
Tungate Road Northbound	46	42	0.60
Aylsham Road Eastbound	166	155	0.87
Skeyton Road Eastbound	92	92	0.00
Morris Road Eastbound	73	82	1.02
Norwich Road Northbound	428	419	0.44
North Walsham Bypass Northbound	325	320	0.28
Grammar School Road Westbound	555	551	0.17
Laundry Loke Eastbound	69	71	0.24
Lyngate Road North	225	241	1.05
Lyngate Road West	320	272	2.79
Folgate Road	47	48	0.15
Total	2835	2777	1.09

6.13 The calibration summary in Table 6-5 demonstrates that the PM peak hour model flows are also closely calibrated against the observed turning counts when analysed by vehicle class, exceeding the requirements set out in TAG. The structure of the junctions and turning counts references included in the PM calibration results can be found in Appendix B.

Table 6-5 - PM Calibration Results - Peak Hour by Vehicle Class

Vehicle Class	Tag Criteria	Within	Total Counts	Percentage Passing
Cars	% Counts within GEH <5	151	151	100%
	% Flows within Individual Flow	151	151	100%
HGVs	% Counts within GEH <5	151	151	100%
11010	% Flows within Individual Flow	151	151	100%
LGVs	% Counts within GEH <5	150	151	99%
	% Flows within Individual Flow	151	151	100%
Total	% Counts within GEH <5	148	151	98%
	% Flows within Individual Flow	151	151	100%

6.14 The PM calibration results in Table 5.6 shows the calibration results for total vehicles entering the model. The results demonstrate that the total entry volumes into the model are calibrated closely with observed data.

Table 6-6 - PM Calibration Results - Model Entries

Junction	Observed	Modelled	GEH
Bradfield Road Joining Cromer Road	5	7	0.82
Cromer Road Eastbound	552	542	0.43
Mundesley Road Southbound	135	143	0.68
Market Street Westbound	0	0	0.00
Tungate Road Northbound	55	46	1.27
Aylsham Road Eastbound	155	147	0.65
Skeyton Road Eastbound	58	54	0.53
Morris Road Eastbound	12	15	0.82
Norwich Road Northbound	537	521	0.70
North Walsham Bypass Northbound	376	373	0.16
Grammar School Road Westbound	530	522	0.35
Laundry Loke Eastbound	167	158	0.71
Lyngate Road Southbound	232	235	0.20
Lyngate Road Westbound	232	235	0.20
Folgate Road	184	188	0.29
Total	3169	3116	0.95

6.15 A flow diagram was constructed to visualise the junctions/ network and show turning flows within the model. The flow diagrams, showing calibration of flows for all turning movements in the AM and PM, can be found in Appendix C.

Calibration Parameters

6.16 Table 6-7 summarises the main calibration and specific driving behaviour parameters recommended by TAG and DfT for microsimulation models. These parameters have been included in the North Walsham VISSIM model in line with the recommended guidance.

Table 6-7 - Microsimulation Model Parameters - TAG/DfT

Parameter	Value	Following Guidance	
Headway	1s time	Yes	
Gap	1 to 4 seconds, depends on location	Yes	
Vehicle Dynamics	Following graphs	Yes	
Reaction Time	-	-	
Desired Speed Distributions	Following graphs	Yes	
Driver Awareness	Following graphs	Yes	
Influence of signing on the approach to a diverge of the motorway lane selection	5	Yes	
	Yes, used on merging and weaving links		
Cooperative Merging	Maximum speed difference - 6.71mph	Yes	
	Maximum collision time – 10s		
Implied Capacity at roundabouts and signal stop lines	-	-	
Min Distance between vehicles at a standstill	1.5m	Yes	

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7. Model Validation

Introduction

- 7.1 Following the model calibration process, the VISSIM models were validated using journey time data. The vehicle travel time results from the models were compared against the surveyed journey time data to validate the queuing and delay in the model. The models were run twenty times using different random seeds to produce a set of average journey time results for comparison with the survey data.
- 7.2 The TAG M3-1 criteria for journey time validation are shown in Table 7-1 below.

Table 7-1 - TAG Validation Criteria

Criteria

Acceptability
Guidelines

Modelled times along routes should be within 15% of surveyed times (or 1
minute, if higher than 15%)

> 85% of routes

Journey Time Validation Results

7.3 Figure 7-1 shows the nine journey time routes which have been defined within the model area. The average observed journey times were compared to the average modelled journey times in accordance with the criteria set out in TAG M3-1. The journey times routes were defined using the camera position of the ANPR surveys used to capture the observed journey time data.

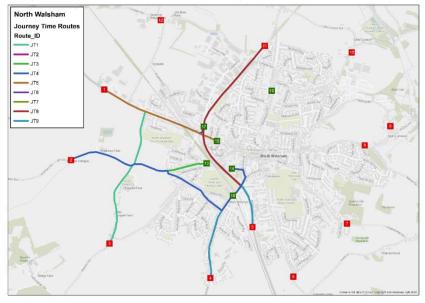


Figure 7-1 – Journey Time Routes

- 7.4 The definition of these journey times routes has been carried out using the position of the ANPR cameras used to capture the observed journey time data. The inner cameras have also been used split the longer routes into sections, so the profile of delays along the routes can be replicated to make sure the main capacity constraints in the area are validated.
- 7.5 Tables 6-2 and 6-3 show the individual performance of each of the defined journey time routes for all vehicles, all of which pass the TAG criteria. For ease, the routes are identified as JT 1 to 9 in the following paragraphs.

Table 7-2 – AM Journey Time Validation

ID	Route Name	Observed	Modelled	% Difference	Validation
1	JT1_EB	183	173	-6%	Yes
2	JT1_WB	167	174	4%	Yes
3	JT2_NB	178	186	5%	Yes
4	JT2_SB	173	168	-3%	Yes
5	JT3_EB	105	109	4%	Yes
6	JT3_WB	129	135	4%	Yes
7	JT4_EB	340	309	-9%	Yes
8	JT4_WB	258	251	-3%	Yes
9	JT5_EB	142	134	-6%	Yes
10	JT5_WB	146	142	-3%	Yes
11	JT6_NB	158	171	8%	Yes
12	JT6_SB	176	175	0%	Yes
13	JT7_NB	222	214	-4%	Yes
14	JT7_SB	94	89	-5%	Yes
15	JT8_NB	291	303	4%	Yes
16	JT8_SB	264	255	-3%	Yes
17	JT9_EB	211	194	-8%	Yes
18	JT9_WB	160	156	-2%	Yes

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Table 7-3 - PM Journey Time Validation

ID	Route Name	Observed	Modelled	% Difference	Validation
1	JT1_EB	204	176	-14%	Yes
2	JT1_WB	180	180	0%	Yes
3	JT2_NB	192	198	3%	Yes
4	JT2_SB	207	206	0%	Yes
5	JT3_EB	104	104	0%	Yes
6	JT3_WB	134	130	-3%	Yes
7	JT4_EB	364	342	-6%	Yes
8	JT4_WB	267	256	-4%	Yes
9	JT5_EB	155	151	-3%	Yes
10	JT5_WB	150	149	0%	Yes
11	JT6_NB	189	186	-1%	Yes
12	JT6_SB	192	184	-4%	Yes
13	JT7_NB	274	244	-11%	Yes
14	JT7_SB	96	94	-2%	Yes
15	JT8_NB	362	349	-4%	Yes
16	JT8_SB	294	295	0%	Yes
17	JT9_EB	265	226	-14.5%	Yes
18	JT9_WB	173	160	-8%	Yes

7.6 The detailed journey time comparisons through the key parts of the model have been extracted and compared against the observed data in the sections below Figure 7-2 to Figure 7-10, showing that the model provides an accurate representation of the journey time and delays along the routes. The comparison of all the journey time routes included in the model routes can be found in Appendix D.

JT1

7.7 JT1 runs from Zone 1 – Cromer Road South to Zone 3 – Skeyton Road, as shown in Figure 7-2. This route is considered important as this is the region of the proposed development. This route shows that the lower speeds included in the models is aligned with the average speed obtained from the observed journey time data.

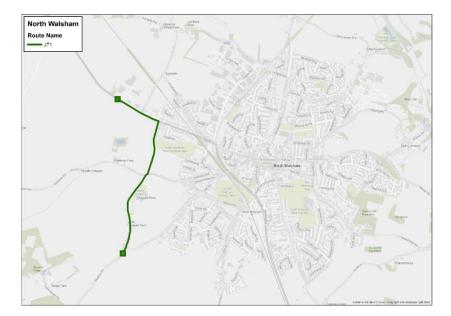


Figure 7-2 – JT1 Route Diagram

7.8 Figure 7-3 show the eastbound validation profile of this route with the observed data for both peaks.

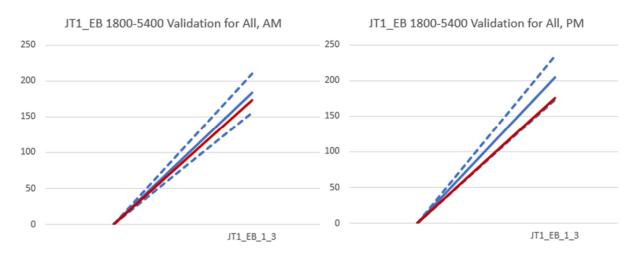


Figure 7-3 – JT1 Eastbound Journey Time Validation profile

7.9 Figure 7-4 show the westbound validation profile of this route with the observed data for both peaks.

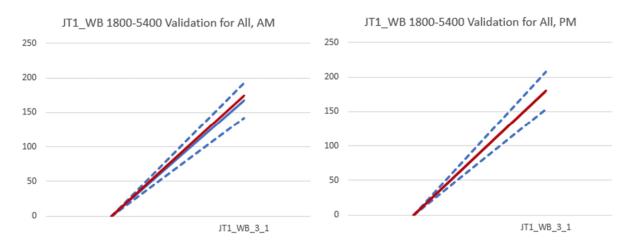


Figure 7-4 – JT1 Westbound Journey Time Validation profile

JT2

7.10 JT2 run from Zone 5 – North Walsham Bypass North to Zone 10 – North Walsham Bypass, as shown in Figure 5-5.



Figure 7-5 – JT 2 Route Diagram

7.11 Figure 7-6 show the northbound validation profile of this route with the observed data for both peaks.

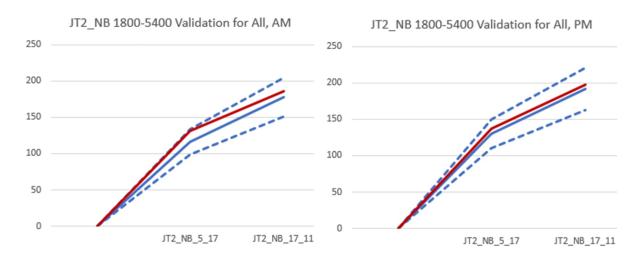


Figure 7-6 – JT2 Northbound Validation Profile

7.12 Figure 7-7 show the southbound validation profile of this route with the observed data for both peaks.

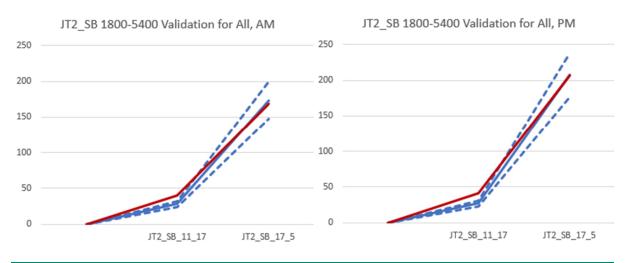


Figure 7-7 – JT2 Southbound Validation Profile

JT4

7.13 JT4 runs from Zone 2 Aylsham Road to Camera 14 Park Lane in the eastbound direction and from Zone 5 to Zone 2 in the westbound direction. This route has a different start/end point in the east as Park Lane is a one-way street.

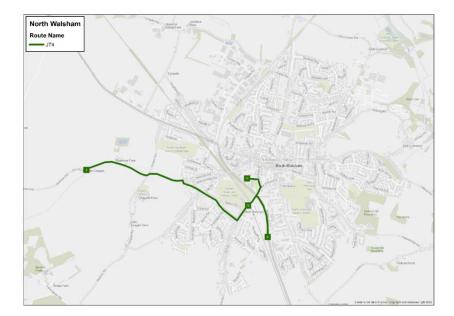


Figure 7-8 – JT4 Route Diagram

7.14 Figure 7-9 show the eastbound validation profile of this route with the observed data for both peaks.

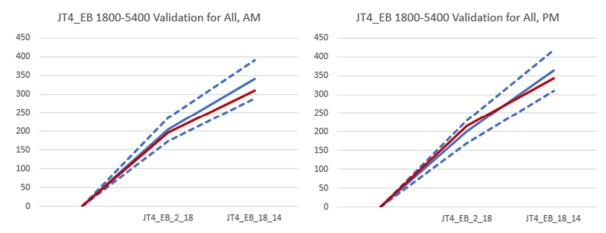


Figure 7-9 – JT4 Eastbound Validation Profile

7.15 Figure 7-10 show the westbound validation profile of this route with the observed data for both peaks.

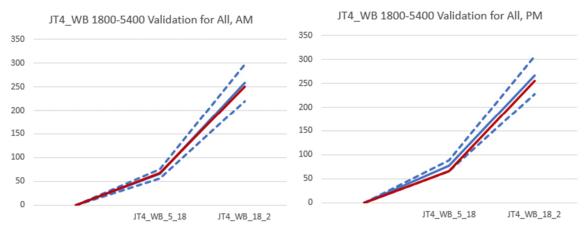


Figure 7-10 – JT4 Westbound Validation profile

Queue Comparison

- 7.16 In addition to the journey time validation of the model, TAG also recommends a review of the queues in the model and how these relate to existing queues. Although journey times provide a more accurate representation of the existing delays, the visual comparison of the queue patterns in the area provides further reassurance to support the model operation and results.
- 7.17 Two main sources have been used to understand the main queues in the model area: survey videos and live traffic information from Google Maps on the day the surveys took place.
- 7.18 The main queues in the AM peak hour are:
 - Queues approaching the signalised crossroads of the B1150 and A149; and
 - Queues approaching the signalised crossroad of Cromer Road and The North Walsham Bypass.
- 7.19 Figure 7-11 shows the typical traffic conditions from Google Maps, on a neutral weekday at 08:30.
- 7.20 Figure 7-12 below, shows a peak hour average speed plot extracted from the model at the same time. The comparison shows that the model provides a reasonable representation of the queuing patterns in the area.
- 7.21 It should be noted that the lower speeds along Millfield Road, Aylsham Road or Tungate Road shown on the average speed plots, result from lower speeds coded in the model to represent the impact of on-street parking or narrow roads.

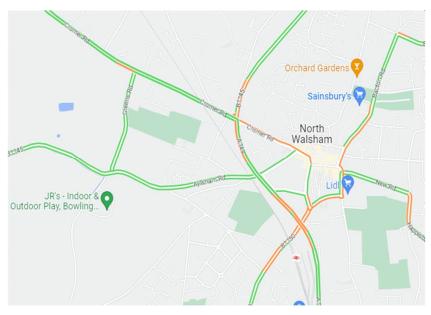


Figure 7-11 - Typical queues from Google Traffic on a Wednesday, 08:30

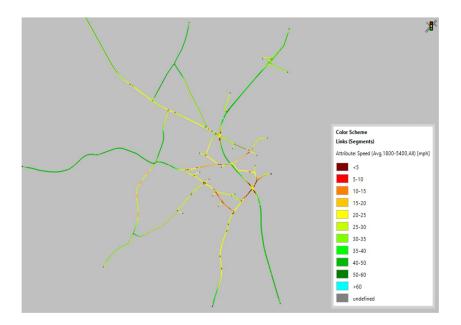


Figure 7-12 - AM Peak Hour Speed Plot

- 7.22 The main queues in PM peak are largely similar to those in the AM peak hour. These are:
 - Queues approaching the crossroads of the A149 and the B1150; and
 - Queues/ reduced speeds on Aylsham Road.

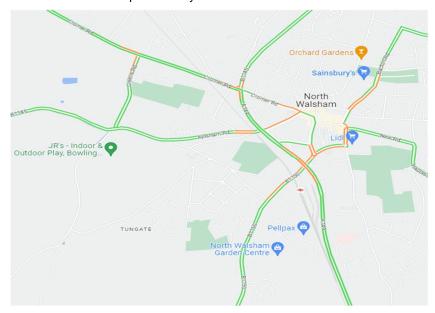


Figure 7-13 - Typical queues from Google Traffic on a Wednesday, 17:00

7.23 Figure 7-13 shows the typical traffic conditions from Google Maps, on a Wednesday at 17:00, and Figure 7-14 below, show the modelled queues during the PM peak. It can be observed that similar queueing patterns are replicated in the model.

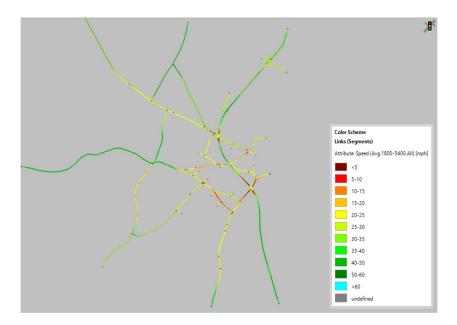


Figure 7-14 - PM Peak Hour Speed Plot

Model Variability

- 7.24 Microsimulation models are run several times with different random seeds to obtain a statistically representative result. This approach replicates daily variability, since each run has different arrival profiles which results in a different chain of events. A representative average of the results is the obtained/presented.
- 7.25 The observed data indicates there is limited variability in the network operation except for the signalised A149/B1150 junction. The queue along Norwich Road approaching this junction is generally long but varied in length, and often disperses every cycle, resulting in highly variable journey times along this section, depending on when the vehicles arrive at the junction.
- 7.26 This operation and the associated variability have been represented in the model. Figure 7-15 and 7-16 show the operation of the signalised junction on the A149 and Norwich Road in the VISSIM model.
- 7.27 The figures show how the queues along Norwich Road northbound build up to a significant length but are discharged fully every cycle. This operation is consistent with the observations from the video footage.

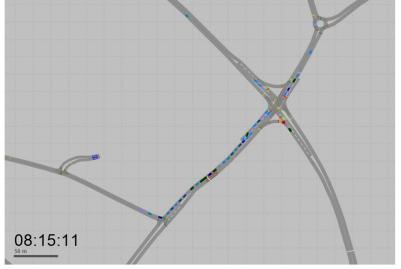


Figure 7-15 - A149/B1150 Junction - Norwich Road northbound green signal starts (AM)

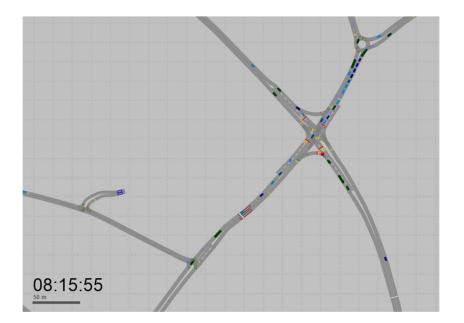


Figure 7-16 - A149/B1150 Junction - Norwich Road northbound green signal ends (AM)

7.28 Figure 7-17 shows the crossroads of the A149 and the B1150 in the VISSIM model at the moment that the green period begins for traffic from the B1150 at 16:42. While Figure 7-18 shows the same junction at the end of the green period. The two figures demonstrate how the queues in this direction build up significantly, but then disperse which is in accordance with observations from video footage.

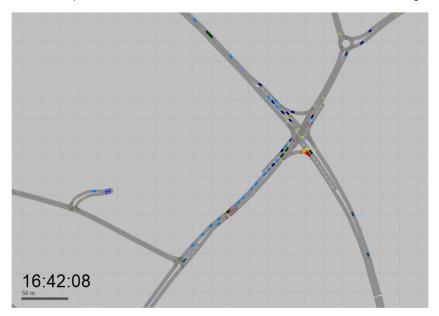


Figure 7-17 - A149/B1150 Junction - Norwich Road northbound green signal starts (PM)

Prepared for: AECOM

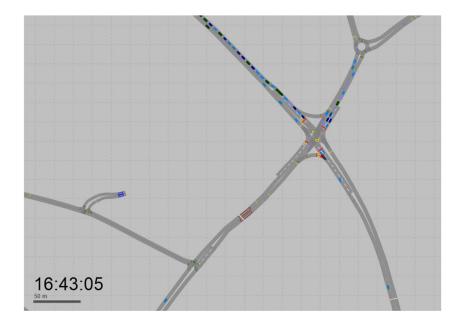


Figure 7-18 - A149/B1150 Junction - Norwich Road northbound green signal ends (PM)

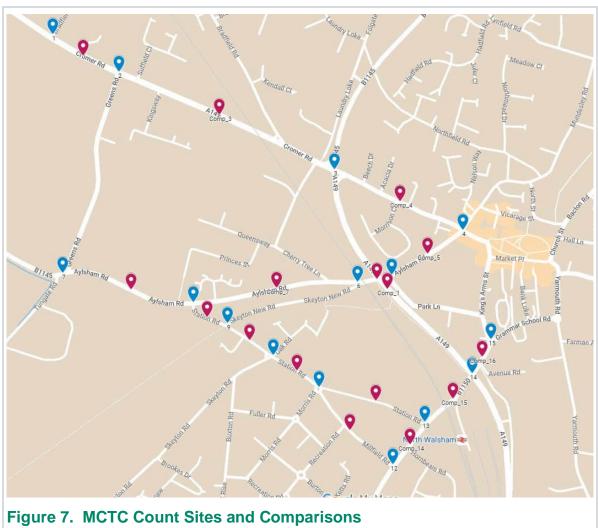
AECOM 32 Prepared for:

8. Conclusion

- 8.1 North Walsham is located on the east of England, north of Norwich. The town experiences some congestion around the signalised junctions and the town centre roads with queues often building up in these areas at AM and PM peak times. However, these queues are not too extensive with vehicles usually progressing through signals in a single cycle, with minimum impacts on nearby junctions.
- 8.2 The base models have been calibrated and validated against the observed traffic flow and journey time data in line with the required criteria set out in TAG and best practice. The calibration/validation results exceed the requirements for turning counts and journey times and the models are therefore closely aligned with observed data. The models also replicate observed queueing patterns and specific behaviours observed from video footage. The models are therefore validated to industry standard guidelines.
- 8.3 It is considered the base models provide a close representation of the queues and delays in the network, as well as the observed driving behaviour in the area, and are fit for the purpose of testing future traffic levels/ patterns or potential changes to the road network.

Prepared for: AECOM

Appendix A – Consistency Checks



				Difference			GE						ference			GE		
D	Site Exit			14/07/2022 AN			########					y 13/07/2022 14				#######		
Comp_1	14 B	3 C	4	12	8			1		14 B	3 C	16	-2	7		1	0	
	3 C	14 B	0	5	3			0		3 C	14 B	23	23	23	16	1	1	
Comp_2	1 C	2 A	11	4	8			0		1 C	2 A	3	1	2		0	0	
• • •	2 A	1 C	0	0	0			0		2 A	1 C	1	2	2		0	0	
Comp_3	2 C	3 B	56	34	45	5		2		2 C	3 B	30	57	44	4	1	3	
	3 B	2 C	3	-19	-8	2		1		3 B	2 C	-40	-21	-31	4	2	1	
Comp_4	3 D	4 B	-10	-12	-11	2		1			4 B	-11	-13	-12		1	1	
	4 B	3 D	11	15	13	6		5		4 B	3 D	5	17	11	6	3	6	
Comp_5	4 C	5 A	0	0	0		#DIV/0!	#DIV/0!	#DIV/0!	4 C	5 A	0	0	0		#DIV/0!	#DIV/0!	#DIV/
	5 A 5 B	4 C 6 A	-3	0	-2			0		5 A 5 B	4 C 6 A	-5	0	-2 1		0	0	
Comp_6			2	0	1			0				2	-		0	0		
Comp_7	6 A 6 B	5 B	0 5	9	0 7			0		6 A 6 B	5 B 8 A	-27	-1 -38	-1 -33	0	2	3	
	8 A	6 B	6	5	6			0		8 A	6 B	-21	-30	-ss -8		0	3	
Comp_8	7 D	8 B	-1	1	- 0			0		7 D	8 B	-2	-14	-0 -1	0	0	0	
	8 B	7 D	-1	0	0			0		8 B	7 D	1	-1	-1		0	0	
	8 C	9 B	1	0	1			0		8 C	9 B	3	2	3		0	0	
Comp_9	9 B	8 C	-2	2	0			0		9 B	8 C	0	-4	-2		0	0	
	a C	10 B	-3	1	-1			0		9 C	10 B	-2	-2	- <u>-2</u>		0	0	
omp_10	10 B	9 C	5	4	5			0		10 B	9 C	-1	4	2		0	0	
	10 D	11 A	-2		-5			1		10 D	11 A	-5	-1	-3		0	0	
comp_11	11 A	10 D	-8	2	-3	1		0		11 A	10 D	-11	6	-3		1	0	
	11 D	13 B	-8	1	-4	-		0			13 B	-19	9	-5		4	1	
comp_12	13 B	11 D	-19	-13	-16			2			11 D	-6	-17	-12		1	3	
	11 C	12 B	23	40	32			3			12 B	10	19	15		1	2	
Comp_13	12 B	11 C	-29	-30	-30			2		12 B	11 C	-32	-50	-41	2	2	4	
	12 A	13 C	31	22	27			1		12 A	13 C	10	12	11		0	1	
Comp_14	13 C	12 A	-9	4	-3			0		13 C	12 A	-23	-10	-17		1	0	
	13 A	14 C	2		3			0		13 A	14 C	48	14	31	33	2	1	
omp_15	14 C	13 A	5	-16	-6			1		14 C	13 A	2	-6	-2		0	0	
	14 A	15 B	-5	10	3			0		14 A	15 B	4	-7	- <u>-</u>		0	0	
omp_16	15 B	14 A	-7	11	2			1			14 A	4	-1	2		0	0	

Figure 8. MCTC Consistency Check

Appendix B - Calibration Results

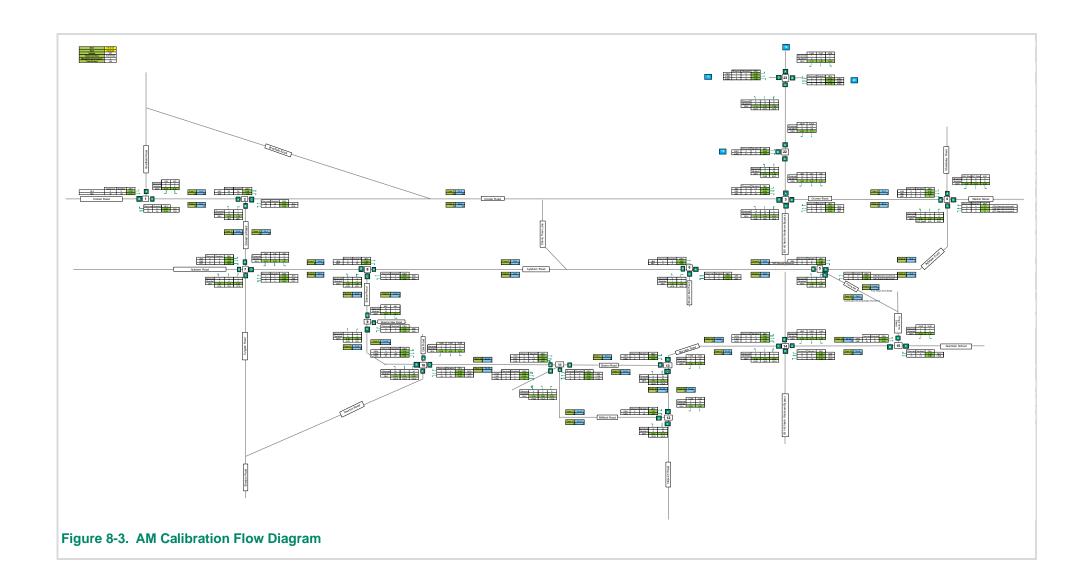
				ALL VEH		Cars	CAR	HGV	HGV	LGV LGV	
1AC 1AB 1BA	Junction From To 1 A C 1 A B 1 B A	Turn ID J1_A_C J1_A_B J1_B_A	Node 101 101 101	Observed Modelled 4 0 3 2 3 2	2.828 0.632 0.632	Observed Modell		Observe	ed Modelled GEH 0 0 0.000 0 0 0.000 0 0 0.000	Observed Modelled	0 2.000 1 0.000 0 1.414
1BC 1CB 1CA	1 B C 1 C B 1 C A	J1_B_C J1_C_B J1_C_A	101 101 101	346 342 537 470 8 4	0.197 3.004 1.509	406 4	253 0.085 357 2.511 4 0.129		33 34 0.164 33 30 0.498 0 0 0.000	56 5 88 8 4	0.033 0.601 0 2.828
2AC 2AB 2BA 2BC	2A C 2A B 2B A	J2_A_C J2_A_B J2_B_A J2_B_C	102 102 102	287 266 74 76 159 130 70 27	1.248 0.265 2.430 6.113	209 52 139 55	196 0.881 56 0.564 107 2.900 25 4.828		29 24 0.981 6 10 1.399 4 5 0.471 7 3 1.897	16 1 14 1	16 0.022 10 1.602 18 0.988 0 3.742
2CB 2CA 3AD	2C B 2C A 3 A D	J2_C_B J2_C_A J3_A_D	102 102 102 103 103	78 64 386 345 29 25	1.699 2.120 0.710	64 273 16	57 0.841 256 1.073 18 0.461		6 0 3.464 26 25 0.148 0 3 2.510	79 6 12	6 0.656 35 1.693 4 2.719
3AC 3AB 3BA 3BD	3A C 3A B 3B A	J3_A_C J3_A_B J3_B_A J3_B_D	103 103 103 103	265 245 174 159 124 89 92 52	1.275 1.182 3.418 4.727	206 135 99 72	197 0.641 123 1.097 62 4.130 38 4.631		15 15 0.051 15 17 0.500 9 17 2.160 2 2 0.000	21 1 15 1	0.097 0.401 0 1.399 12 0.660
3BC 3CB 3CA	3B C 3C B 3C A	J3_B_C J3_C_B J3_C_A	103 103 103	197 167 282 232 211 240	2.193 3.125 1.951	145 192 149	135 0.841 177 1.089 184 2.731		22 10 3.045 18 9 2.370 16 14 0.463	29 2 68 4 40 4	23 1.281 15 2.994 12 0.289
3CD 3DC 3DB 3DA	3 C D 3 D C 3 D B	J3_C_D J3_D_C J3_D_B J3_D_A	103 103 103	14 0 3 2 5 6 3 3	5.292 0.632 0.282 0.057	12 3 4 3	0 4.899 2 0.632 4 0.258 3 0.057		0 0 0.000 0 0 0.000 0 0 0.000	0	0 2.000 0 0.000 2 0.916 0 0.000
4AD 4BA 4BD	4 A D 4 B A 4 B D	J4_A_D J4_B_A J4_B_D	103 104 104 104	137 135 70 38 55 30	0.141 4.378 3.826	119 55 38	118 0.064 26 4.483 22 2.983		0 0 0.000 0 3 2.530 3 4 0.485	17 1	0.000 17 0.012 8 1.179 4 1.423
4CA 4CD 5BA 5CB	4 C A 4 C D 5 B A	J4_C_A J4_C_D J5_B_A	104 104 105	224 243 120 120 195 135 208 158	1.240 0.046 4.641	193 93 156 168	211 1.249 102 0.936 122 2.875 143 2.013		2 3 0.772 3 0 2.449 3 0 2.449 3 1 1.596	22 1	17 1.093 13 2.084
5CA 6AC 6AB	5 C A 6 A C 6 A B	J5_C_B J5_C_A J6_A_C J6_A_B	105 105 106 106	152 228 46 42 164 115	3.716 5.497 0.680 4.135	131 37 131	192 4.768 41 0.562 102 2.682		1 3 1.543 1 0 1.414 2 0 2.000	19 3 4	
6BA 6BC 6CB	6B A 6B C 6C B	J6_B_A J6_B_C J6_C_B	106 106 106	179 126 6 2 7 3	4.252 1.907 1.789	4	113 2.881 0 2.828 2 1.155		2 0 2.000 0 0 0.000 0 1 1.414	2	2 0.104 0 0.000
6CA 7AD 7AC 7AB	7A D 7A C 7A B	J6_C_A J7_A_D J7_A_C J7_A_B	106 107 107 107	16 0 76 70 21 25 56 45	5.657 0.660 0.844 1.526	10 58 17 42	0 4.472 50 1.053 25 1.756 39 0.511		1 0 1.414 5 10 1.811 2 0 2.000 5 0 3.162	13 1 2	0 0.000 10 0.838 0 2.000 6 0.937
7BA 7BD 7BC	7B A 7B D 7B C	J7_B_A J7_B_D J7_B_C	107 107 107	62 30 109 126 0 0	4.796 1.551 0.000	48 90 0	27 3.485 107 1.684 0 0.000		6 3 1.497 2 6 1.924 0 0 0.000	8 12 1 0	0 4.000 13 0.366 0 0.000
7CB 7CA 7CD 7DC	7C B 7C A 7C D	J7_C_B J7_C_A J7_C_D J7_D_C	107 107 107 107	4 4 22 5 22 34 18 13	0.076 4.663 2.183 1.229	4 16 17	4 0.076 5 3.434 27 2.141 12 0.043		0 0 0.000 3 0 2.449 1 4 2.090 2 0 2.000	2 3	0 0.000 0 2.000 2 0.632 1 0.816
7DB 7DA 8AC	7D B 7D A 8A C	J7_D_B J7_D_A J8_A_C	107 107 108	128 129 146 124 35 13	0.119 1.893 4.416	96 128 27	105 0.854 101 2.503 11 3.629		2 3 0.487 2 5 1.561 3 2 0.530	26 2 13 1 4	0.806 18 1.247 0 2.828
8AB 8BA 8BC 8CB	8 A B 8 B A 8 B C	J8_A_B J8_B_A J8_B_C J8_C_B	108 108 108 108	141 91 101 77 105 153 151 176	4.627 2.572 4.194 1.989	114 79 85 123	78 3.641 63 1.868 120 3.466 141 1.541		0 0 0.000 2 5 1.645 6 15 2.826 5 8 1.089	16 12 1	13 1.981 8 2.176 17 1.385 28 1.633
9AC 9AB	8C A 9A C 9A B	J8_C_A J9_A_C J9_A_B	108 109 109	78 38 51 45 2 2	5.191 0.873 0.000	69 46 1	32 5.148 41 0.766 0 1.414		2 0 2.000 1 1 0.000 0 0 0.000	5 4 1	6 0.447 3 0.535 2 0.816
9BA 9BC 9CB 9CA	9B A 9B C 9C B	J9_B_A J9_B_C J9_C_B J9_C_A	109 109 109 109	2 5 139 161 229 213 16 10	1.645 1.784 1.049 1.711	0 112 193 14	4 2.775 127 1.412 174 1.425 10 1.202		1 1 0.236 8 16 2.357 7 8 0.276 0 0 0.000	16 1 24 3	0 0.000 17 0.295 32 1.503 0 0.000
10AD 10AC 10AB	10 A D 10 A C 10 A B	J10_A_D J10_A_C J10_A_B	110 110 110	4 1 1 0 4 2	1.897 1.414 1.155	1 0 3	0 1.414 0 0.000 0 2.449		0 0 0.000 0 0 0.000 0 0 0.000	3 0 0	1 1.414 0 0.000 2 2.000
10BA 10BD 10BC 10CB	10 B A 10 B D 10 B C	J10_B_A J10_B_D J10_B_C J10_C_B	110 110 110 110	2 0 133 165 52 41 55 64	2.000 2.618 1.660 1.142	1 109 44 48	0 1.414 131 2.047 37 1.116 53 0.690		0 0 0.000 9 17 2.266 0 0 0.000 0 0 0.000	15 1 5	0 1.414 16 0.329 4 0.572 11 1.686
10CA 10CD 10DC	10 C B 10 C A 10 C D 10 D C	J10_C_A J10_C_D J10_D_C	110 110 110 110	3 0 41 28 33 38	2.449 2.251 0.839	0 33 31	0 0.000 28 0.943 37 0.980		0 0 0.000 0 0 0.000 0 0 0.000	0 5	0 0.000 0 3.162 1 0.280
10DB 10DA 11AD 11AC	10 D B 10 D A 11 A D	J10_D_B J10_D_A J11_A_D J11_A_C	110 110 111 111	181 158 5 15 34 25 129 142	1.790 3.198 1.627 1.117	151 2 30 102	131 1.684 14 4.198 25 0.924 110 0.777		7 8 0.258 0 0 0.000 0 0 0.000 9 14 1.592	2 2	19 0.232 1 0.502 0 2.000 18 0.107
11AB 11AA 11BA	11 A B 11 A A 11 B A	J11_A_B J11_A_A J11_B_A	111 111 111	12 14 1 13 42 62	0.461 4.470 2.736	11 1 39	14 0.755 10 3.812 60 2.953		0 0 0.000 0 3 2.366 0 0 0.000	1 0	0 1.414 0 0.000 2 0.036
11BD 11BC 11BB 11CB	11 B D 11 B C 11 B B 11 C B	J11_B_D J11_B_C J11_B_B	111 111 111	13 0 21 20 0 0 13 10	5.099 0.243 0.000 0.948	11 18 0	0 4.690 18 0.024 0 0.000 10 0.948		0 0 0.000 0 0 0.000 0 0 0.000	3 0	0 0.000 2 0.632 0 0.000 0 0.000
11CB 11CA 11CD 11CC	11 C B 11 C A 11 C D	J11_C_B J11_C_A J11_C_D J11_C_C	111 111 111 111	13 10 162 133 3 0 0 11	2.401 2.449 4.712	13 133 3 0	108 2.244 0 2.449 4 2.846		7 5 0.861 0 0 0.000 0 0 0.000	17 2	0 0.000 0 0.608 0 0.000 7 3.755
11DC 11DB 11DA	11 D C 11 D B 11 D A	J11_D_C J11_D_B J11_D_A	111 111 111	2 0 3 0 22 4	2.000 2.449 4.895	1 3 19	0 1.414 0 2.449 4 4.321		0 0 0.000 0 0 0.000 0 0 0.000	0	0 1.414 0 0.000 0 2.000
11DD 12AC 12AB 12BA	11 D D 12 A C 12 A B 12 B A	J11_D_D J12_A_C J12_A_B J12_B_A	111 112 112 112	0 0 385 327 122 78 86 84	0.000 3.055 4.422 0.272	0 308 105 74	0 0.000 263 2.691 74 3.237 73 0.093		0 0 0.000 14 11 0.985 2 0 2.000 0 1 1.414	13	0 0.000 54 0.101 3 3.330 9 0.827
12BC 12CB 12CA 13AC	12 B C 12 C B 12 C A	J12_B_C J12_C_B J12_C_A	112 112 112	89 120 85 99 350 320	3.064 1.495 1.667 4.891	68 66 262	86 2.078 68 0.202 256 0.370		7 15 2.350 5 5 0.045 14 14 0.121 15 10 1.276	12 2 69 5	19 1.856 27 3.360 50 2.477
13AC 13AB 13BA 13BC	13 A C 13 A B 13 B A 13 B C	J13_A_C J13_A_B J13_B_A J13_B_C	113 113 113 113	511 406 35 26 40 64 1 0	1.610 3.340 1.414	417 33 35 1	338 4.066 26 1.269 62 3.889 0 1.414		15 10 1.276 0 0 0.000 0 0 0.000 0 0 0.000	1 3	58 1.407 0 1.414 2 0.632 0 0.000
13CB 13CA 14AD	13 C B 13 C A 14 A D	J13_C_B J13_C_A J14_A_D	113 113 114	10 2 455 399 47 71	3.293 2.715 3.177	34	2 2.712 325 1.555 37 0.520		0 0 0.000 15 15 0.130 1 13 4.448	81 5 11 2	0 2.000 59 2.623 22 2.657
14AC 14AB 14BA 14BD	14 A C 14 A B 14 B A 14 B D	J14_A_C J14_A_B J14_B_A J14_B_D	114 114 114 114	277 247 130 161 89 117 160 141	1.825 2.535 2.764 1.578	70	205 2.067 139 4.182 97 2.965 104 0.614		5 5 0.067 6 4 0.749 9 4 1.938 21 16 1.113	28 1 6 1	37 0.676 17 2.295 16 2.992 21 1.268
14BC 14CB 14CA	14 B C 14 C B 14 C A 14 C D	J14_B_C J14_C_B J14_C_A	114 114 114	216 155 179 146 279 264	4.479 2.630 0.898	172 123 234	131 3.374 114 0.789 225 0.621		7 5 0.707 11 3 2.903 7 12 1.523	29 1 44 2 31 2	19 1.985 28 2.694 28 0.562
14CD 14DC 14DB 14DA	14 D C 14 D B 14 D A	J14_C_D J14_D_C J14_D_B J14_D_A	114 114 114 114	47 51 55 30 194 168 84 121	0.557 3.791 1.906 3.668	35 42 133 73	46 1.662 29 2.145 110 2.120 105 3.421		0 0 0.000 3 0 2.449 15 16 0.316 1 2 0.816	9 39 4	5 2.258 1 3.546 12 0.541 14 1.115
15AC 15AB 15AA	15 A C 15 A B 15 A A 15 B A	J15_A_C J15_A_B J15_A_A J15_B_A	115 115 115 115	30 21 60 59 0 0	1.815 0.071 0.000	21 46 0	21 0.033 49 0.435 0 0.000		1 0 1.414 1 5 2.478 0 0 0.000	3 11 0	0 2.449 5 2.121 0 0.000
15BA 15BC 15BB 15CB	15 B C 15 B B	J15_B_A J15_B_C J15_B_B J15_C_B	115 115	139 190 307 298 1 14 400 409	3.998 0.535 4.716 0.433	252 1	170 4.269 248 0.237 8 3.271 328 0.308		2 3 0.744 15 13 0.674 0 2 2.000 11 14 0.862	33 3 0	0.185 0.668 4 2.811 0.635
15CA 15CC 22AC	15 C B 15 C A 15 C C 22 A C	J15_C_A J15_C_C J22_A_C	115 115 115 122	165 142 0 0 190 195	1.852 0.000 0.339	137 0 139	0 0.884 0 0.000 135 0.333		1 0 1.414 0 0 0.000 16 22 1.324	22 1 0 35 3	1.577 0 0.000 38 0.472
22AB 22BC 22BA 22CA	22 A B 22 B C 22 B A 22 C A 22 C B	J22_A_B J22_B_C J22_B_A J22_C_A	122 122 122 122	141 138 6 0 63 72 389 357	0.284 3.464 1.125 1.683	3 30	114 0.212 0 2.449 41 1.854 297 1.704		9 9 0.116 0 0 0.000 11 11 0.015 19 24 1.109	3 22 2	1.442 0 2.449 20 0.403 35 1.205
22CB 23AB 23AC	23 A B 23 A C	J22_C_B J23_A_B J23_A_C	122 123 123	12 12 47 47 160 178	0.014 0.000 1.385	8 41 132	8 0.000 41 0.016 159 2.227		0 0 0.000 0 0 0.000 7 4 1.303	6 21 1	4 0.025 6 0.041 15 1.363
23AD 23BA 23BC 23BD	23 A D 23 B A 23 B C	J23_A_D J23_B_A J23_B_C J23_B_D	123 123 123 123	18 16 45 47 224 174	0.485 0.229 3.575 0.000	11 36 198	10 0.324 36 0.025 145 4.072 38 0.139		1 0 1.414 3 4 0.704 5 8 1.177 1 0 1.414	6 21 2	6 0.020 6 0.020 21 0.022
23CA 23CB 23CD	23 B D 23 C A 23 C B 23 C D	J23_C_A J23_C_B J23_C_D	123 123 123	51 51 123 117 67 55 22 23	0.525 1.557 0.179	37 81 47 13	75 0.633 47 0.029 13 0.084		8 9 0.259 8 4 1.681 6 9 1.145	34 3 12 3	33 0.155 4 2.940 1 1.414
23DA 23DB 23DC	23 D A 23 D B 23 D C	J23_D_A J23_D_B J23_D_C	123 123 123	11 12 18 19 18 17	0.295 0.244 0.203	4 7 6	4 0.025 7 0.019 2 2.000		4 5 0.494 2 3 0.661 8 12 1.293		3 0.000 9 0.017 3 0.506

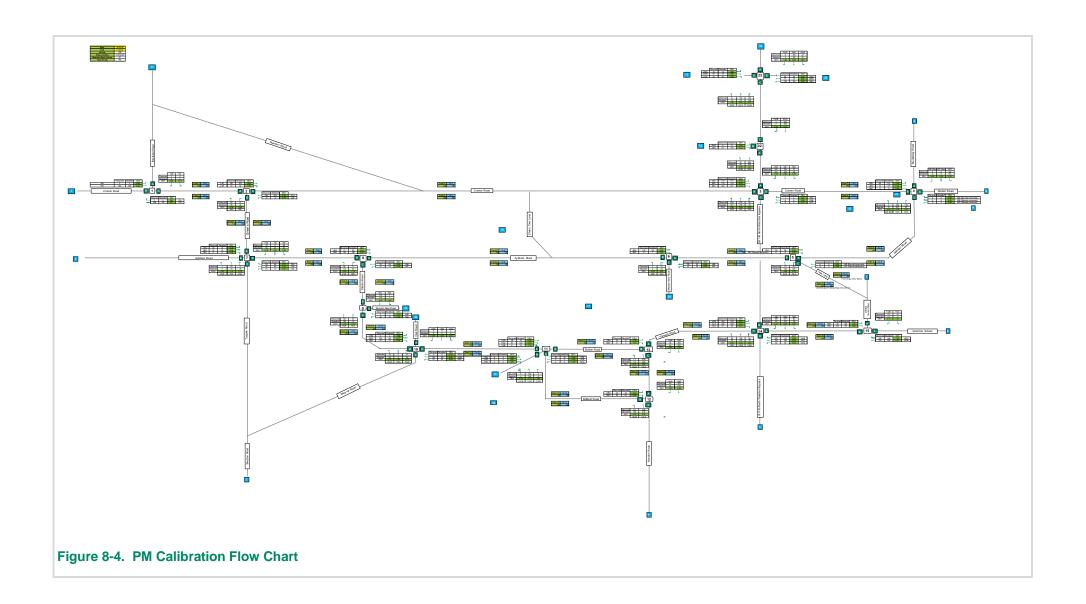
Figure 8-1. AM Cal Turns

hunstine Francisco	T-	Tues ID	Nada Ob		ALL VEH	CELL	Observed	CAR	OF!!	HGV	III-4 OFIL	LGV	oru
Junction From 1 A 1 A	C B	J1_A_C J1_A_B	101 101	served 6 3	Modelled 3	1.332 0.584	Observed N	Nodelled 3	0.717 0.661	Observed Mode 0	0 0.000 0 0.000	Observed Mode 0	0 0.000 1 0.049
1 B 1 B	A C	J1_B_A J1_B_C	101 101	6 563	4 536	0.944	4 452	4 456	0.050 0.197	0 17	0 0.000 16 0.159	1 78	0 1.414 64 1.705
1 C 1 C	B A	J1_C_B J1_C_A	101 101	467 2	439	1.323 2.000	388 1	374 0	0.709 1.414	13 1	19 1.397 0 1.414	54 0	46 1.109 0 0.000
2 A 2 A	C B	J2_A_C J2_A_B	102 102	482 88	438 104	2.073 1.604	387 70	378 83	0.481 1.486	15 2	13 0.411 3 0.632	65 12	47 2.478 18 1.479
2 B 2 B	A C	J2_B_A J2_B_C	102 102	115 53	116 48	0.102 0.696	95 41	95 44	0.041 0.438	3	3 0.000 0 1.033	13	19 1.386 4 1.961
2 C 2 C	A A	J2_C_B J2_C_A	102	79 353	76 323	0.352 1.632	70 296	72 280	0.190 0.958	1 12	0 1.414 16 0.944	6 37	4 0.749 28 1.626
3 A 3 A	D C B	J3_A_D J3_A_C J3_A_B	103 103 103	60 287 194	52 282 184	1.104 0.293 0.727	47 232 164	46 219 161	0.191 0.842 0.220	7 9	0 0.000 8 0.276 8 0.290	12 45 14	6 1.981 55 1.407 15 0.172
3 B 3 B	A D	J3_B_A J3_B_D	103	148	134 135	1.153	113 119	111	0.198 0.300	9 2	4 1.891 3 0.772	23 11	19 0.816 16 1.385
3 B 3 C	C B	J3_B_C J3_C_B	103	290 269	226 211	3.955 3.727	233 228	201 191	2.176 2.545	9	7 0.632 3 1.252	45 32	18 4.746 17 3.077
3 C 3 C	A D	J3_C_A J3_C_D	103 103	275 28	258 23	1.038	215 26	216 23	0.058 0.523	11 0	16 1.336 0 0.000	40 1	26 2.379 0 1.414
3 D 3 D	C B	J3_D_C J3_D_B	103 103	6	9	1.112 1.079	6	9	1.112 1.079	0	0 0.000	0	0 0.000
3 D 4 A 4 B	A D	J3_D_A J4_A_D J4_B_A	103 104 104	1 139 107	0 142 68	1.414 0.261 4.128	1 127 88	131 52	1.414 0.326 4.296	0 0 2	0 0.000 0 0.000 0 2.000	0 8 16	0 0.000 11 1.092 16 0.075
4 B 4 C	D A	J4_B_D J4_C_A	104	91 304	95 260	0.379 2.617	72 252	79 247	0.749 0.294	0	3 2.550 0 1.414	13 41	13 0.028 13 5.462
4 C 4 D	D C (Banned Movement)	J4_C_D Banned M	104 104	121	131	0.930	102 0	97 0	0.486 0.000	2	3 0.632 0 0.000	12 0	31 4.148 0 0.000
4 D 4 D	B (Banned Movement) A (Banned Movement)	Banned M Banned M	104 104	0	0	0.000	0	0	0.000 0.000	0	0 0.000 0 0.000	0	0 0.000 0 0.000
5 A 5 A	C (Banned Movement) B (Banned Movement)	Banned M Banned M	105 105	0	0	0.000	0	0	0.000 0.000 4.002	0	0 0.000	0	0 0.000
5 B	C (Banned Movement)	J5_B_A Banned M	105 105	180 0 194	110 0 139	5.818 0.000 4.304	142 0 171	98 0 122	0.000 4.084	0 4	0 1.414 0 0.000 0 2.828	24 0 12	12 2.884 0 0.000 17 1.289
5 C	A C	J5_C_B J5_C_A J6_A_C	105 105 106	248 50	282 38	2.074 1.737	213 42	247	2.220 0.560	2 0	3 0.632 0 0.000	29	32 0.561 0 0.000
6 A 6 B	B A	J6_A_B J6_B_A	106 106	148 159	100 94	4.320 5.769	129 128	83 82	4.463 4.457	4	0 2.828 0 1.414	12 24	17 1.277 12 2.884
6 B 6 C	C B	J6_B_C J6_C_B	106 106	9 5	7 5	0.670 0.000	6	7	0.430 0.000	0	0 0.000 0 0.000	0	0 0.000 1 0.000
6 C 7 A	A D	J6_C_A J7_A_D	106	21 81	16 101	1.162 2.052	14 68	16 80	0.516 1.356	1	0 0.000 3 1.414	0 10	0 0.000 18 2.115
7 A 7 A 7 B	C B A	J7_A_C J7_A_B J7_B_A	107 107 107	27 64 40	21 59 35	1.203 0.625 0.741	17 53 30	21 55 31	0.939 0.232 0.226	1 0	0 1.414 0 1.414 0 0.548	4 7 9	0 2.828 4 1.089 4 1.938
7 B	A D C	J7_B_D J7_B_C	107	116	104	1.174	91 5	91	0.021 0.000	2 0	3 0.744 0 0.000	18	10 2.230 0 0.000
7 C	B A	J7_C_B J7_C_A	107	5 29	4 22	0.496 1.439	4 24	4 19	0.025 1.136	0 2	0 0.000 3 0.632	1 2	0 1.414 0 2.000
7 C 7 C 7 D	A D C	J7_C_D J7_D_C	107 107	22 24	16 17	1.266 1.594	17 21	16 17	0.134 0.966	0	0 0.000 0 0.000	5 2	0 3.162 0 2.000
7 D 7 D	B A	J7_D_B J7_D_A	107 107	79 101	78 108	0.164 0.685	66 82	64 89	0.236 0.773	2 2	0 2.000 0 2.000	10 15	13 1.008 19 0.936
8 A 8 A	C B	J8_A_C J8_A_B	108	20 97 99	18 67 68	0.530 3.331	15 79	16 59 62	0.179 2.453	4	0 1.414 0 2.828	3 13	2 0.632 8 1.474 7 4.022
8 B 8 B	C B	J8_B_A J8_B_C J8_C_B	108 108 108	116 106	153 136	3.339 3.194 2.740	71 100 89	126 112	1.142 2.424 2.290	1 2 0	0 1.414 6 2.093 0 0.000	22 11 14	7 4.022 21 2.511 24 2.334
8 C 9 A	A C	J8_C_A J9_A_C	108	77	56 42	2.549	59 42	48 42	1.475	1 0	0 1.414	14	8 1.809 0 0.000
9 A 9 B	B A	J9_A_B J9_B_A	109 109	4	1 2	1.897 1.292	3	1 2	1.414 0.676	0	0 0.000 0 0.000	0 2	0 0.000 0 2.000
9 B 9 C	C B	J9_B_C J9_C_B	109 109	134 178	169 192	2.828 1.008	113 145	139 160	2.350 1.175	3 0	6 1.511 0 0.000	15 28	23 1.866 32 0.766
9 C 10 A	A D	J9_C_A J10_A_D	109	24 6	14 0	2.333 3.464	20	12	1.972 2.000	0	0 0.000	0	2 0.640 0 0.000
10 A 10 A 10 B	B A	J10_A_C J10_A_B J10_B_A	110 110 110	0 6 0	8	0.000 0.756 1.924	0 6 0	0 8 2	0.000 0.756 1.924	0 0	0 0.000 0 0.000 0 0.000	0 0 0	0 0.000 0 0.000 0 0.000
10 B 10 B	C C	J10_B_D J10_B_C	110	127 47	168 41	3.395 0.905	108 44	139	2.768	2	6 2.093 0 1.414	14	23 2.143 0 1.414
10 C 10 C	B A	J10_C_B J10_C_A	110 110	34	30 0	0.671 2.000	29	30	0.221	0	0 0.000	2	0 2.000 0 0.000
10 C 10 D	D C	J10_C_D J10_D_C	110 110	28 27	20 45	1.644 2.978	21 19	20 35	0.232 3.038	0	0 0.000 0 0.000	6 8	0 3.464 10 0.698
10 D 10 D	B A	J10_D_B J10_D_A	110	162 5	167 4	0.394	130 5 28	133	0.257 0.397	0	0 0.000	27 0	34 1.285 0 0.000
11 A 11 A 11 A	D C B	J11_A_D J11_A_C J11_A_B	111 111 111	33 111 9	18 150 12	2.993 3.418 0.854	28 91 8	16 122 12	2.583 3.044 1.193	0 2 0	0 0.000 6 2.129 0 0.000	18 1	2 0.000 21 0.734 0 1.414
11 A	A A	J11_A_A J11 B A	111	8	9	0.293	6	9	1.046	0	0 0.000	2 2	0 2.000
11 B 11 B 11 B 11 B	A D C	J11_B_D J11_B_C	111 111	3 2	2 2	0.632	2 2	2	0.000 0.000	0	0 0.000 0 0.000	0	0 0.000
11 C	B B	J11_B_B J11_C_B	111 111	0 10	0	0.000 2.314	0 6	0	0.000 0.944	0	0 0.000 0 0.000	0	0 0.000 0 2.449
11 C 11 C	A D	J11_C_A J11_C_D J11_C_C	111 111 111	163	154 0 2	0.703 2.828 0.782	126 3	124 0 2	0.183 2.449 0.782	0 0	0 0.000 0 0.000 0 0.000	33 1 0	0 0.498 0 1.414 0 0.000
11 D 11 D	C B	J11_D_C J11_D_B	111	2	0	2.000	2	0	2.000	0	0 0.000	0	0 0.000
11 D 11 D	A D	J11_D_A J11_D_D	111 111	27 0	43 0	2.667 0.000	22 0	33 0	2.080 0.000	1 0	0 1.414 0 0.000	2	10 3.225 0 0.000
12 A	C B	J12_A_C J12_A_B	112 112	388 101	390 56	0.104 5.137	303 80	315 46	0.691 4.334	10	14 1.141 0 0.000	68 20	61 0.878 10 2.612
12 A 12 B 12 C 12 C 13 A 13 A 13 B 13 B	A C	J12_B_A J12_B_C	112	51 68 109	44 85 125	0.956 1.987 1.510	44 55 85	42 63 109	0.243 0.991 2.446	3	0 0.000 7 1.643	6 10 19	2 2.000 16 1.713 16 0.655
12 C 12 C	B A C	J12_C_B J12_C_A J13_A_C	112 112 113	442 501	395 441	2.292	358 394	319 357	2.097	0 9 11	0 0.000 12 1.053 14 0.822	66 88	16 0.655 63 0.342 71 1.948
13 A 13 B	В	J13_A_B J13_B_A	113 113	35 25	40 42	0.777 2.967	30 43	40 41	1.651 0.379	0	0 0.000	4 2	0 2.828 2 0.259
13 B 13 C 13 C	A C B	J13_B_C J13_C_B	113 113	9	4 10	2.079 0.667	8 11	4 10	1.753 0.309	0	0 0.000 0 0.000	0	0 0.000 0 2.449
13 C 14 A	A D C B	J13_C_A J14_A_D	113 114	492 60	428 61	2.998 0.173	399 53	350 49	2.537 0.517	10	13 0.745 0 1.414	74 6	65 1.042 12 2.014
14 A 14 A	B	J14_A_C J14_A_B	114 114 114	237 132 96	227 122 58	0.650 0.892 4.369	194 105 80	189 111 58	0.332 0.582 2.688	5 3 4	7 0.760 3 0.000 0 2.828	34 22 12	31 0.553 8 3.647 0 4.899
14 A 14 A 14 A 14 B 14 B 14 B	A D C	J14_B_A J14_B_D J14_B_C	114	263 239	261 199	0.142	211 189	212 157	0.079 2.405	10	11 0.443 4 0.485	38 44	37 0.147 38 0.978
14 C	B A	J14_C_B J14_C_A	114 114	194 289	150 261	3.331 1.679	160 238	129 208	2.605 2.009	4 5	3 0.450 8 1.246	25 44	18 1.405 45 0.142
14 C 14 D	D C	J14_C_D J14_D_C	114 114	58 64	55 57	0.446 0.920	51 52	50 52	0.212 0.021	1 2	1 0.236 3 0.689	6 10	4 0.944 2 3.321
14 C 14 D 14 D 14 D 15 A	B A C	J14_D_B J14_D_A J15_A_C	114 114 115	237 85	93 24	1.024 0.858 0.254	195 65	192 70	0.237 0.632	10 2	13 0.787 3 0.689	26 14	17 1.905 20 1.411 3 0.661
15 A 15 A	B A	J15_A_C J15_A_B J15_A_A	115 115 115	20 60 0	21 51 0	0.254 1.215 0.000	16 50 0	17 51 0	0.270 0.134 0.000	0 0	0 0.000 0 0.000 0 0.000	9 0	3 0.661 0 4.243 0 0.000
15 B 15 B	B A A C	J15_B_A J15_B_C	115	190 280	172 235	1.304	151 230	138 193	1.047 2.562	4 7	0 2.828 11 1.436	31 40	34 0.535 31 1.591
15 A 15 A 15 B 15 B 15 C 15 C 15 C 22 A	B B	J15_B_B J15_C_B	115 115	1 361	4 358	1.875 0.137	1 294	4 298	1.875 0.209	0 8	0 0.000 10 0.651	0 52	0 0.000 51 0.160
15 C 15 C	A C C	J15_C_A J15_C_C	115 115	180	164	1.251 0.000	160 0	148	0.996 0.000	0	3 0.632 0 0.000	14 0	13 0.286 0 0.000
22 A 22 A 22 B	C B C	J22_A_C J22_A_B	122 122 122	338 74 8	304 89 8	1.921 1.709 0.018	282 47 8	259 69 8	1.411 2.859 0.018	10 10 0	10 0.048 10 0.047 0 0.000	46 17 0	35 1.737 11 1.738 0 0.000
22 B 22 B	A A B	J22_B_C J22_B_A J22_C_A J22_C_B	122 122 122	163 367	155 363	0.018 0.655 0.194	127 316	125 303	0.018 0.218 0.750	6 10	2 2.000 14 1.115	30 41	0 0.000 28 0.334 47 0.853
22 C 23 A		J22_C_B J23_A_B	122 122 123	5 38	6 38	0.194 0.447 0.049	3 3 27	2 27	0.632 0.029	10 2 5	2 0.000 5 0.044	0	2 2.025 6 0.020
23 A 23 A	C D	J23_A_B J23_A_C J23_A_D	123 123	120 9	115	0.438 1.915	105 8	96 4	0.893 1.609	2 0	4 1.131 0 0.000	13	15 0.599 0 1.311
23 B 23 B	B C D A C D A B	J23_B_A J23_B_C	123 123	68 152	69 151	0.121 0.114	58 130	59 125	0.085 0.483	0 5	0 0.000 8 1.194	10 17	10 0.110 18 0.239
23 B	D A	J23_B_D J23_C_A	123 123 123	12 160 142	15 151	0.816 0.722	11 124	13 117	0.577 0.601 0.474	0 6	0 0.000 6 0.121	1 30	2 0.816 27 0.504
23 C	B				145	0.284	132	138	0.474	0	0.000	10	8 0.702
22 B 22 C 22 C 23 A 23 A 23 B 23 B 23 C 23 C 23 C 23 C 23 D	B D A B	J23_C_B J23_C_D J23_D_A J23_D_B	123	14	16 19	0.491	8 16	12 15	1.336 0.254	4 0	4 0.179 0 0.000	2 3	0 2.000 4 0.510

Figure 8-2. PM Cal Turns

Appendix C – Flow Diagram

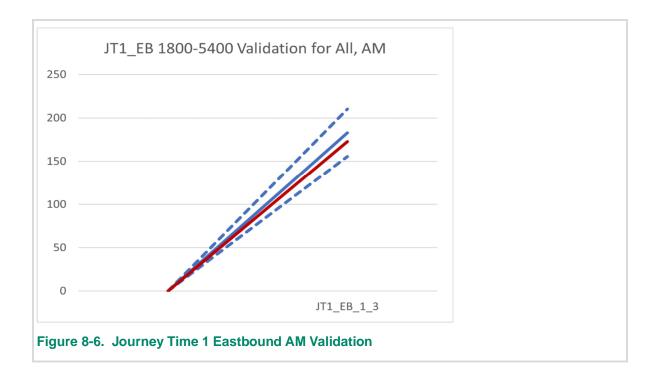




Appendix D – Journey Time Validation Results



Figure 8-5. JT1 Route Diagram



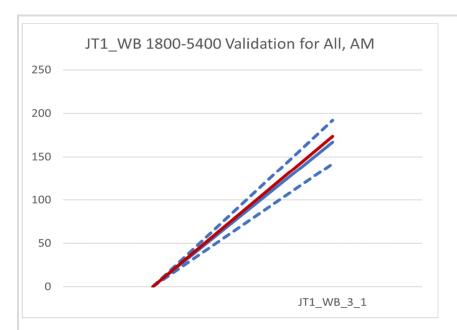


Figure 8-7. Journey Time 1 Westbound AM Validation

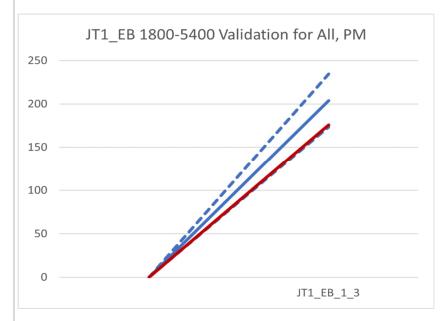
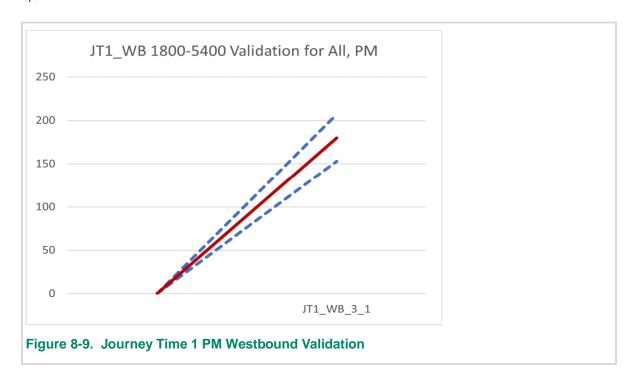
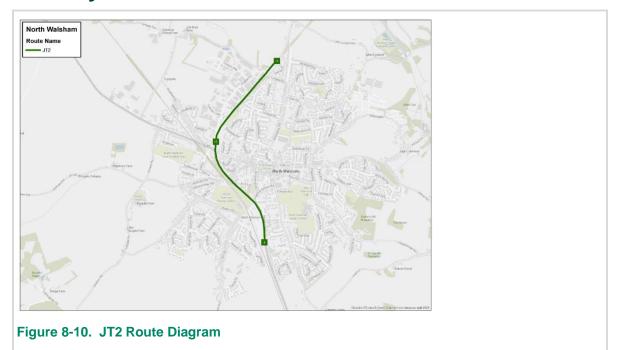
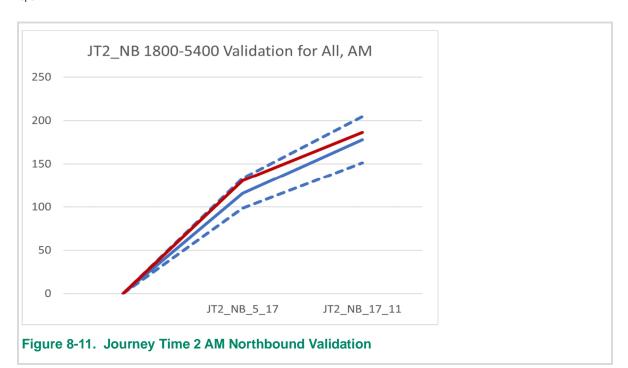
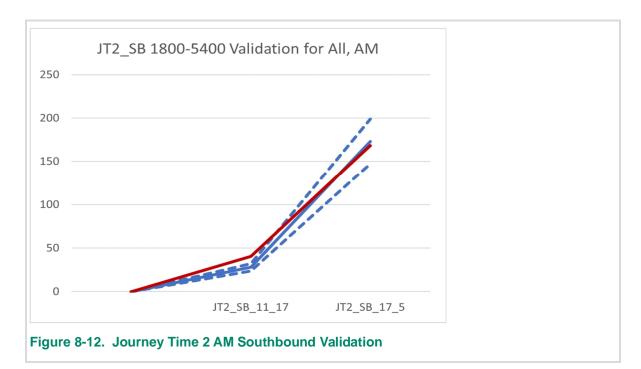


Figure 8-8. Journey Time 1 PM Eastbound Validation









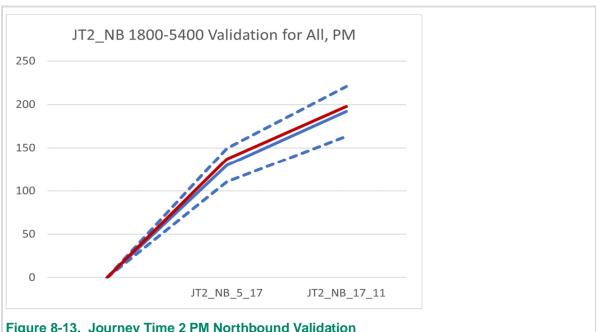


Figure 8-13. Journey Time 2 PM Northbound Validation

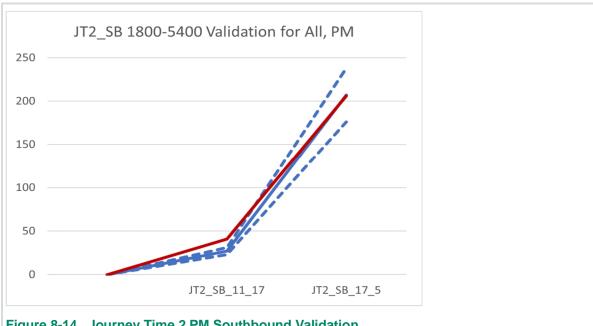


Figure 8-14. Journey Time 2 PM Southbound Validation

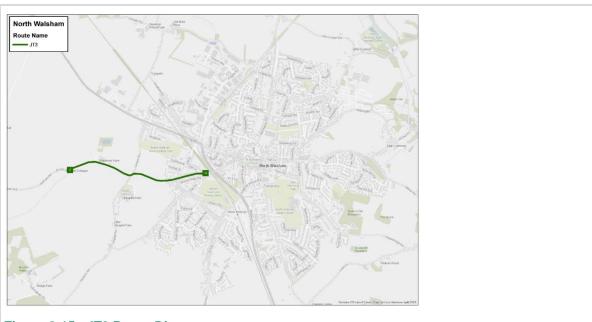
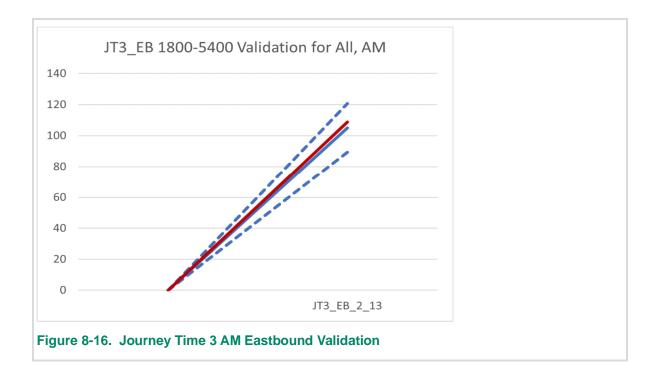
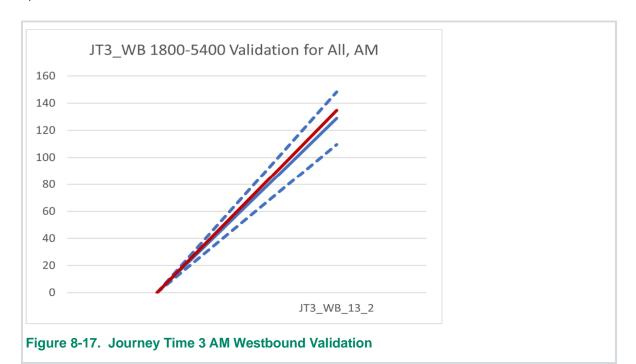
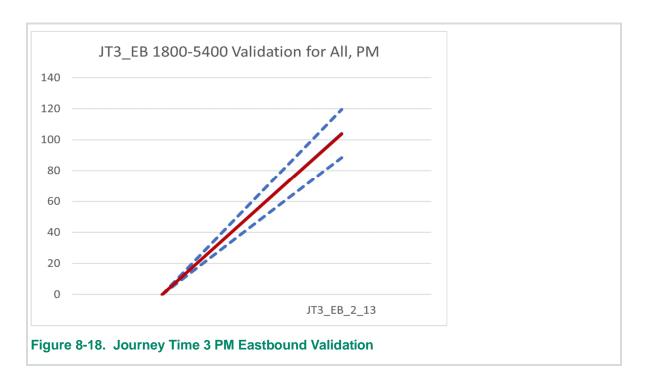
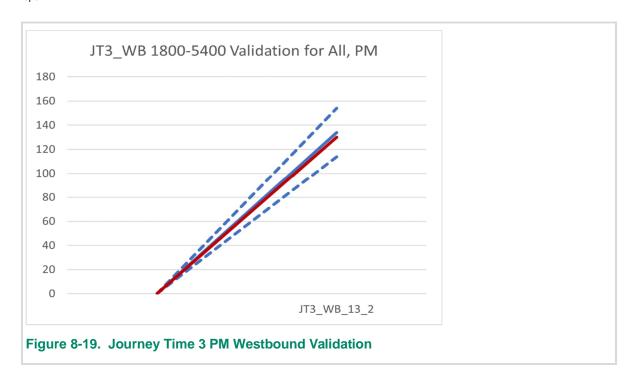


Figure 8-15. JT3 Route Diagram









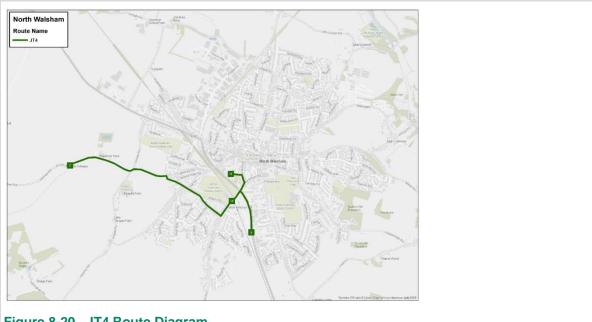
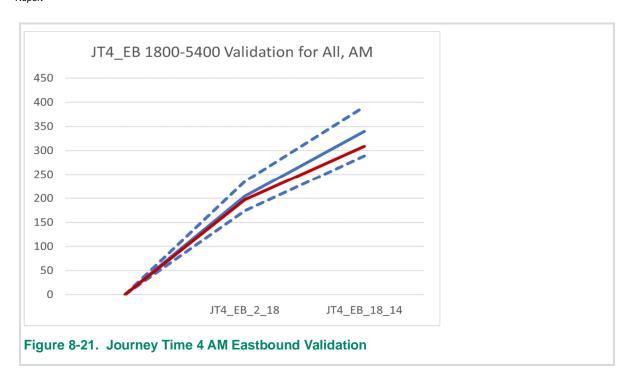
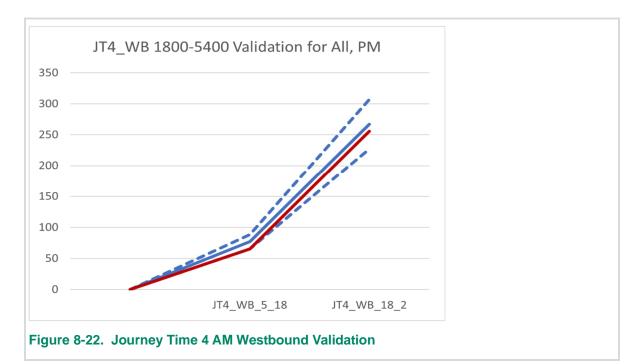
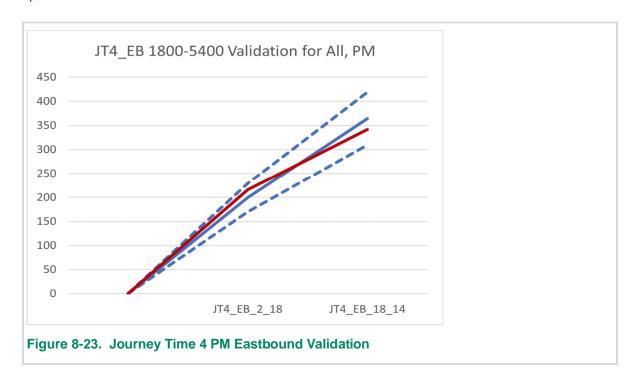


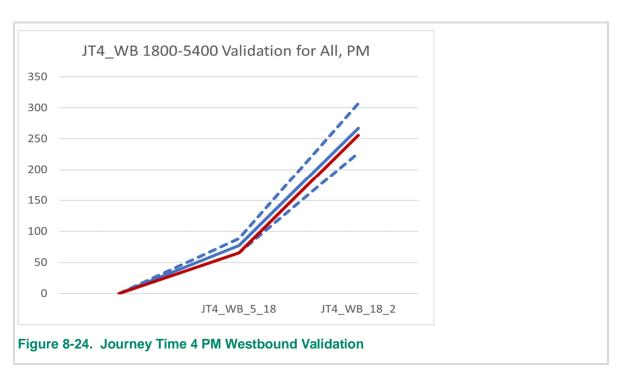
Figure 8-20. JT4 Route Diagram





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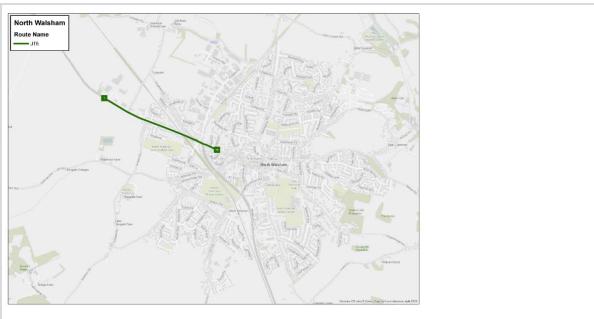
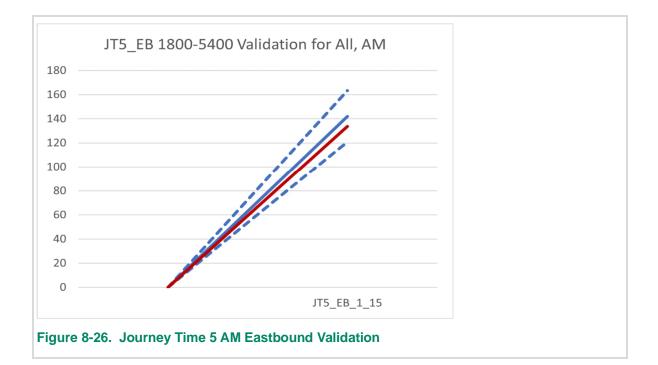
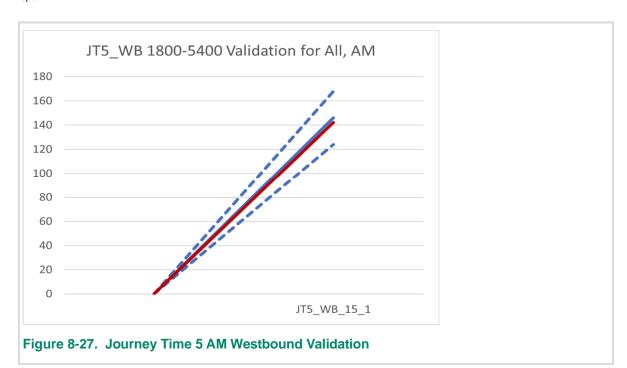
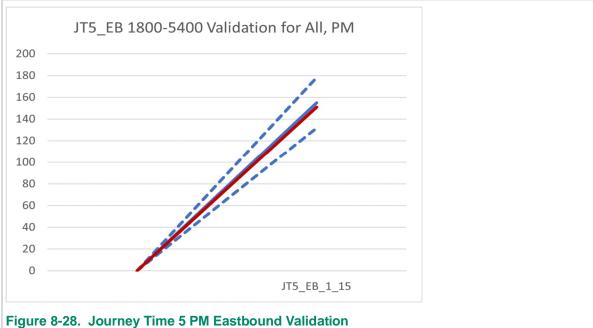


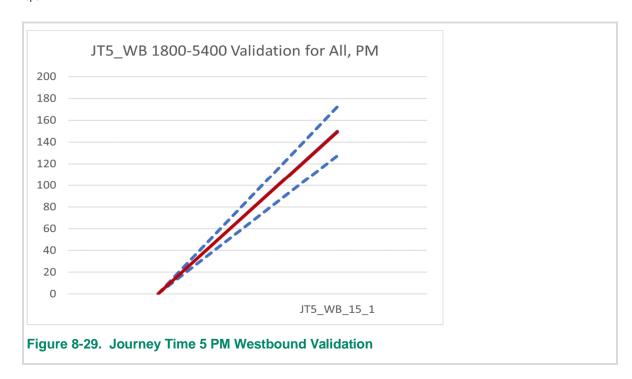
Figure 8-25. JT5 Route Diagram

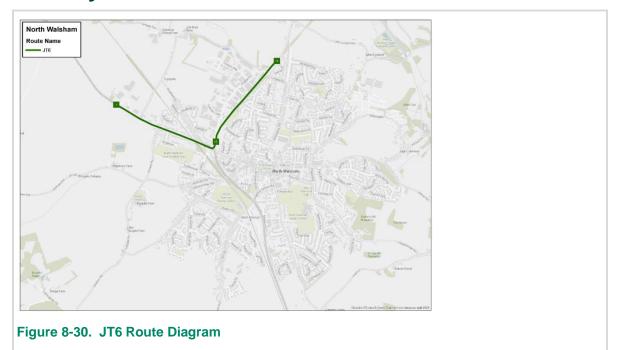


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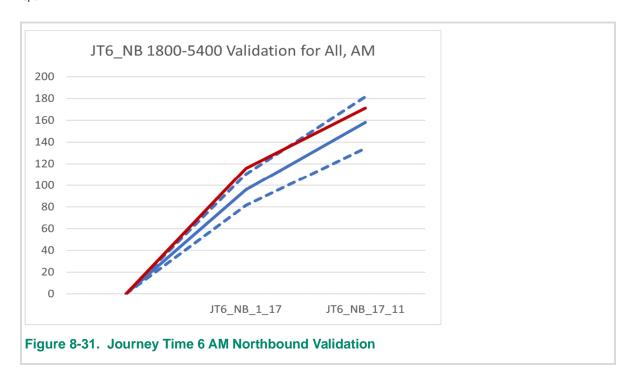


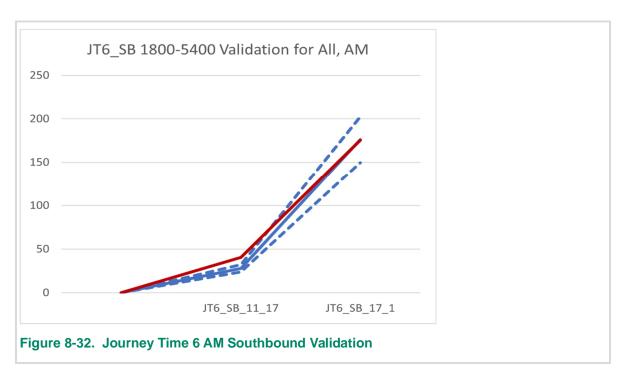


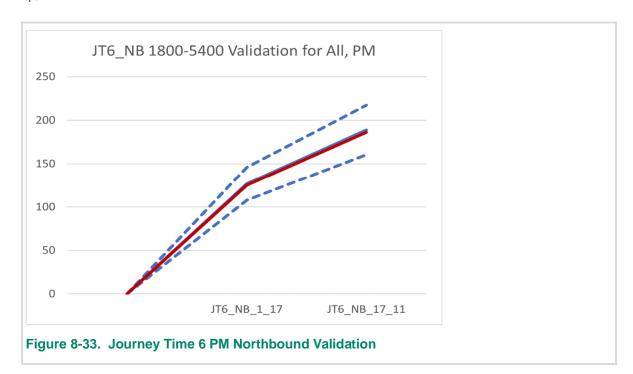


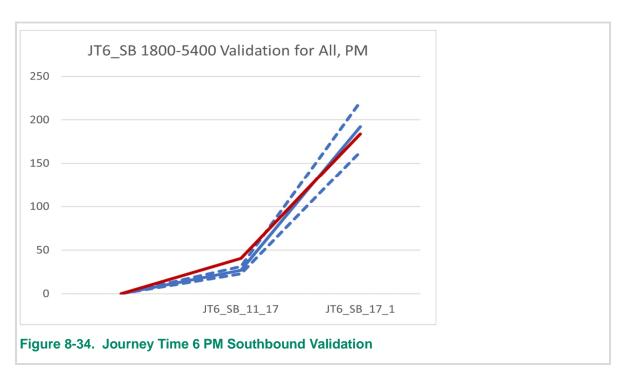


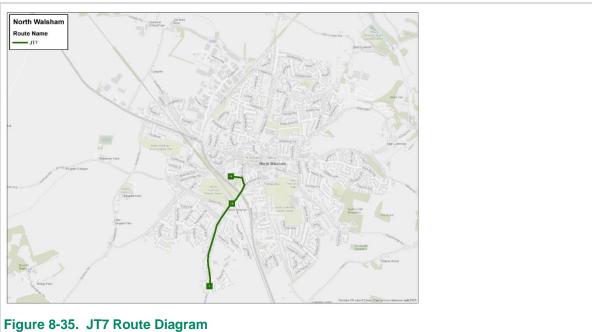
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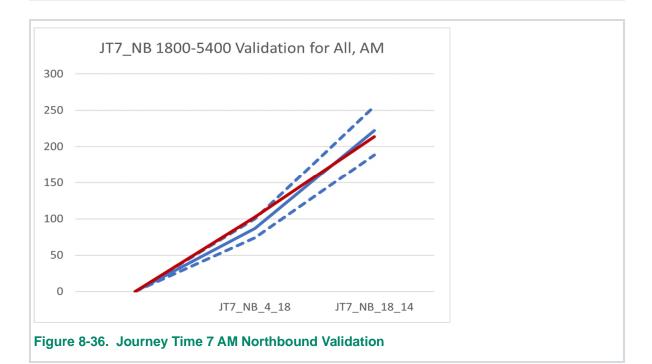


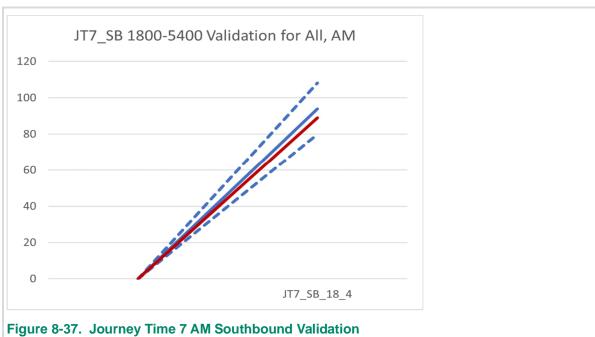


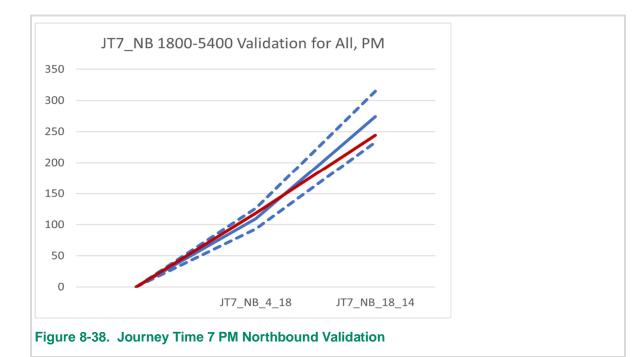




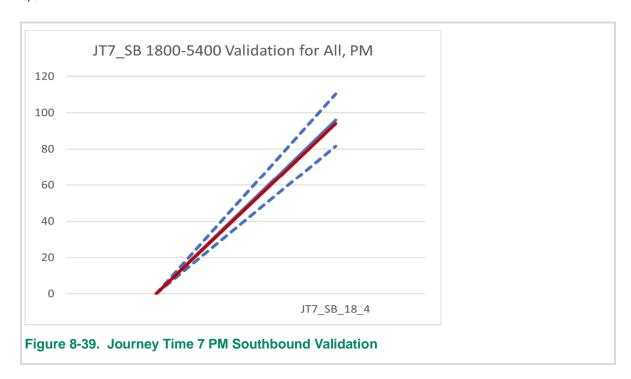


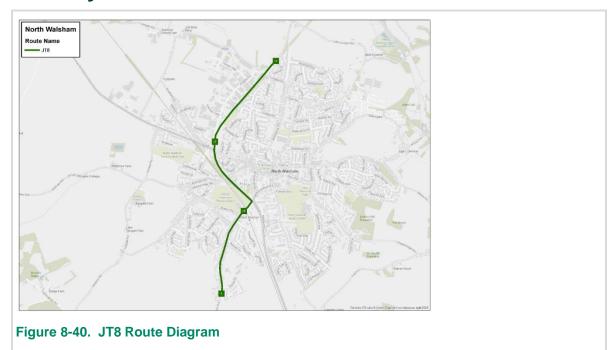


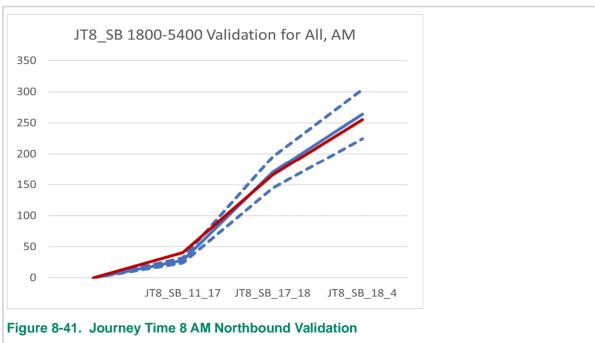


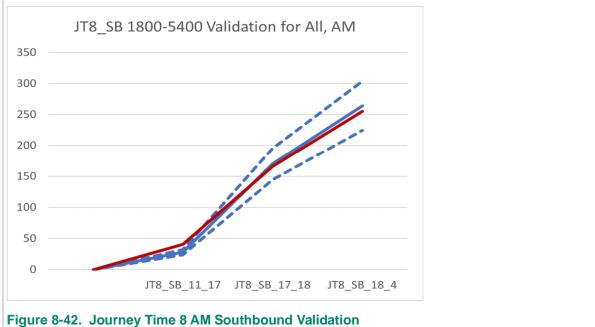


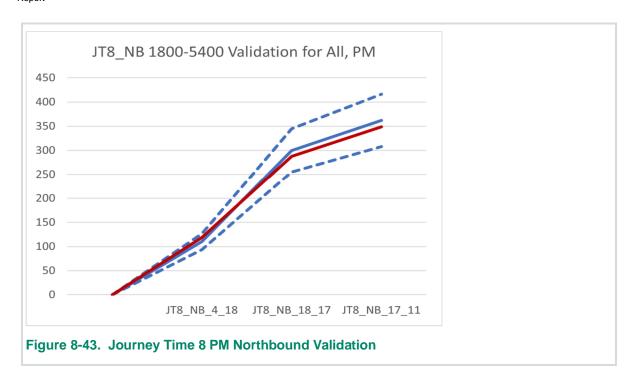
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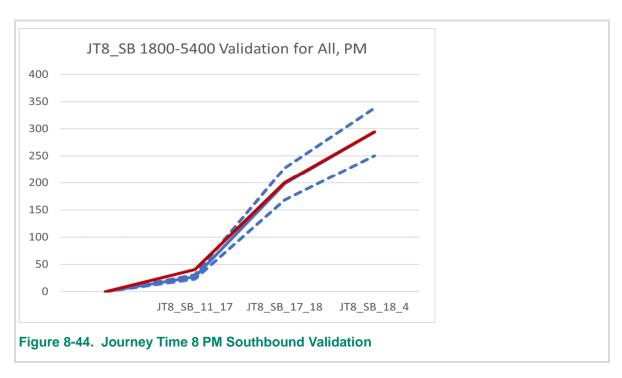






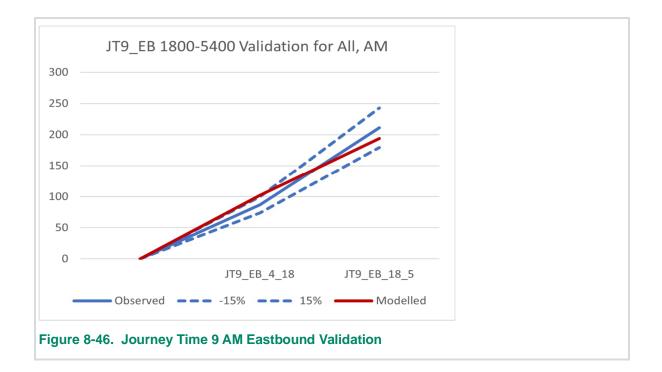


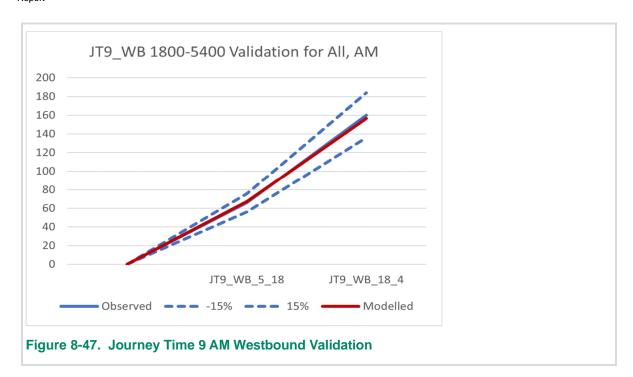


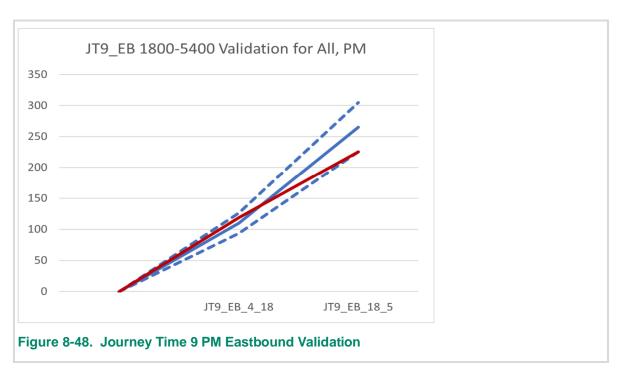


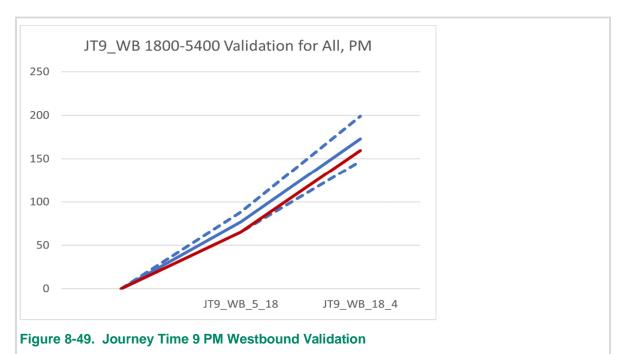




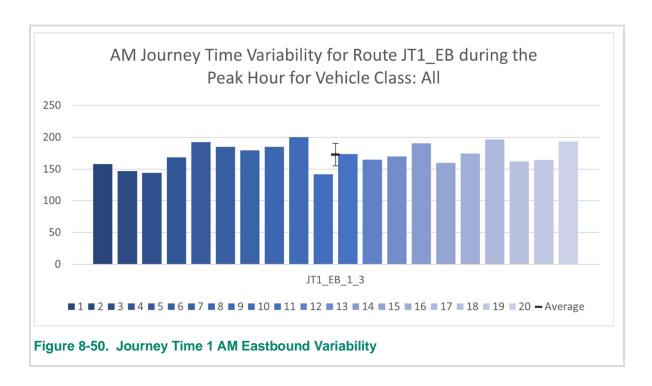


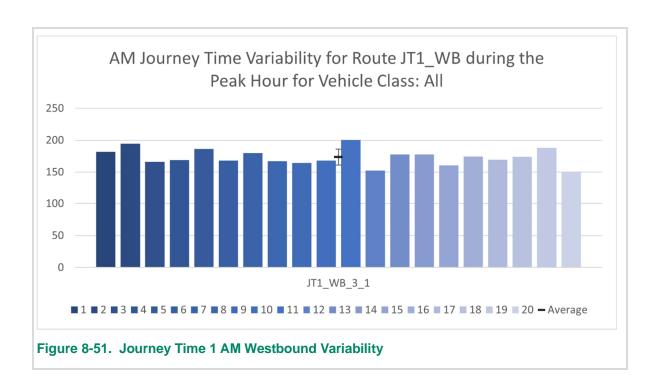


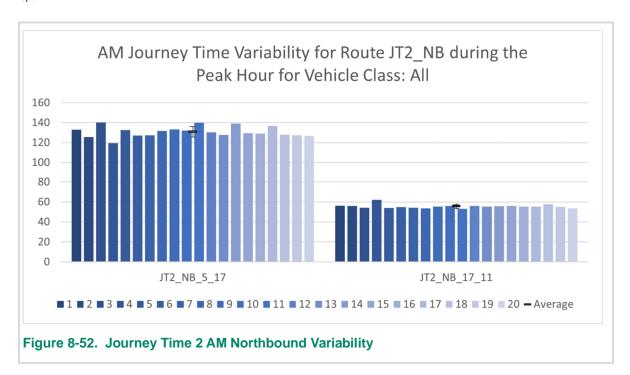


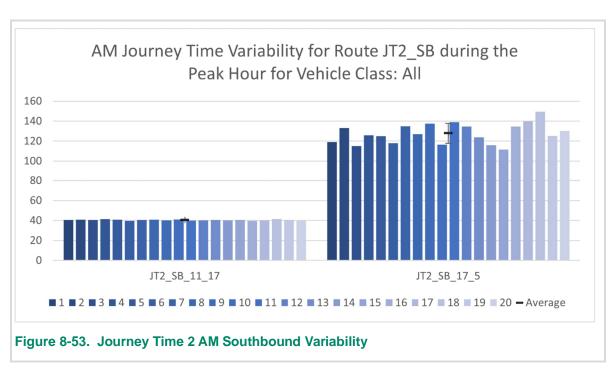


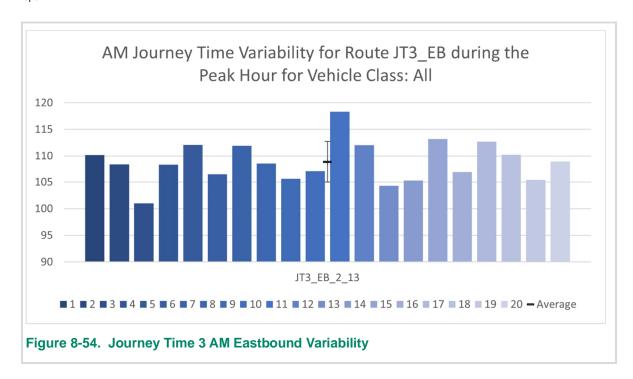
Appendix E – Journey Time Variability

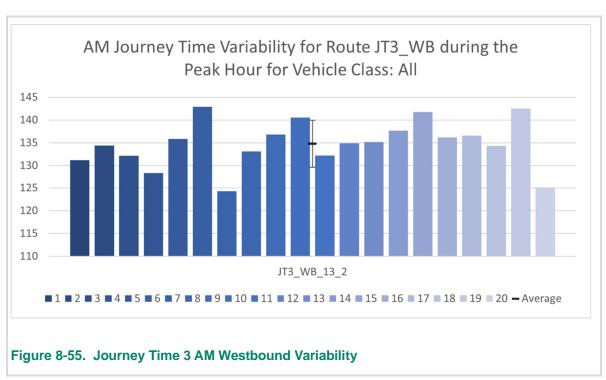


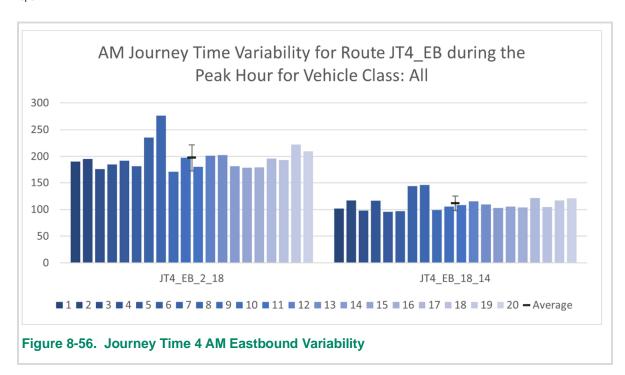


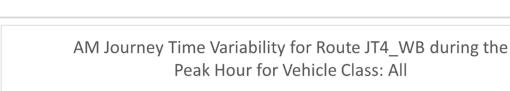












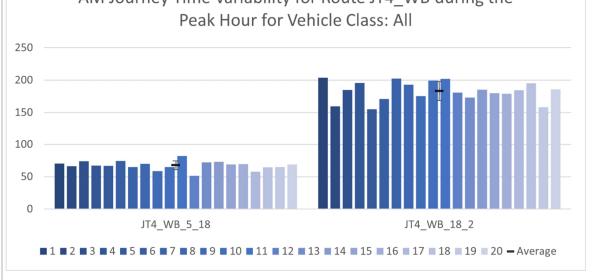
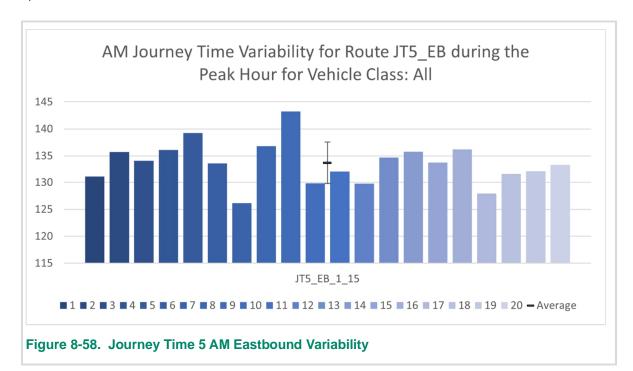


Figure 8-57. Journey Time 4 AM Westbound Variability



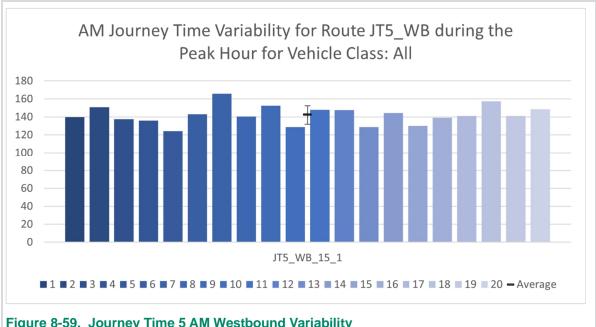
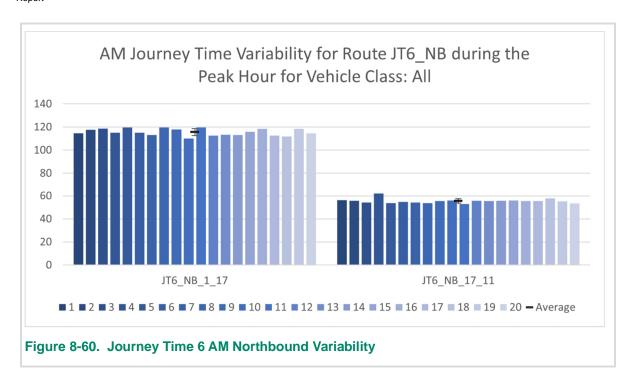
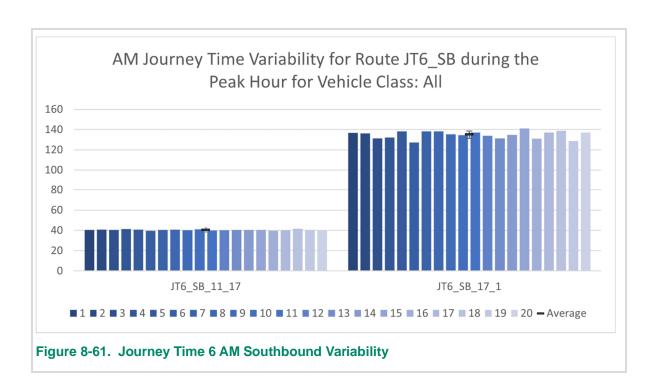
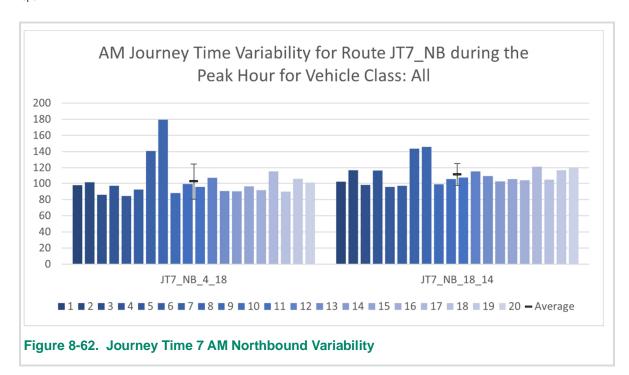
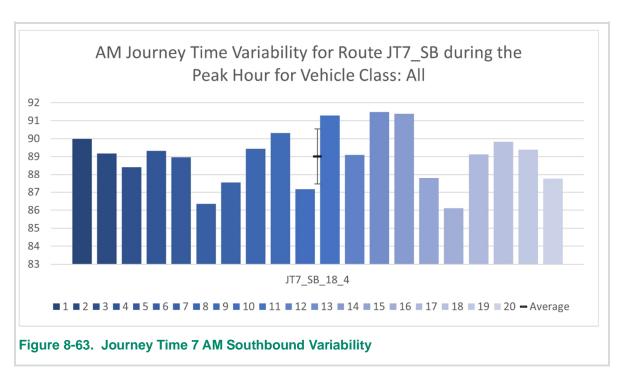


Figure 8-59. Journey Time 5 AM Westbound Variability









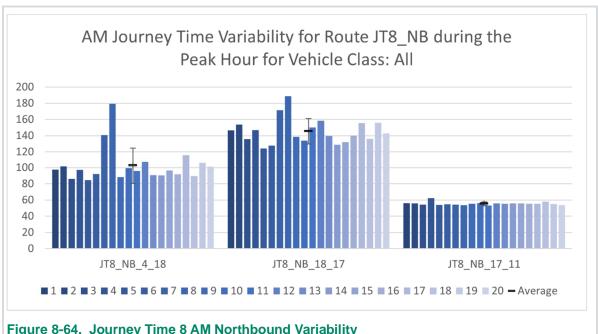
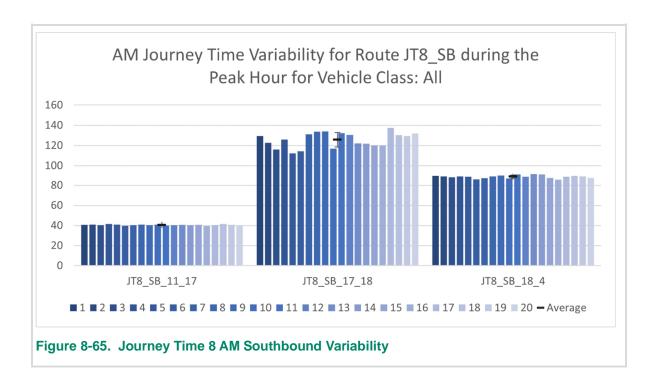
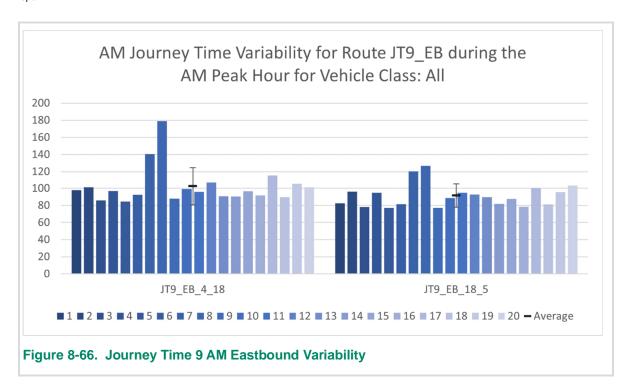
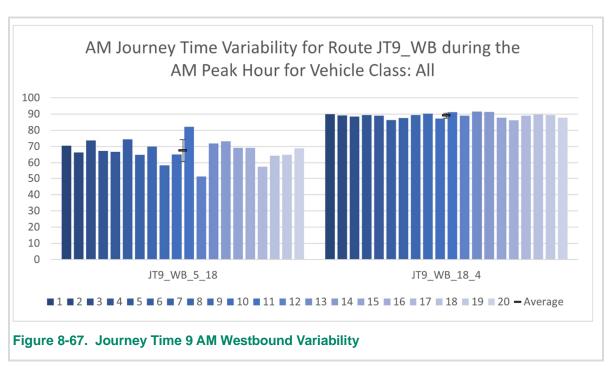
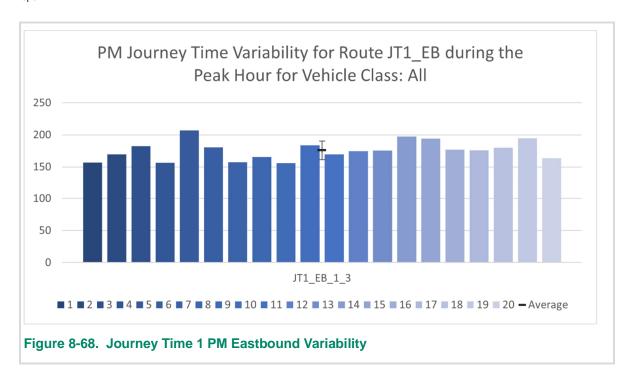


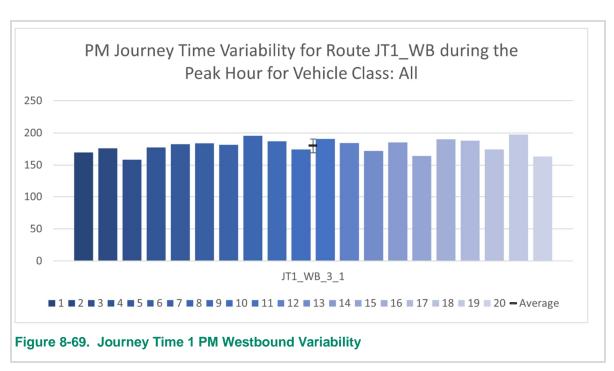
Figure 8-64. Journey Time 8 AM Northbound Variability

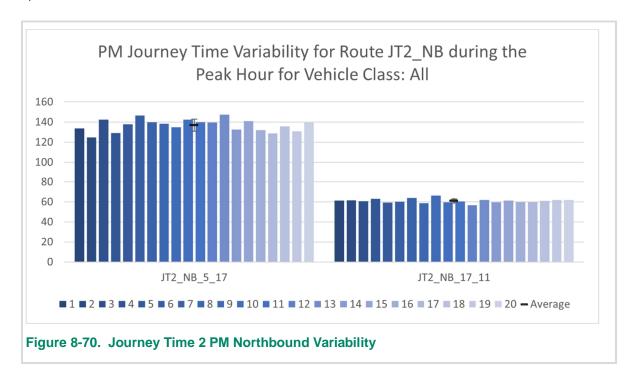












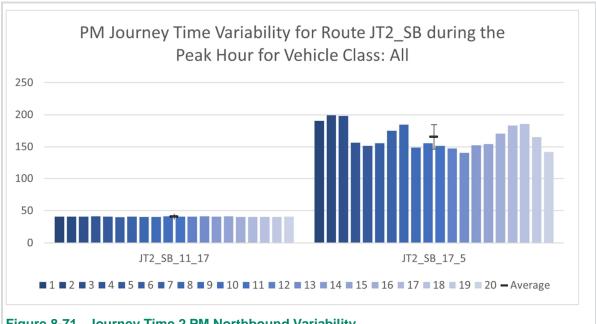
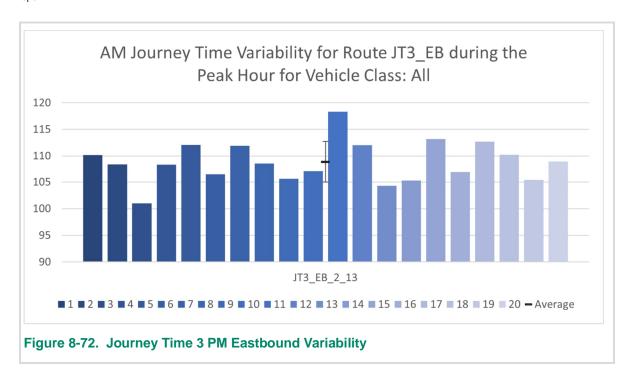
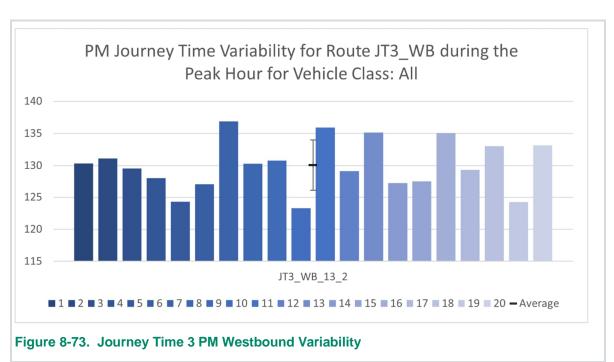
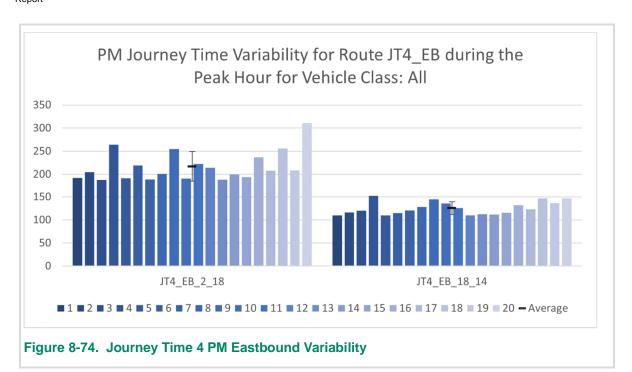


Figure 8-71. Journey Time 2 PM Northbound Variability







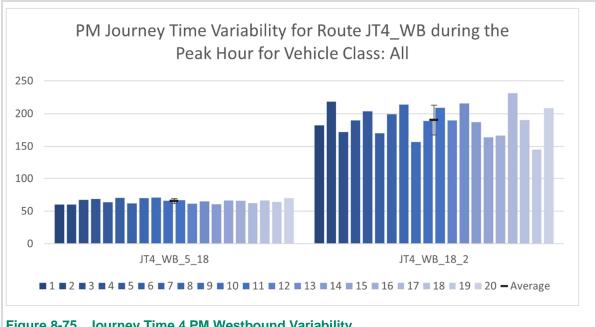
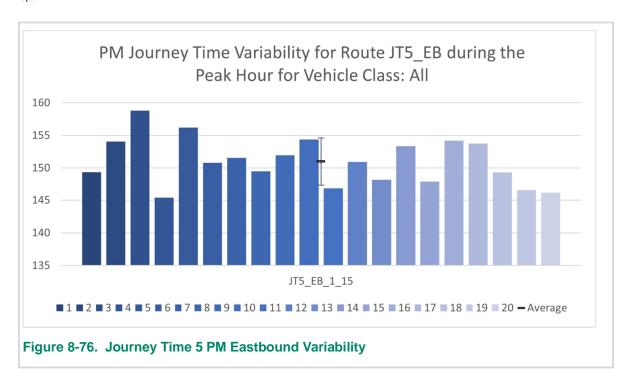
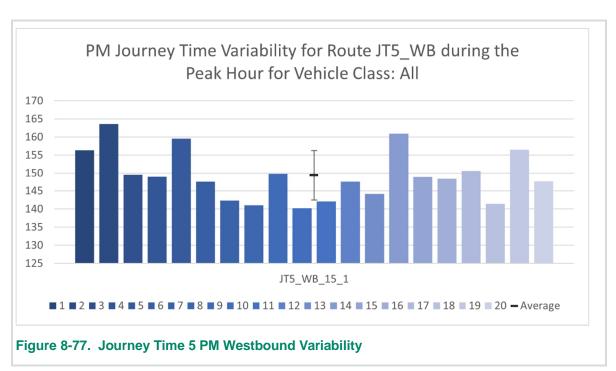
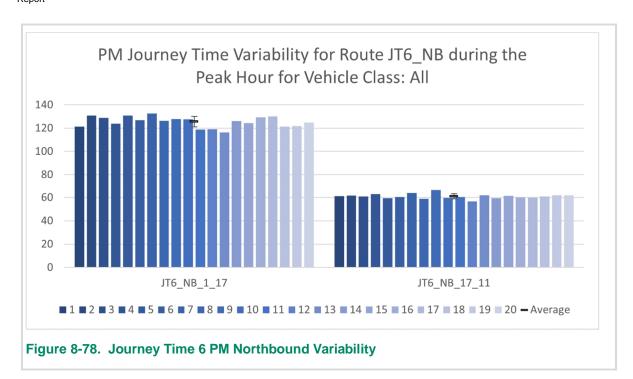
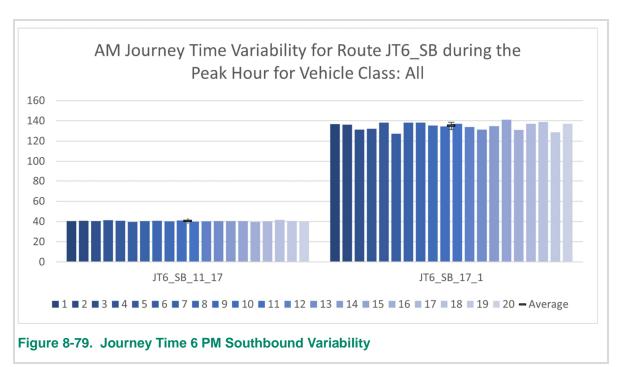


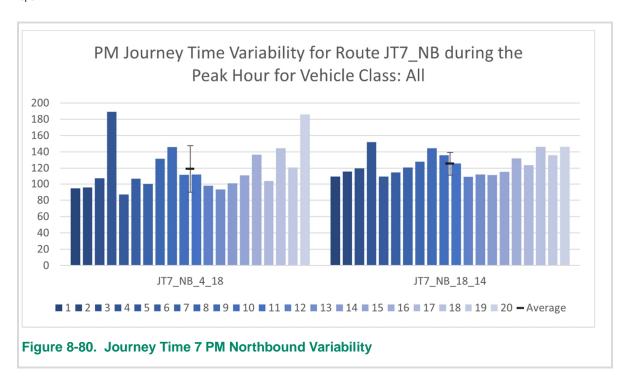
Figure 8-75. Journey Time 4 PM Westbound Variability

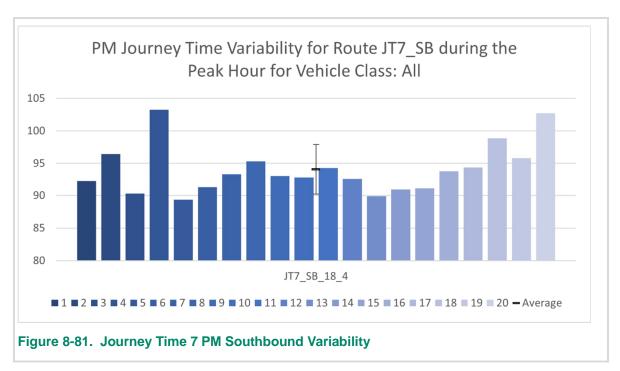












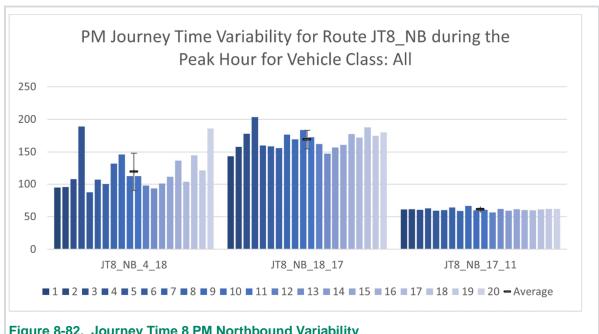
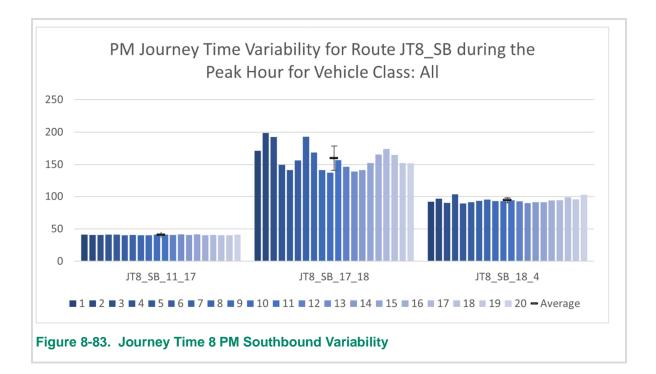
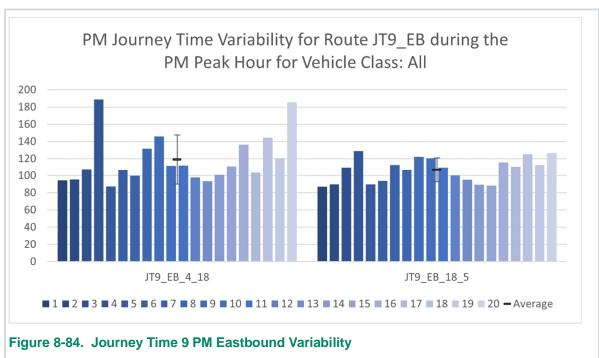
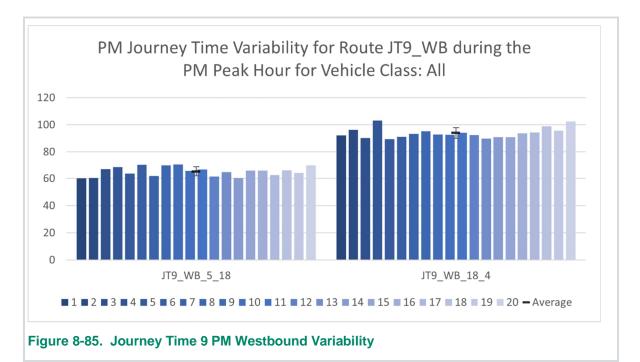


Figure 8-82. Journey Time 8 PM Northbound Variability







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Coltishall Vissim Model Validation Report

ESCO Developments, Flagship Housing Group and Lovell Partnerships

21 April 2023

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Revision Histo	ry				
Revision	Revision date	Details	Authorized	Name	Position
1.0	21/04/2023	Revision for Client Review	ВС	B Carey	Regional Director
Distribution Lis	st				
# Hard Copies PDF Required		Association / Company Name			

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1. Introduction

Background and Report Structure

- 1.1 ESCO Developments, Flagship Housing Group and Lovell Partnerships ('The Client Group') have commissioned AECOM to develop a VISSIM base model of the village of Coltishall to set up a reliable basis to assess the future operation of the network and the potential impact of the North Walsham Western Urban Extension (NWWUE). The model has been calibrated and validated to replicate the operation of the town based on data collected in November 2022.
- 1.2 This report documents the data collection and analysis, the development of the network and base year demand, and the calibration/ validation. The report is structured as follows:
 - Data collection and analysis;
 - · Demand development;
 - · Network Development;
 - · Model Calibration results;
 - · Model Validation results; and
 - Conclusion.

Model Scope

1.3 The Vissim model has been developed for the area shown in Figure 1-1. The Coltishall network has no signalised junctions with all the junctions operating as priority controlled. The model area includes a mini roundabout to the west of the village, a small gyratory road around a petrol station in the centre of the village and the narrow bridge over the river in the middle of the village. The Vissim model area shown in Figure 1-1 includes the B1150, which is the main corridor between Norwich and North Walsham, and the critical junctions/ links constraining the capacity of the corridor, such as the bridge and the village centre.



Figure 1-1 - Coltishall Modelled Area

1.4 Figure 1-2 below shows the key junctions/ locations identified from the survey data/ observations in the model area that have a critical impact on network operation.



Figure 1-2 - Key areas in Coltishall

- 1.5 The key areas are defined as follows:
 - 1. Roundabout linking Rectory Road to the B1150;
 - 2. Bridge over the River Bure on the B1150;
 - 3. Gyratory road around the Esso Petrol Filling Station (PFS); and
 - 4. High Street in Coltishall.
- 1.6 These areas have been considered when developing the model to replicate the existing operation and driving behaviour observed in the video footage available. It should be noted that the operation of some of these critical areas is entirely dependent on variable factors such as on-street parking and courtesy/ give way behaviours, which have been modelled and calibrated to observed queuing patterns/ levels of delay.
- 1.7 The Vissim Base models have been developed for the AM and PM peak hours, including 15-minute warm-up and 15-minute cool-down periods.
- 1.8 The Base models have been developed in line with modelling requirements and the calibration and validation criteria defined in Transport Analysis Guidance (TAG) and the Guidelines for the Use of Microsimulation Software published in May 2022 by National Highways.

2. Data Collection and Analysis

Introduction

2.1 The data collection exercise undertaken by AECOM to inform the Vissim Base model development has been summarised in this section.

Manual Classified Turning Count (MCTC) Data

2.2 Manual Classified Turning Counts (MCTCs) were carried out at the sites indicated in Figure 2-1 on Thursday 10th November 2022 between 07:00 and 19:00. The MCTC data was used to develop the base model demand and calibrate the turning flows at each junction shown in Figure 2-1.

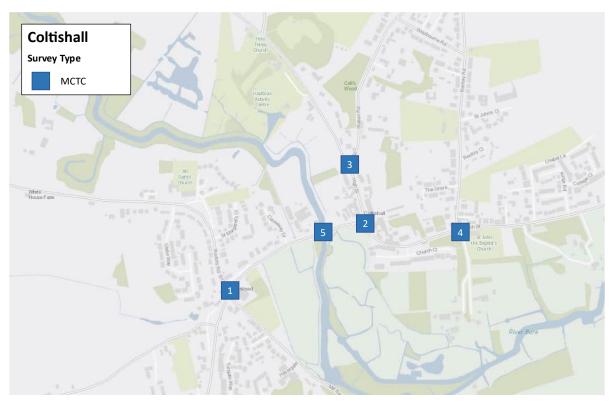


Figure 2-1 - Manual Classified Turning Counts sites

Automatic Traffic Count (ATC) data

- 2.3 The link counts were collected using Automatic Traffic Count (ATC) loops. The ATC data was collected over two weeks between Thursday 10th of November and Wednesday 23rd of November 2022.
- 2.4 Five ATC sites were surveyed in total that have been used to inform the total trip ends at the entry/ entry points to the model. Their locations are shown below in Figure 2-2.



Figure 2-2 – Link counts (Automatic Traffic Counts)

Journey Time Data

2.5 The surveys also captured floating car data for two routes through the modelled area on 30th November 2022. The surveyed journey time routes are shown in Figure 2-3.

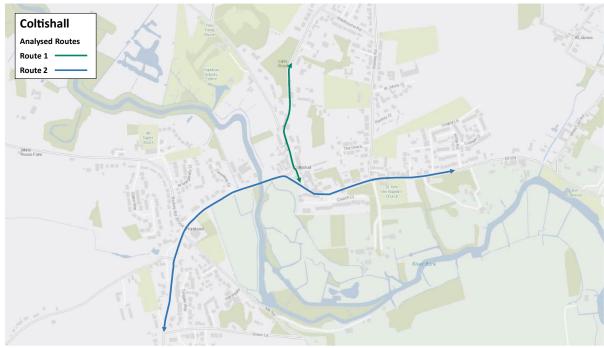


Figure 2-3 Journey Time Routes

Camera Footage

2.6 Camera footage, which was recorded to produce the MCTC and floating car journey time data, was obtained to provide the modellers with a more detailed view of the driving behaviour in the area.

Data Review and Analysis

Consistency Review

- 2.7 The locations of MCTC counts with labelled approach arms and model entry points to assist with the analysis of the data consistency review can be found in Appendix A.
- 2.8 The consistency between the different data sets was assessed to understand the reliability of the data and identify any discrepancies which could affect the model development. The full details of the consistency checks undertaken can be found in Appendix B.
- 2.9 The flow analysis and consistency checks highlighted a small flow difference between some junctions, these differences were below GEH 3 and will not affect the model calibration.
- 2.10 However, the flow difference between the PFS and the Rectory Road/ Norwich Road mini roundabout (Causeway Drive) could be affected by a potential increase in queue length from the bridge. To address this flow difference and ensure the model will capture any detrimental effects on Causeway Drive in the forecast scenarios, an additional model zone was added to represent Causeway Drive, to balance the flows between the junctions.

Peak Hour Analysis

- 2.11 The survey data available was processed to identify the morning and evening peak hours by analysing the profile of traffic volumes during the surveyed period. For this calculation, all vehicle movements have been considered as well as calculations of the inbound flows to the model area.
- 2.12 MCTC data was analysed using two methods to determine the peak hour, by totalling all movements and by totalling only entries in the model area. In the AM period, the peak hour was calculated to be 07.45-08.45, both when considering entries into the modelled area and when using all available data. In the PM period calculations similarly returned a consistent peak hour of 16.30-17.30 using both methods. The ATC data was also analysed and showed the same peak hours as analysis of the MCTC data.

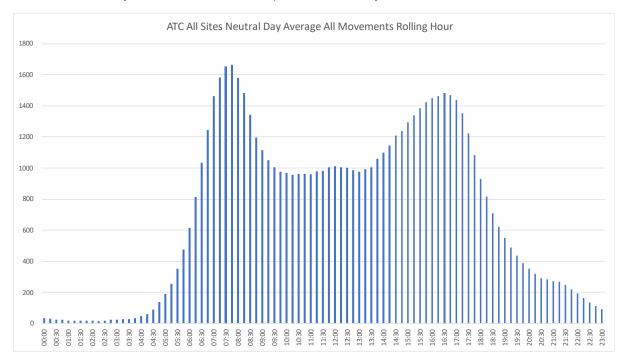


Figure 2-4 ATC Neutral Day Average All Movements Rolling Hour

- 2.13 Based on the assessment of the cumulative hourly flows shown above in Figure 2-4, the following morning and evening peak periods for the general traffic were assumed as follows:
 - Morning Peak (AM): 07:45 to 08:45; and
 - Evening Peak (PM): 16:30 to 17:30.

2.14 The modelled simulation periods include a 15-minute warm-up period to fully saturate the network before the simulated peak hour and a 15-minute cool-down period to allow vehicles to complete their journeys. The modelled periods are therefore:

• AM modelled period: 07:30 - 09:00; and

• PM modelled period: 16:15 - 17:45.

3. Demand Development

Overview

- 3.1 This section describes the demand methodology and the routing analysis undertaken to develop and calibrate the traffic demand and routing in the Vissim Base model.
- 3.2 The model was developed using the dynamic assignment module, as it would allow the model to predict future changes in routing as a consequence of the demand growth, committed schemes or proposed mitigation measures in the area.
- 3.3 The traffic demand has been calculated for each vehicle type included in the model (Car, Light Goods Vehicles (LGV) and Heavy Goods Vehicles (HGV)) for the modelled peak hours. The available survey data has been used to develop the hourly Origin-destination matrices and the 15-minute profiles for each origin zone.

Methodology

- 3.4 To ensure the best possible correlation between the observed data and the Vissim model demand, the vehicle inputs and origin/destination routing have been developed by combining two different components:
 - Prior Matrix This was developed using MCTC turning count proportions to define origin to destination
 routes
 - New Zones Matrix a synthetic zone was added on Causeway Drive, labelled as Zone 2. The demand
 at this zone has been estimated based on the flow differences identified between the adjacent MCTC
 data.
- 3.5 Figure 3-1 shows the location of the defined zones in Vissim. The MCTC sites are labelled with numbers 101-105, whilst the origin zones are labelled with numbers 1-9.



Figure 3-1 Vissim Zone Map

- 3.6 The movements to and from Zone 2, which was added as a synthetic zone, were estimated from flow difference between MCTC-1 and MCTC-5. All other zone movements were estimated through turn proportion data gathered from MCTC surveys.
- 3.7 The final matrix was sense-checked against key movements in the modelled area to ensure accuracy, most notably the movement between Zones 4 to 9, since this is the central corridor which passes through Coltishall, linking North Walsham to Norwich in the south.

Convergence

3.8 The models have been converged using standard convergence criteria from Vissim, although there is no route choice available in the Coltishall model network.

Routing Analysis & Closures

- 3.9 The routing proportions obtained from the convergence process were analysed and reviewed to ensure that there are not unrealistic route patterns included in the model.
- 3.10 Several paths were highlighted as unrealistic and have been closed to prevent abnormal or unrealistic driving behaviour. Some examples of these routes are shown in Figure 3-2 and Figure 3-3.
- 3.11 As shown in Figure 3-2, a route for vehicles travelling northbound on the B1150 which involves looping around the roundabout on Rectory Road to turn onto Mill Road has been closed, since drivers can make a direct right-turn onto Mill Road before the roundabout.



Figure 3-2 Closed route at Rectory Road roundabout

3.12 As shown in Figure 3-3, a route for vehicles travelling from the B1150 onto the High Street which involves a circulating around the petrol station has been closed, since drivers can make continue straight onto the high street instead.



Figure 3-3 Closed route at petrol station gyratory

4. Network Development

Network coding

- 4.1 Scaled Bing maps within Vissim have been used to code the network geometry and structure, such as number of lanes and flare lengths and reference was also made to Google Maps and Streetview to ensure the network reflects conditions on the ground.
- 4.2 Observation from the video footage available have also been used to inform the network coding and replicate the operation of the existing layout.

Desired Speed Decisions

- 4.3 Desired Speed Decisions, defining the speed distribution that vehicles follow at each point of the network, have been updated to represent the posted speed limits for each link.
- 4.4 The speed distributions used in the model, and the variability that a group of vehicles show at the same speed limit, have been obtained from two different sources. The Guidelines for the Use of Microsimulation Software from National Highways provide distributions for 50 mph and 70 mph, while 30 mph and 60 mph have been obtained from the SPE0111 Vehicle Speed Compliance by road type and vehicle type in Great Britain from the Department for Transport (DfT).
- 4.5 40mph distributions have been obtained by interpolation between the 30 mph and the 50 mph distributions. The 30 mph, 40 mph and 50 mph distributions are shown in Appendix C.
- 4.6 It should be noted that the speed distribution for 20mph included in the models has been calculated using the journey time data on the section operating in free flow conditions.

Reduced Speed Areas

- 4.7 Reduced Speed Areas (RSAs) have been included to replicate driving behaviour, for example on curved roads and turns onto roads.
- 4.8 RSA have also been used to represent specific behaviours observed in the model area. It should be noted that additional RSAs have been coded in the PM model to represent the queuing patterns observed on the High Street. These queues are caused by parked cars which were only observed in the PM peak and these RSAs have not been included in the AM peak hour model, as the parked vehicles were not present.

Priority Rules and Conflict areas

- 4.9 Priority Rules and Conflict Areas have been coded following the industry standard approach and were calibrated to replicate the observed network conditions and driver behaviour.
- 4.10 Priority rules have also been used to represent the give way operation observed on the Norwich Road bridge, where large vehicles give way to each other as they cannot pass over the bridge at the same time.
- 4.11 It should be noted that additional priority rules were coded in the PM model to reflect the observed queuing and give way behaviour on the High Street. The floating car journey time video footage was used to observe give way behaviour, which was replicated in the model, so the queues caused by the parked cars in the PM peak are replicated.

Public Transport

4.12 Bus routes and departure times included in the modelled area were sourced from the website https://bustimes.org/. An average dwell time of ten seconds was assumed for all bus stops in the model.

Differences between AM and PM model networks

4.13 Some limited differences between the AM and PM peak hour models were coded to replicate the operation of the High Street, where the queues, delays and give way behaviour caused by the parked cars along this route were only present in the PM peak hour.

5. Model Calibration

Introduction

5.1 The purpose of the model calibration process is to ensure that the model represents existing traffic conditions. Calibration is an iterative process in which the model is revised to replicate observed traffic volumes, traffic conditions and vehicle behaviour as closely as possible.

Flow Calibration Criteria

- 5.2 This section presents the traffic flow calibration and the comparison between the modelled and observed traffic flows using the criteria provided in TAG Unit M3-1.
- 5.3 The observed and modelled turning flows were compared for each of the junctions for the AM and PM peak hours, using the TAG criteria (Unit M3.1) for flow calibration as shown in Table 1.

Table 1 - TAG Calibration Criteria

Criteria	Acceptability Guidelines
Criteria 1 - % Flows	
 a. Individual flows within 15% for flows 700-2700 vph b. Individual flows within 100 vph for flows < 700 vph c. Individual flows within 400 vph for flows > 2700 vph 	> 85% of all cases
Criteria 2 – GEH Criteria	
a. GEH Statistic -Individual flows: GEH < 5	

- 5.4 The differences between modelled and observed flows were calculated and the TAG criteria, both for absolute differences and for GEH statistic, were used to determine if these differences were acceptable. The GEH statistic incorporates both relative and the absolute differences and provides a better indication of the significance of differences, compared to using percentage differences which can be misleading.
- 5.5 The GEH statistic is defined as:

GEH=
$$\sqrt{\frac{(M-C)^2}{(M+C)/2}}$$
 , where M and C are different datasets to be compared.

Flow Calibration Results

- 5.6 The modelled turning flows were compared against the surveyed turning flows to calibrate the demand inputs and model assignment. The models were run twenty times using different random seeds to produce a set of average turning count results for comparison with the survey data.
- 5.7 The structure of the junctions and turning counts references within the model area can be seen in Appendix A, whilst tables indicating the GEH scores can be found in Appendix D.
- 5.8 The AM calibration results in Table 2 show the calibration results for each vehicle type. The results demonstrate that the AM peak hour flows are calibrated closely against the observed turning counts when analysed vehicle class, and all exceed the thresholds set out in TAG.

Table 2 – AM Calibration Results - Peak Hour by Vehicle Class

Vehicle Class	Tag Criteria	Within	Total Counts	Percentage Passing
Coro	% Counts within GEH <5	50	50	100%
Cars	% Flows within Individual Flow	50	50	100%
LGVS	% Counts within GEH <5	50	50	100%
	% Flows within Individual Flow	50	50	100%

Vehicle Class	Tag Criteria	Within	Total Counts	Percentage Passing
HGVs	% Counts within GEH <5	50	50	100%
HGVS	% Flows within Individual Flow	50	50	100%
Total	% Counts within GEH <5	50	50	100%
	% Flows within Individual Flow	50	50	100%

- 5.9 The AM calibration results in Table 3 show the calibration results for total vehicles entering the model. Although not required in TAG, explicitly matching the observed number of vehicles entering the network is a key metric to validate the capacity and delays of the microsimulation models.
- 5.10 The results demonstrate that all entry junctions into the model are calibrated closely with observed data. It has therefore been checked that the correct number of vehicles are entering the model.

Table 4 - AM Peak Hour Calibration results - Model Entries

From	Observed	Modelled	% Diff.
Mill Road	20	20	0.0%
B1150 / Norwich Road (EB)	637	634	-0.5%
B1354 / Buxton Road	255	249	-2.4%
Station Road	527	523	-0.8%
Great Hautbois Road	10	10	0.0%
Rectory Road	58	56	-3.4%
B1354 / Wroxham Road (WB)	285	280	-1.8%
Church Loke	8	8	0.0%

5.11 The calibration summary in Table 5 demonstrates that the PM peak hour model flows are also closely calibrated against the observed turning counts when analysed by vehicle class, exceeding the requirements set out in TAG

Table 5 - PM Calibration Results - Peak Hour by Vehicle Class

Vehicle Class	Tag Criteria	Within	Total Counts	Percentage Passing
C	% Counts within GEH <5	50	50	100%
Car	% Flows within Individual Flow	50	50	100%
LCV	% Counts within GEH <5	50	50	100%
LGV	% Flows within Individual Flow	50	50	100%
HGV	% Counts within GEH <5	50	50	100%
пGV	% Flows within Individual Flow	50	50	100%
Total	% Counts within GEH <5	50	50	100%
	% Flows within Individual Flow	50	50	100%

5.12 The PM calibration results in Table 6 shows the calibration results for total vehicles entering the model. The results demonstrate that all entry junctions into the model are calibrated closely with observed data. It has therefore been checked that the correct number of vehicles are entering the model.

Table 6 - PM Peak Hour Calibration Results - Model Entries

From	Observed	Modelled	% Diff.
Mill Road	21	20	-4.8%
B1150 / Norwich Road (EB)	730	715	-2.1%
B1354 / Buxton Road	200	197	-1.5%
Station Road	427	418	-2.1%

From	Observed	Modelled	% Diff.
Great Hautbois Road	36	34	-5.6%
Rectory Road	44	43	-2.3%
B1354 / Wroxham Road (WB)	305	302	-1.0%
Church Loke	4	4	0.0%

Calibration Parameters

5.13 Table 7 summarises the main calibration and specific driving behaviour parameters recommended by TAG and DfT for microsimulation models. These parameters have been included in the Coltishall Vissim model in line with the recommended guidance.

Table 7 – Microsimulation Model Parameters – TAG/DfT

Parameter	Value	Following guidance
Headway	1s time	Yes
Gap	1 to 4 seconds, depends on location.	Yes
Vehicle Dynamics	Following graphs	Yes
Reaction Time	-	-
Desired Speed Distributions	Following graphs	Yes
Driver Awareness	Following graphs	Yes
Influence of signing on the approach to a diverge of the motorway lane selection	5	Yes
Cooperative Merging	Yes, used on merging and weaving links.	Yes
	Maximum speed difference - 6.71mph	
	Maximum collision time – 10s	
Implied Capacity at roundabouts and signal stop lines	-	-
Min Distance between vehicles at a standstill	1.5m	Yes

6. Model Validation

Introduction

- 6.1 Following the model calibration process, the VISSIM models were validated using journey time data. The vehicle travel time results from the models were compared against the surveyed journey time data to validate the queuing and delay in the model. The models were run twenty times using different random seeds to produce a set of average journey time results for comparison with the survey data.
- 6.2 The TAG M3-1 criteria for journey time validation are shown in Table 8 below.

Table 8 - TAG Validation Criteria

Criteria	Acceptability Guidelines
Modelled times along routes should be within 15% of surveyed times (or 1 minute, if higher than 15%)	> 85% of routes

Journey Time Validation Results

6.3 Figure 6-1 shows the two journey time routes which have been defined within the model area. The average observed journey times were compared to the average modelled journey times in accordance with the criteria set out in TAG M3-1. The journey times routes were defined using the GPS position of the floating car video footage used to capture the observed journey time data.



Figure 6-1 Coltishall Routes

6.4 Table 9 and Table 10 show the individual performance of each of the defined journey time routes for all vehicles, all of which pass the TAG criteria.

Table 9 – AM Journey Time Validation

ID Route Name Observed Modelled % Difference Validation

1	JT1_SB	58	62	7%	Yes
2	JT1_NB	75	70	-6%	Yes
3	JT2_EB	174	175	1%	Yes
4	JT2_WB	154	165	7%	Yes

Table 10 – PM Journey Time Validation

ID Route Name Observed Modelled % Difference Validation

1	JT1_SB	102	102	0%	Yes
2	JT1_NB	96	88	-8%	Yes
3	JT2_EB	187	176	-6%	Yes
4	JT2_WB	151	164	9%	Yes

6.5 Figure 6-2 to Figure 6-7 show the cumulative journey time profiles of these routes with the maps and observed data for both peaks. It can be seen that the models closely replicate the profile of delay along the modelled routes.

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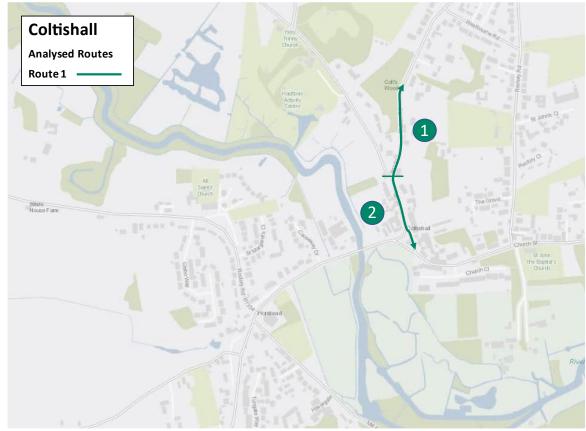


Figure 6-2 - Route 1 SB Map

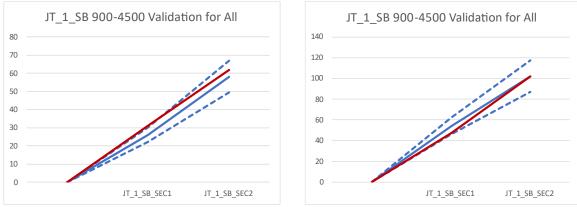


Figure 6-3 – Route 1 SB journey time validation profiles

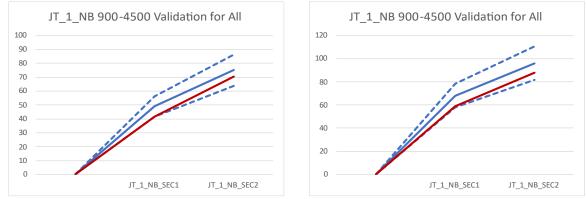


Figure 6-4 - Route 1 NB journey time validation profiles

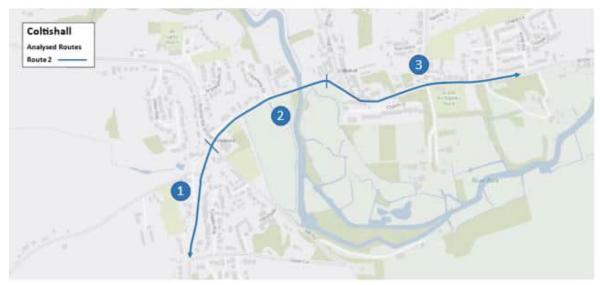
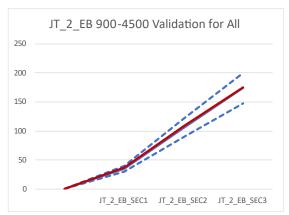


Figure 6-5 - Route 2 EB Map



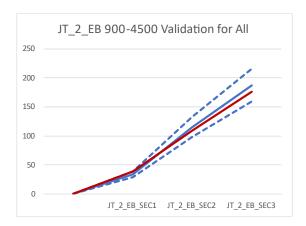
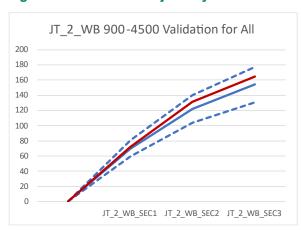


Figure 6-6 – Route 2 EB journey time validation profiles



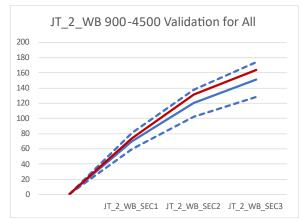


Figure 6-7 – Route 2 WB journey time validation profiles

Queue Calibration

- 6.6 In addition to the journey time validation of the model, TAG recommends a review of the representation of existing queues in the model. Although journey times provide a more accurate representation of the existing delays, the visual comparison of the queue patterns in the area provides further reassurance that the model represents the operation of the network.
- Two main sources have been used to define the main queues of the model: the floating car footage of driving behaviour in Coltishall and the typical travel speed information taken from Google Maps.

AM Peak Hour

6.8 The main queue in the AM period occurs on the B1150 as traffic approaches the petrol station from the southwest. This queueing behaviour can be seen in Figure 6-8, which was captured from floating car footage of Route 2, this was a moving queue caused by right turning vehicles waiting to turn into the B1150 northwards.



Figure 6-8 - Floating car footage of AM queuing on B1150

6.9 Figure 6-9 shows the typical traffic conditions according to Google Maps on a Tuesday at 08:30. Figure 6-10 shows the peak hour average speed plot from the AM model, where it can be observed that a similar queue is present.

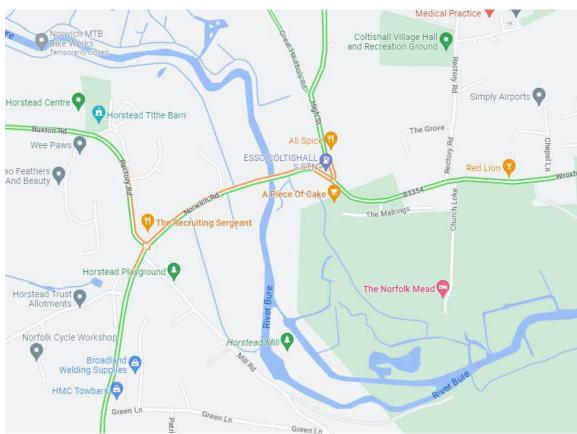


Figure 9 - Typical queues from Google traffic on a Wednesday, 08:30



Figure 10 - AM Peak Hour Speed Plot

PM Peak Hour

6.10 The main queue in PM period occurs on the High Street, where parked cars prevent the free flow of traffic in both directions simultaneously. The presence of parked cars can be seen in Figure 6-11, taken from a Google StreetView. This image shows that cars are parked on both sides of the street, which limits the road space available for vehicles to pass. Figure 6-12 is a still taken from the floating car footage of the Route 1 southbound journey in the PM period which shows how parked cars impede the free flow of traffic in both directions.



Figure 6-11-1 Parked cars on High Street



Figure 6-12 PM queuing on High Street, from floating car footage

6.11 Figure 6-13 shows the typical traffic conditions according to Google Maps on a Tuesday at 16:40, whilst Figure 6-14 shows the modelled queues during the PM peak, where this queuing is replicated.

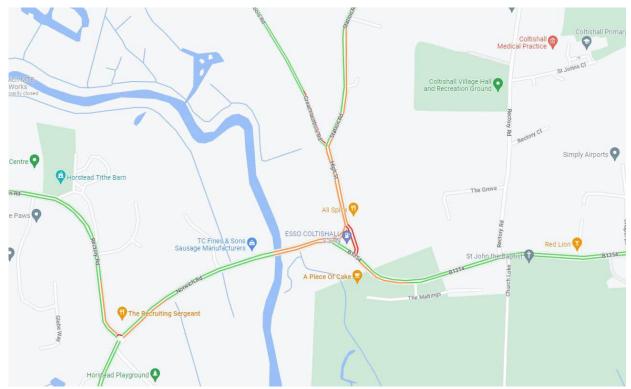


Figure 6-13 – Google traffic view captured on a Monday at 16:40



Figure 6-14 – PM peak hour Speed Plot

Model Variability

- 6.12 Microsimulation models are run several times with different random seeds to obtain a statistically representative result. This approach replicates daily variability, since each run has different arrival profiles which results in a different chain of events. A representative average of the results is the obtained/ presented.
- 6.13 The survey videos show that the queues on the High Street in the PM period can be highly variable since they can appear and disappear in short periods of time.
- 6.14 A variability analysis of the modelling journey times results has been undertaken in this section. Figure 6-15 shows the modelled journey times for Route 1 SB in the PM period for all of the model runs, whilst Figure 6-16 shows the modelled journey times for Route 1 NB in the PM period for all the model runs.

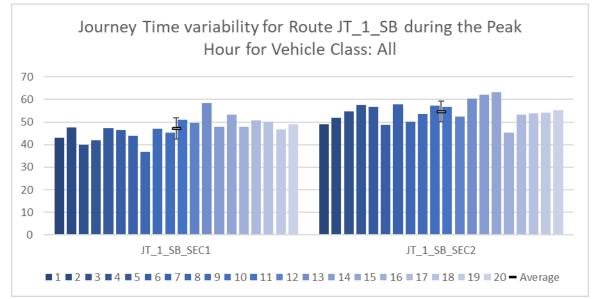


Figure Error! No text of specified style in document.-2 - Route 1 SB modelled journey times

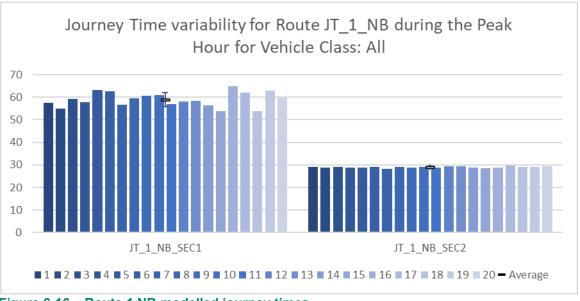


Figure 6-16 – Route 1 NB modelled journey times

6.15 As can be seen in these graphs, the modelled journey times in the PM peak are variable, particularly in the southbound direction. This variability is caused by parked cars on the High Street and the subsequent give way behaviour and queuing. This phenomenon has been replicated in the model, replicating the variability seen in the surveys.

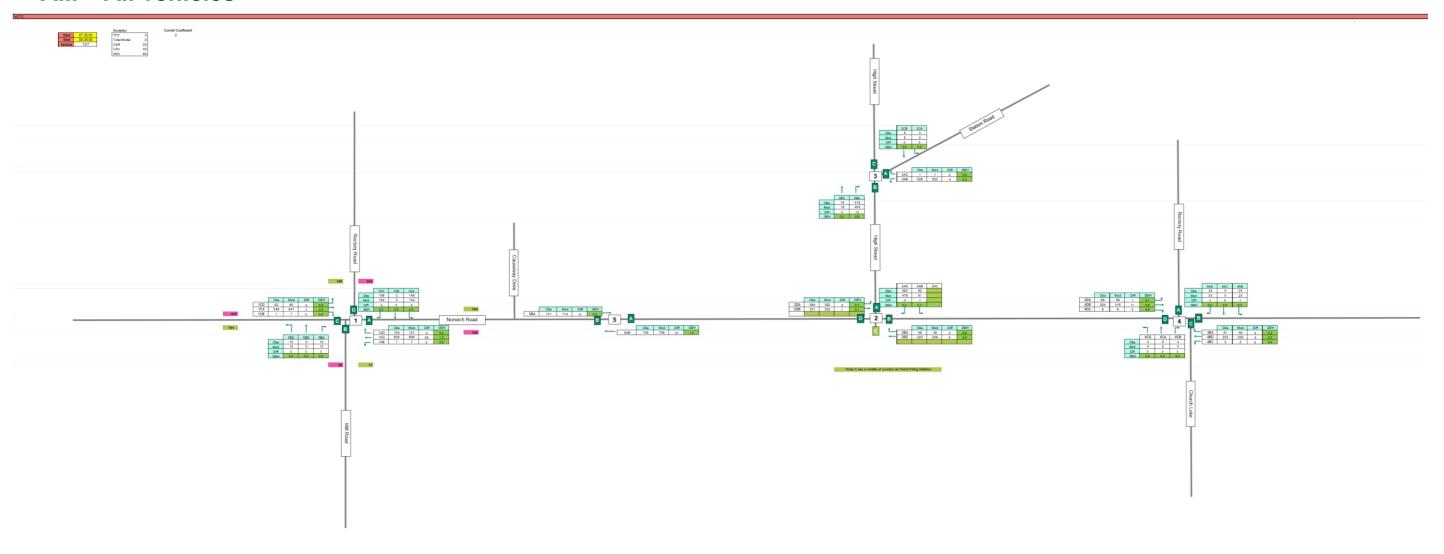
7. Conclusion

- 7.1 Coltishall is a village located on the B1150 between Norwich and North Walsham and the road network is therefore busy at peak times. In the AM period there is a small amount of congestion on the eastbound approach to the petrol station due to the vehicles waiting to turn right into B1150 northwards, as explained in paragraph 6.8, whilst in the PM period parked cars on the High Street were seen to cause a significant amount of queuing, particularly in the southbound direction.
- 7.2 The base models have been calibrated and validated against the observed data in line with the required criteria. The calibration/validation results exceed the requirements for turning counts and journey times and the models are therefore closely aligned with observed data. The models also replicate observed queueing patterns well. The models are therefore validated to industry standard guidelines.
- 7.3 It is considered the base models provide a close representation of the queues and delays in the network, as well as the observed driving behaviour in the area, and are fit for the purpose of testing future traffic levels/ patterns or potential changes to the road network.

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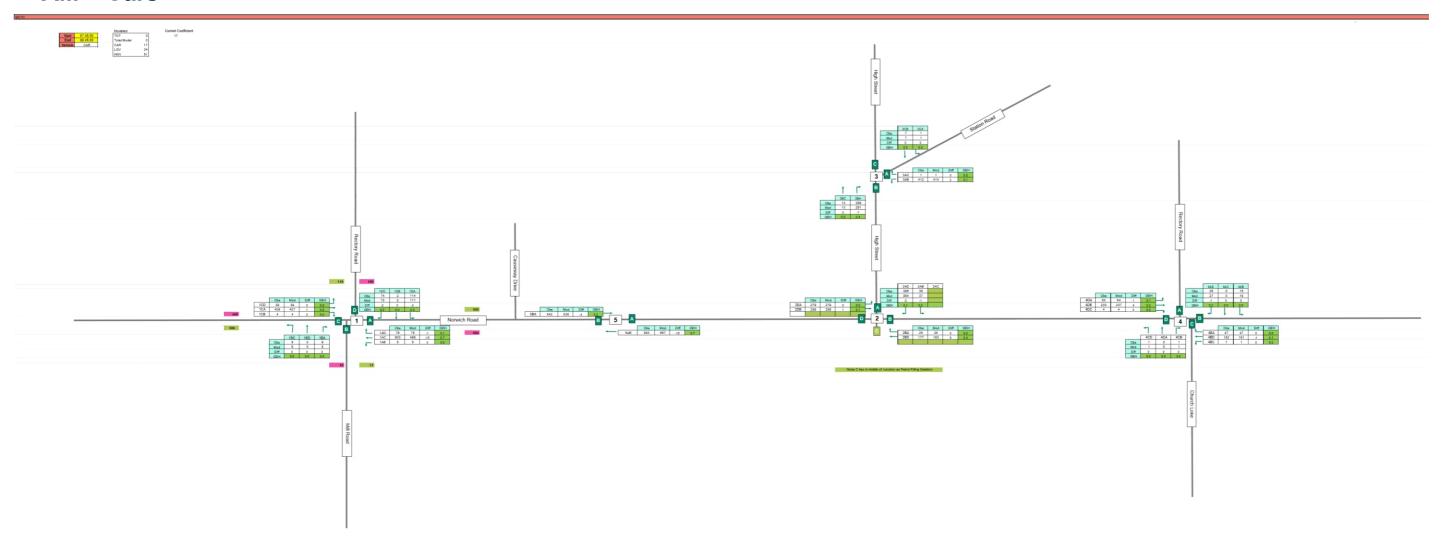
Appendix A MCTC Turning Counts

AM - All vehicles



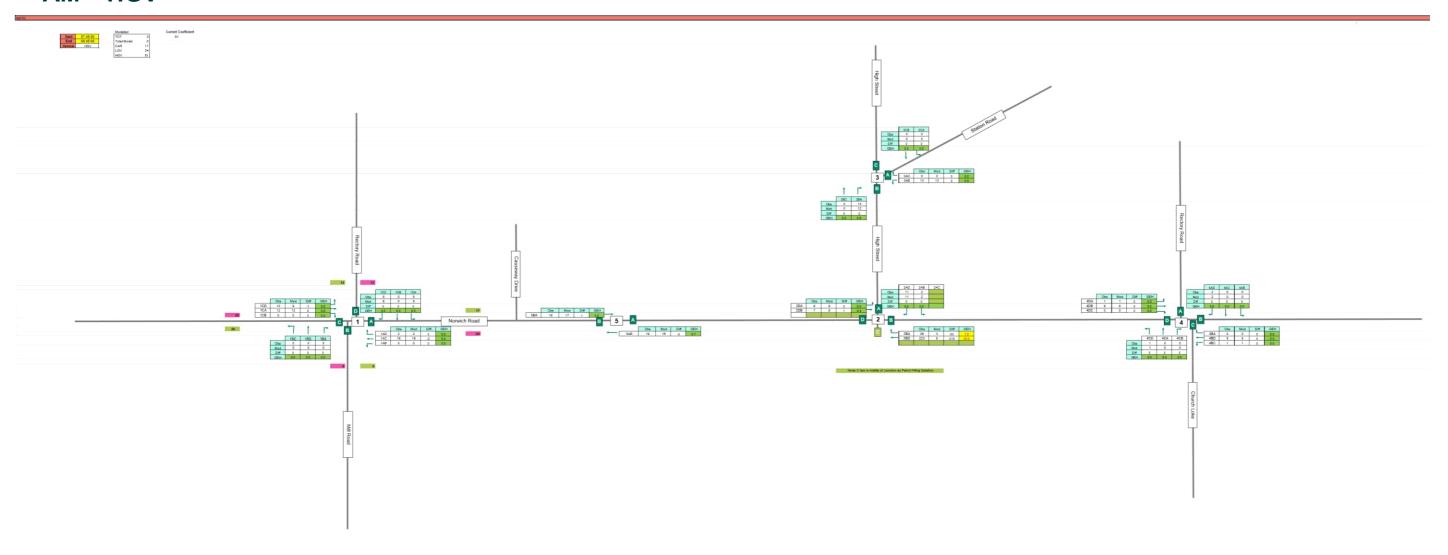
AECOM 30 Prepared for: The Client Group

AM - Cars



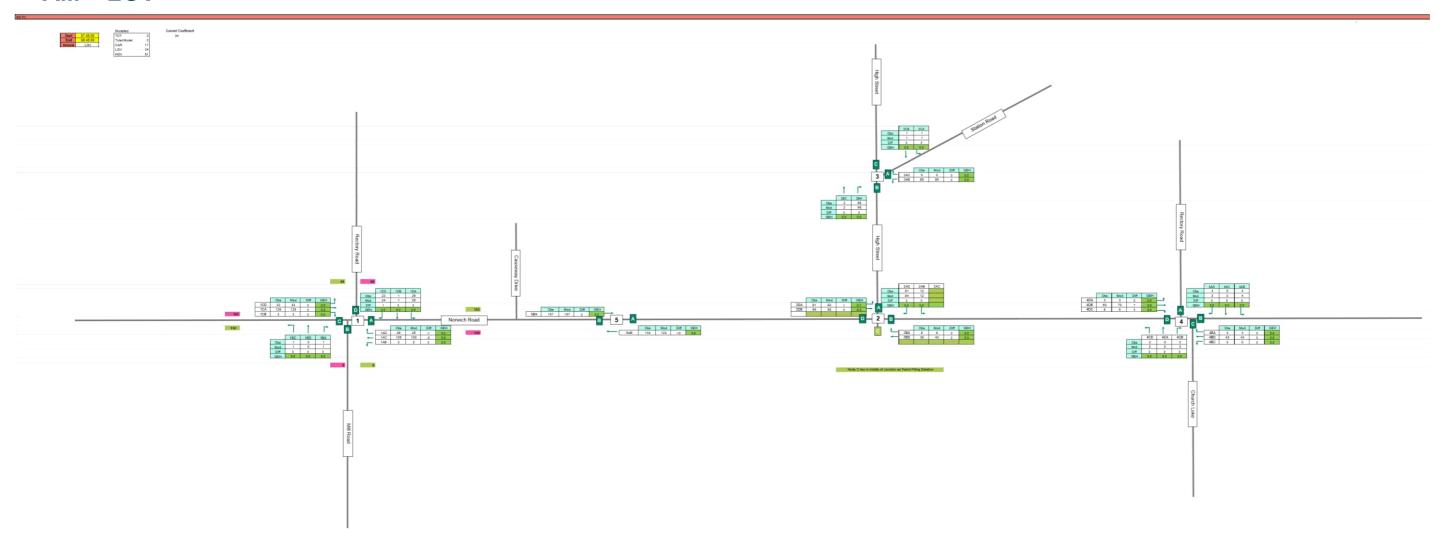
AECOM 31 Prepared for: The Client Group

AM – HGV



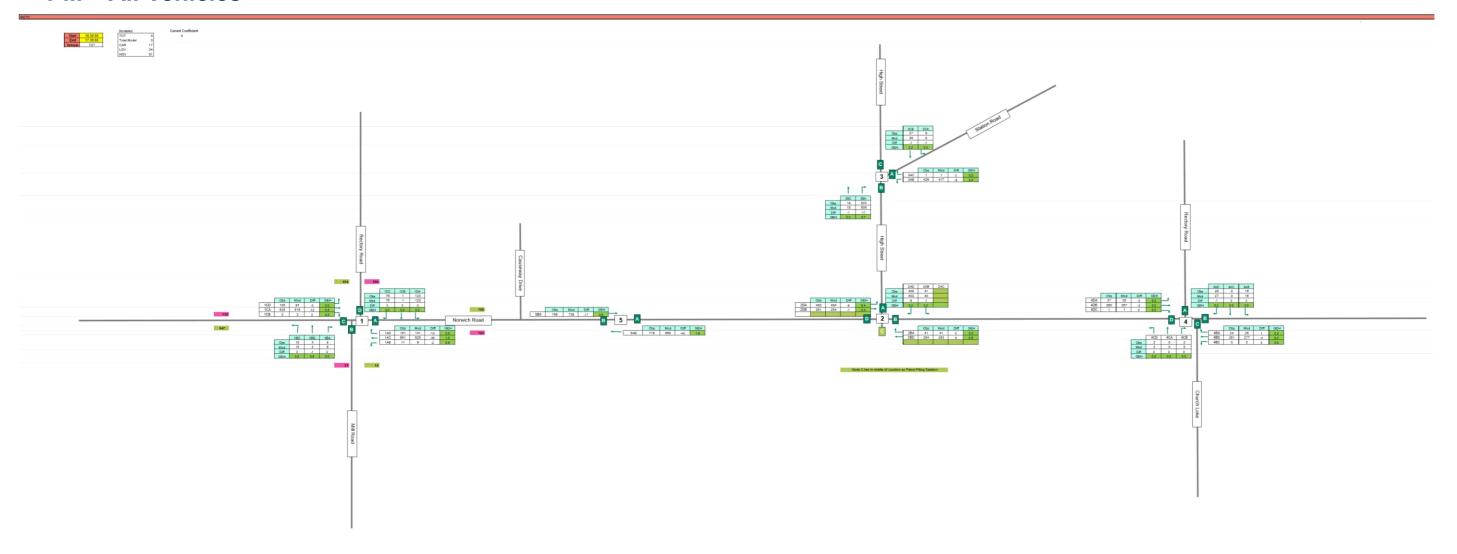
AECOM 32 Prepared for: The Client Group

AM – LGV



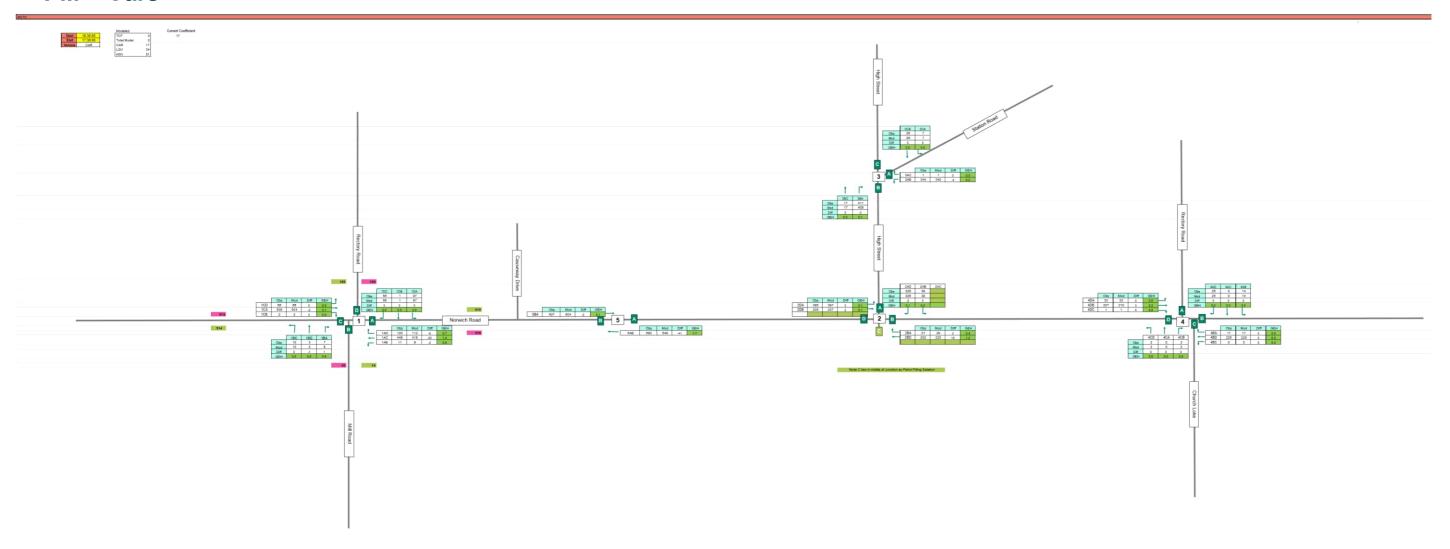
AECOM 33 Prepared for: The Client Group

PM - All Vehicles



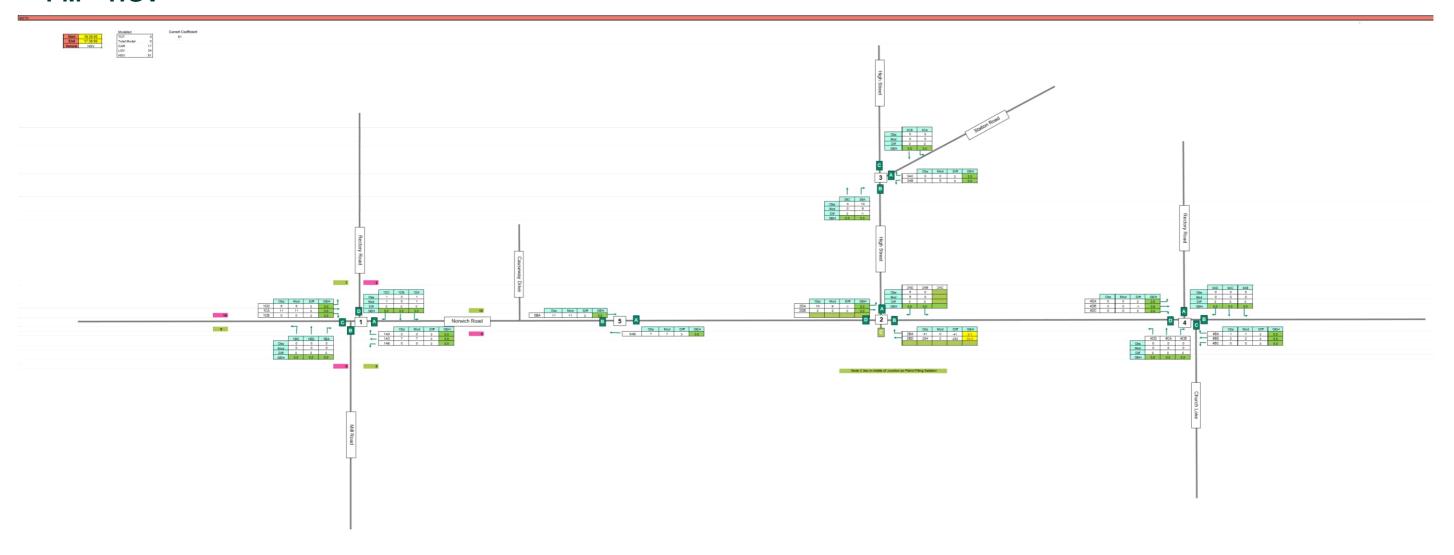
AECOM 34 Prepared for: The Client Group

PM - Cars



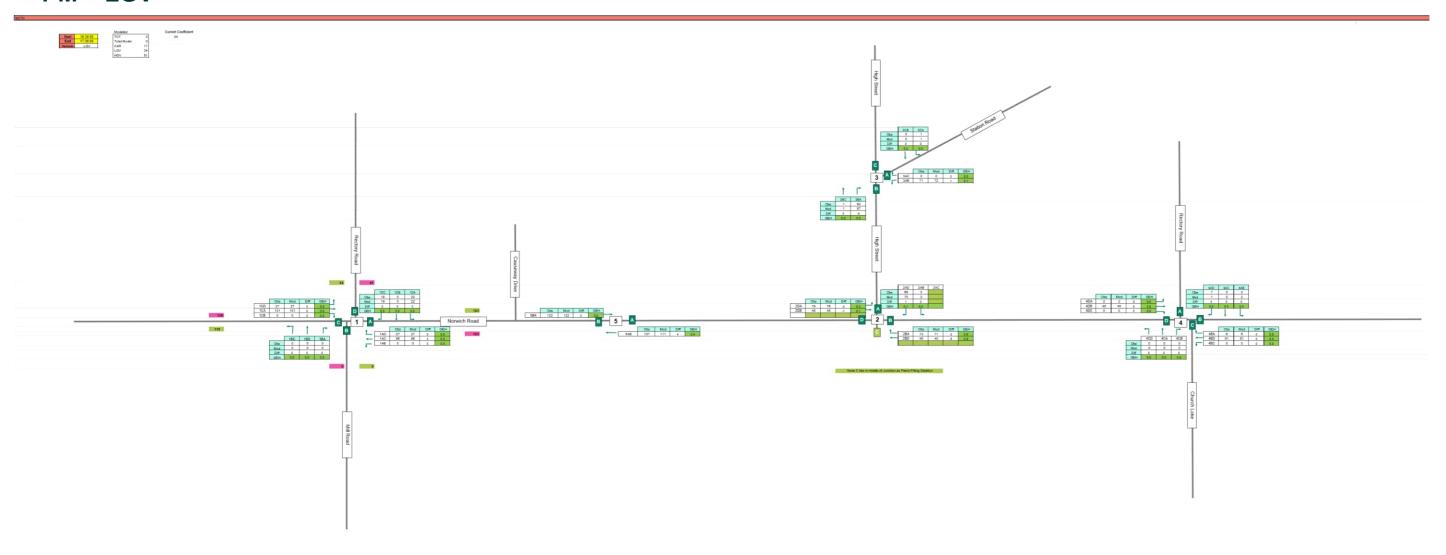
AECOM 35 Prepared for: The Client Group

PM – HGV



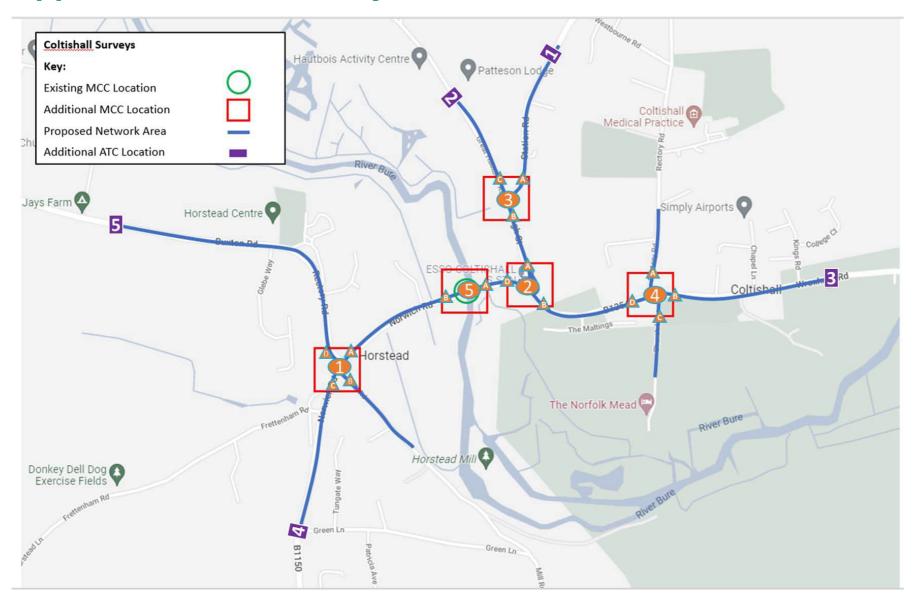
AECOM 36 Prepared for: The Client Group

PM – LGV



AECOM 37 Prepared for: The Client Group

Appendix B Consistency Checks



Fr	om	Traffic	Flow	to		Traffic	Flow	Differ	ence	GEH	
Site	Arm	CAR	LGV	Site	Arm	CAR	LGV	CAR	LGV	CAR	LGV
1	Α	3398	714	5	В	3390	701	8	13	0.1	0.5
5	В	3410	809	1	А	3427	788	-17	21	0.3	0.7
5	Α	3390	701	2	D	3312	659	78	42	1.3	1.6
2	D	3403	808	5	Α	3410	809	-7	-1	0.1	0.0
2	Α	2384	474	3	В	2339	472	45	2	0.9	0.1
3	В	2343	549	2	А	2348	558	-5	-9	0.1	0.4
2	В	1383	288	4	D	1405	266	-22	22	0.6	1.3
4	D	1481	334	2	В	1556	357	-75	-23	1.9	1.2

Prepared for: The Client Group

Appendix C Desired Speed Distributions

Description	Posted Limit		Normal Distribut	ributions (mph)			
		LV	/s	ŀ	HVs		
		Lower	Upper	Lower	Upper		
DfT's Motorways	70	50	89	50	89		
DfT's Dual Carriageways	70	58	80	48	80		
DfT's Single Carriageways	60	20	70	20	69		

Prepared for: The Client Group

Appendix D Turning Count Calibration Tables

AM - All vehicles

VISSIM Node 101 Vehicle Type Total

		Node						Flow Peak	Гime	Differen	ice		GEH	
Junction Name	MCC Site	No.	From Arm	FromLink	To Arm	ToLink	MCC ID	Observed	Modelled	Value	%	Value	<5	Individual Flows
Rectory Road roundabout	1	101	А	38	Α	3	1AA	0	2	2	-	2	Υ	OK
Rectory Road roundabout	1	101	Α	38	В	19	1AB	7	7	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	А	38	С	22	1AC	635	605	-30	-5%	1	Υ	OK
Rectory Road roundabout	1	101	Α	38	D	18	1AD	104	101	-3	-3%	0	Υ	OK
Rectory Road roundabout	1	101	В	20	Α	3	1BA	10	10	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	В	20	В	19	1BB	0	0	0	-	0	Υ	OK
Rectory Road roundabout	1	101	В	20	С	22	1BC	10	10	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	В	20	D	18	1BD	0	0	0	-	0	Υ	OK
Rectory Road roundabout	1	101	С	1	Α	3	1CA	548	547	-1	0%	0	Υ	OK
Rectory Road roundabout	1	101	С	1	В	19	1CB	7	7	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	С	1	С	22	1CC	0	0	0	-	0	Υ	OK
Rectory Road roundabout	1	101	С	1	D	18	1CD	82	80	-2	-2%	0	Υ	OK
Rectory Road roundabout	1	101	D	17	Α	3	1DA	146	142	-4	-3%	0	Υ	OK
Rectory Road roundabout	1	101	D	17	В	19	1DB	3	3	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	D	17	С	22	1DC	106	104	-2	-2%	0	Υ	OK
Rectory Road roundabout	1	101	D	17	D	18	1DD	0	0	0	-	0	Υ	OK

Vehicle Type Total **VISSIM Node** 102

		Node					MCC	Flow Pea	ak Time	Diffe	rence		GEH	
Junction Name	MCC Site	No.	From Arm	FromLink	To Arm	ToLink	ID	Observed	Modelled	Value	%	Value	<5	Individual Flows
Petrol Station Gyratory	2	102	Α	10011	А	15	2AA	0	0	0	-	0	Υ	OK
Petrol Station Gyratory	2	102	Α	10011	В	10	2AB	52	51	-1	-2%	0	Υ	OK
Petrol Station Gyratory	2	102	Α	34	D	12	2AD	483	479	-4	-1%	0	Υ	OK
Petrol Station Gyratory	2	102	В	11	Α	15	2BA	36	36	0	0%	0	Υ	OK
Petrol Station Gyratory	2	102	В	11	В	10	2BB	0	0	0	-	0	Υ	OK
Petrol Station Gyratory	2	102	В	11	D	12	2BD	223	229	6	3%	0	Υ	OK
Petrol Station Gyratory	2	102	D	37	Α	15	2DA	384	382	-2	-1%	0	Υ	OK
Petrol Station Gyratory	2	102	D	37	В	10	2DB	331	332	1	0%	0	Υ	OK
Petrol Station Gyratory	2	102	D	37	D	12	2DD	0	1	1	-	1	Υ	OK

VISSIM Node 103 Vehicle Type Total Flow Peak Time MCC Site **Junction Name** From Arm FromLink To Arm **ToLink** Difference GEH

AECOM 40 Prepared for: The Client Group

		Node					МСС	Observati	Note all all and	Value	0/	Walter	_	Individual
		No.					ID	Observed	Modelled	value	%	Value	<5	Flows
Great Hautbois Road / Station Road	3	103	Α	4	Α	33	3AA	0	0	0	-	0	Υ	OK
Great Hautbois Road / Station Road	3	103	Α	4	В	34	3AB	526	522	-4	-1%	0	Υ	OK
Great Hautbois Road / Station Road	3	103	Α	4	С	31	3AC	1	1	0	0%	0	Υ	OK
Great Hautbois Road / Station Road	3	103	В	15	Α	33	3BA	415	403	-12	-3%	1	Υ	OK
Great Hautbois Road / Station Road	3	103	В	15	В	34	3BB	0	0	0	•	0	Υ	OK
Great Hautbois Road / Station Road	3	103	В	15	С	31	3BC	15	15	0	0%	0	Υ	OK
Great Hautbois Road / Station Road	3	103	С	32	Α	33	3CA	2	2	0	0%	0	Υ	OK
Great Hautbois Road / Station Road	3	103	С	32	В	34	3CB	8	8	0	0%	0	Υ	OK
Great Hautbois Road / Station Road	3	103	С	32	С	31	3CC	0	0	0	•	0	Υ	OK

Vehicle Type Total **VISSIM Node** 104

		Node					MCC	Flow Pea	ak Time	Diffe	rence		GEH	
Junction Name	MCC Site	Node No.	From Arm	FromLink	To Arm	ToLink	MCC ID	Observed	Modelled	Value	%	Value	< 5	Individual Flows
Church Loke	4	104	А	24	Α	23	4AA	0	0	0	-	0	Υ	OK
Church Loke	4	104	Α	24	В	29	4AB	24	23	-1	-4%	0	Υ	OK
Church Loke	4	104	Α	24	С	27	4AC	0	0	0	-	0	Υ	OK
Church Loke	4	104	Α	24	D	26	4AD	34	33	-1	-3%	0	Υ	OK
Church Loke	4	104	В	6	Α	23	4BA	51	49	-2	-4%	0	Υ	OK
Church Loke	4	104	В	6	В	29	4BB	0	0	0	-	0	Υ	OK
Church Loke	4	104	В	6	С	27	4BC	2	2	0	0%	0	Υ	OK
Church Loke	4	104	В	6	D	26	4BD	232	229	-3	-1%	0	Υ	OK
Church Loke	4	104	С	28	Α	23	4CA	0	0	0	-	0	Υ	OK
Church Loke	4	104	С	28	В	29	4CB	4	4	0	0%	0	Υ	OK
Church Loke	4	104	С	28	С	27	4CC	0	0	0	-	0	Υ	OK
Church Loke	4	104	С	28	D	26	4CD	4	4	0	0%	0	Υ	OK
Church Loke	4	104	D	10	Α	23	4DA	58	59	1	2%	0	Υ	OK
Church Loke	4	104	D	10	В	29	4DB	304	315	11	4%	1	Υ	OK
Church Loke	4	104	D	10	С	27	4DC	9	9	0	0%	0	Υ	OK
Church Loke	4	104	D	10	D	26	4DD	0	0	0	-	0	Υ	OK

VISSIM Node Vehicle Type Total 105

		Mada					MCC	Flow Pea	ak Time	Diffe	rence		GEH	
Junction Name	MCC Site	Node No.	From Arm	FromLink	To Arm	ToLink	MCC ID	Observed	Modelled	Value	%	Value	<5	Individual Flows
B1150 Bridge	5	105	А	12	А	37	5AA	0	0	0	-	0	Υ	OK
B1150 Bridge	5	105	Α	12	В	12	5AB	745	708	-37	-5%	1	Υ	OK
B1150 Bridge	5	105	В	37	Α	37	5BA	721	713	-8	-1%	0	Υ	OK
B1150 Bridge	5	105	В	37	В	12	5BB	0	0	0	-	0	Υ	OK

AM - Cars

VISSIM Node	101	Vehicle Type Car		
Junction Name		From Arm Fromlink To Arm	Tol ink MCC ID Flow Peak Time	Difference GFH

AECOM 41 Prepared for: The Client Group

	MCC Site	Node No.						Observed	Modelled	Value	%	Value	<5	Individual Flows
Rectory Road roundabout	1	101	А	38	A	3	1AA	0	1	1	-	1	Y	OK
Rectory Road roundabout	1	101	Α	38	В	19	1AB	5	5	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	Α	38	С	22	1AC	503	488	-15	-3%	1	Υ	OK
Rectory Road roundabout	1	101	А	38	D	18	1AD	76	75	-1	-1%	0	Υ	OK
Rectory Road roundabout	1	101	В	20	Α	3	1BA	9	9	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	В	20	В	19	1BB	0	0	0	-	0	Υ	OK
Rectory Road roundabout	1	101	В	20	С	22	1BC	9	9	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	В	20	D	18	1BD	0	0	0	-	0	Υ	OK
Rectory Road roundabout	1	101	С	1	Α	3	1CA	406	407	1	0%	0	Υ	OK
Rectory Road roundabout	1	101	С	1	В	19	1CB	4	4	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	С	1	С	22	1CC	0	0	0	-	0	Υ	OK
Rectory Road roundabout	1	101	С	1	D	18	1CD	39	39	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	D	17	А	3	1DA	114	111	-3	-3%	0	Υ	OK
Rectory Road roundabout	1	101	D	17	В	19	1DB	2	2	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	D	17	С	22	1DC	74	72	-2	-3%	0	Υ	OK
Rectory Road roundabout	1	101	D	17	D	18	1DD	0	0	0	-	0	Υ	OK

Vehicle Type Car 102 **VISSIM Node**

	мсс	Node						Flow Pe	ak Time	Diffe	rence		GEH	
Junction Name	Site	No.	From Arm	FromLink	To Arm	ToLink	MCC ID	Observed	Modelled	Value	%	Value	<5	Individual Flows
Petrol Station Gyratory	2	102	Α	10011	А	15	2AA	0	0	0	-	0	Υ	OK
Petrol Station Gyratory	2	102	Α	10011	В	10	2AB	38	37	-1	-3%	0	Υ	OK
Petrol Station Gyratory	2	102	А	34	D	12	2AD	386	384	-2	-1%	0	Υ	OK
Petrol Station Gyratory	2	102	В	11	Α	15	2BA	25	25	0	0%	0	Υ	OK
Petrol Station Gyratory	2	102	В	11	В	10	2BB	0	0	0	-	0	Υ	OK
Petrol Station Gyratory	2	102	В	11	D	12	2BD	177	183	6	3%	0	Υ	OK
Petrol Station Gyratory	2	102	D	37	Α	15	2DA	279	279	0	0%	0	Υ	OK
Petrol Station Gyratory	2	102	D	37	В	10	2DB	258	259	1	0%	0	Υ	OK
Petrol Station Gyratory	2	102	D	37	D	12	2DD	0	1	1	-	1	Υ	OK

VISSIM Node 103 Vehicle Type Car

	MCC	Mode						Flow Pe	ak Time	Diffe	rence		GEH	
Junction Name	MCC Site	Node No.	From Arm	FromLink	To Arm	ToLink	MCC ID	Observed	Modelled	Value	%	Value	<5	Individual Flows
Great Hautbois Road / Station Road	3	103	А	4	А	33	3AA	0	0	0	-	0	Υ	OK
Great Hautbois Road / Station Road	3	103	А	4	В	34	3AB	412	414	2	0%	0	Υ	OK
Great Hautbois Road / Station Road	3	103	А	4	С	31	3AC	1	1	0	0%	0	Υ	OK
Great Hautbois Road / Station Road	3	103	В	15	Α	33	3BA	298	291	-7	-2%	0	Υ	OK
Great Hautbois Road / Station Road	3	103	В	15	В	34	3BB	0	0	0	-	0	Υ	OK
Great Hautbois Road / Station Road	3	103	В	15	С	31	3BC	13	13	0	0%	0	Υ	OK
Great Hautbois Road / Station Road	3	103	С	32	Α	33	3CA	1	1	0	0%	0	Υ	OK
Great Hautbois Road / Station Road	3	103	С	32	В	34	3CB	7	7	0	0%	0	Υ	OK
Great Hautbois Road / Station Road	3	103	С	32	С	31	3CC	0	0	0	-	0	Υ	OK

AECOM 42 Prepared for: The Client Group

104 Vehicle Type Car VISSIM Node

	MCC	Nodo						Flow Pe	ak Time	Diffe	rence		GEH	
Junction Name	MCC Site	Node No.	From Arm	FromLink	To Arm	ToLink	MCC ID							Individual
	Site	NO.						Observed	Modelled	Value	%	Value	<5	Flows
Church Loke	4	104	Α	24	Α	23	4AA	0	0	0	-	0	Υ	OK
Church Loke	4	104	Α	24	В	29	4AB	19	19	0	0%	0	Υ	OK
Church Loke	4	104	Α	24	С	27	4AC	0	0	0	-	0	Υ	OK
Church Loke	4	104	A	24	D	26	4AD	28	27	-1	-4%	0	Υ	OK
Church Loke	4	104	В	6	Α	23	4BA	47	47	0	0%	0	Υ	OK
Church Loke	4	104	В	6	В	29	4BB	0	0	0	-	0	Υ	OK
Church Loke	4	104	В	6	С	27	4BC	1	1	0	0%	0	Υ	OK
Church Loke	4	104	В	6	D	26	4BD	182	181	-1	-1%	0	Υ	OK
Church Loke	4	104	С	28	Α	23	4CA	0	0	0	-	0	Υ	OK
Church Loke	4	104	С	28	В	29	4CB	1	1	0	0%	0	Υ	OK
Church Loke	4	104	С	28	С	27	4CC	0	0	0	-	0	Υ	OK
Church Loke	4	104	С	28	D	26	4CD	1	1	0	0%	0	Υ	OK
Church Loke	4	104	D	10	Α	23	4DA	53	54	1	2%	0	Υ	OK
Church Loke	4	104	D	10	В	29	4DB	233	237	4	2%	0	Υ	OK
Church Loke	4	104	D	10	С	27	4DC	4	4	0	0%	0	Υ	OK
Church Loke	4	104	D	10	D	26	4DD	0	0	0	-	0	Υ	OK

VISSIM Node 105 Vehicle Type Car

	MCC	Mada						Flow Pe	ak Time	Diffe	rence		GEH	
Junction Name	MCC Site	Node No.	From Arm	FromLink	To Arm	ToLink	MCC ID							Individual
	Site	NO.						Observed	Modelled	Value	%	Value	<5	Flows
B1150 Bridge	5	105	Α	12	Α	37	5AA	0	0	0	-	0	Υ	OK
B1150 Bridge	5	105	Α	12	В	12	5AB	583	567	-16	-3%	1	Υ	OK
B1150 Bridge	5	105	В	37	Α	37	5BA	542	538	-4	-1%	0	Υ	OK
B1150 Bridge	5	105	В	37	В	12	5BB	0	0	0	-	0	Y	OK

AM – LGV

Vehicle Type LGV **VISSIM Node** 101

	мсс	Node						Flow P	eak Time	Diffe	rence		GEH	
Junction Name	Site	No.	From Arm	FromLink	To Arm	ToLink	MCC ID	Observed	Modelled	Value	%	Value	< 5	Individual Flows
Rectory Road roundabout	1	101	А	38	Α	3	1AA	0	1	1	-	1	Υ	OK
Rectory Road roundabout	1	101	Α	38	В	19	1AB	2	2	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	А	38	С	22	1AC	108	100	-8	-7%	1	Υ	OK
Rectory Road roundabout	1	101	А	38	D	18	1AD	26	25	-1	-4%	0	Υ	OK
Rectory Road roundabout	1	101	В	20	Α	3	1BA	1	1	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	В	20	В	19	1BB	0	0	0	-	0	Υ	OK
Rectory Road roundabout	1	101	В	20	С	22	1BC	1	1	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	В	20	D	18	1BD	0	0	0	-	0	Υ	OK
Rectory Road roundabout	1	101	С	1	Α	3	1CA	126	126	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	С	1	В	19	1CB	3	3	0	0%	0	Υ	OK

AECOM 43 Prepared for: The Client Group

Rectory Road roundabout	1	101	С	1	С	22	1CC	0	0	0	-	0	Υ	OK
Rectory Road roundabout	1	101	С	1	D	18	1CD	32	32	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	D	17	Α	3	1DA	26	26	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	D	17	В	19	1DB	1	1	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	D	17	С	22	1DC	23	24	1	4%	0	Υ	OK
Rectory Road roundabout	1	101	D	17	D	18	1DD	0	0	0	-	0	Y	OK

Vehicle Type LGV **VISSIM Node** 102

	MCC	Node						Flow Peak	Time	Difference	e		GEH	
Junction Name	Site	Noae No.	From Arm	FromLink	To Arm	ToLink	MCC ID							Individual
	Site	NO.						Observed	Modelled	Value	%	Value	<5	Flows
Petrol Station Gyratory	2	102	Α	10011	Α	15	2AA	0	0	0	-	0	Υ	OK
Petrol Station Gyratory	2	102	Α	10011	В	10	2AB	12	12	0	0%	0	Υ	OK
Petrol Station Gyratory	2	102	Α	34	D	12	2AD	81	84	3	4%	0	Υ	OK
Petrol Station Gyratory	2	102	В	11	Α	15	2BA	8	8	0	0%	0	Υ	OK
Petrol Station Gyratory	2	102	В	11	В	10	2BB	0	0	0	-	0	Υ	OK
Petrol Station Gyratory	2	102	В	11	D	12	2BD	38	40	2	5%	0	Υ	OK
Petrol Station Gyratory	2	102	D	37	Α	15	2DA	91	92	1	1%	0	Υ	OK
Petrol Station Gyratory	2	102	D	37	В	10	2DB	65	65	0	0%	0	Υ	OK
Petrol Station Gyratory	2	102	D	37	D	12	2DD	0	0	0	-	0	Υ	OK

Vehicle Type LGV **VISSIM Node** 103

	мсс	Nede						Flow P	eak Time	Differ	ence		GEH	
Junction Name	Site	Node No.	From Arm	FromLink	To Arm	ToLink	MCC ID	Observed	Modelled	Value	%	Value	<5	Individual Flows
Great Hautbois Road / Station Road	3	103	А	4	Α	33	3AA	0	0	0	-	0	Υ	OK
Great Hautbois Road / Station Road	3	103	A	4	В	34	3AB	95	95	0	0%	0	Υ	OK
Great Hautbois Road / Station Road	3	103	A	4	С	31	3AC	0	0	0	-	0	Υ	OK
Great Hautbois Road / Station Road	3	103	В	15	Α	33	3BA	98	98	0	0%	0	Υ	OK
Great Hautbois Road / Station Road	3	103	В	15	В	34	3BB	0	0	0	-	0	Υ	OK
Great Hautbois Road / Station Road	3	103	В	15	С	31	3BC	2	2	0	0%	0	Υ	OK
Great Hautbois Road / Station Road	3	103	С	32	Α	33	3CA	1	1	0	0%	0	Υ	OK
Great Hautbois Road / Station Road	3	103	С	32	В	34	3CB	1	1	0	0%	0	Υ	OK
Great Hautbois Road / Station Road	3	103	С	32	С	31	3CC	0	0	0	-	0	Υ	OK

Vehicle Type LGV VISSIM Node 104

	MCC	Node						Flow P	eak Time	Diffe	rence		GEH	
Junction Name	Site	No.	From Arm	FromLink	To Arm	ToLink	MCC ID	Observed	Modelled	Value	%	Value	< 5	Individual Flows
Church Loke	4	104	А	24	Α	23	4AA	0	0	0	-	0	Υ	OK
Church Loke	4	104	А	24	В	29	4AB	4	4	0	0%	0	Υ	OK
Church Loke	4	104	Α	24	С	27	4AC	0	0	0	-	0	Υ	OK
Church Loke	4	104	Α	24	D	26	4AD	3	3	0	0%	0	Υ	OK
Church Loke	4	104	В	6	Α	23	4BA	3	3	0	0%	0	Υ	OK
Church Loke	4	104	В	6	В	29	4BB	0	0	0	-	0	Υ	OK
Church Loke	4	104	В	6	С	27	4BC	0	0	0	-	0	Υ	OK

AECOM 44 Prepared for: The Client Group

Church Loke	4	104	В	6	D	26	4BD	43	43	0	0%	0	Υ	OK
Church Loke	4	104	С	28	А	23	4CA	0	0	0	-	0	Υ	OK
Church Loke	4	104	С	28	В	29	4CB	3	3	0	0%	0	Υ	OK
Church Loke	4	104	С	28	С	27	4CC	0	0	0	-	0	Υ	OK
Church Loke	4	104	С	28	D	26	4CD	2	2	0	0%	0	Υ	OK
Church Loke	4	104	D	10	Α	23	4DA	3	3	0	0%	0	Υ	OK
Church Loke	4	104	D	10	В	29	4DB	63	70	7	11%	1	Y	OK
Church Loke	4	104	D	10	С	27	4DC	5	5	0	0%	0	Υ	OK
Church Loke	4	104	D	10	D	26	4DD	0	0	0	-	0	Υ	OK

Vehicle Type LGV VISSIM Node 105

	MCC	Mada						Flow P	eak Time	Diffe	rence		GEH	
Junction Name	MCC Site	Node No.	From Arm	FromLink	To Arm	ToLink	MCC ID							Individual
	Oito	110.						Observed	Modelled	Value	%	Value	<5	Flows
B1150 Bridge	5	105	Α	12	Α	37	5AA	0	0	0	-	0	Υ	OK
B1150 Bridge	5	105	Α	12	В	12	5AB	134	124	-10	-7%	1	Υ	OK
B1150 Bridge	5	105	В	37	Α	37	5BA	157	157	0	0%	0	Υ	OK
B1150 Bridge	5	105	В	37	В	12	5BB	0	0	0	-	0	Υ	OK

AM – HGV

VISSIM Node 101 Vehicle Type HGV

	MCC	Nede						Flow P	eak Time	Diffe	rence		GEH	
Junction Name	MCC Site	Node No.	From Arm	FromLink	To Arm	ToLink	MCC ID	Observed	Modelled	Value	%	Value	<5	Individual Flows
Rectory Road roundabout	1	101	Α	38	Α	3	1AA	0	0	0	-	0	Υ	OK
Rectory Road roundabout	1	101	Α	38	В	19	1AB	0	0	0	-	0	Υ	OK
Rectory Road roundabout	1	101	Α	38	С	22	1AC	18	16	-2	-11%	0	Υ	OK
Rectory Road roundabout	1	101	Α	38	D	18	1AD	2	2	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	В	20	Α	3	1BA	0	0	0	-	0	Υ	OK
Rectory Road roundabout	1	101	В	20	В	19	1BB	0	0	0	-	0	Υ	OK
Rectory Road roundabout	1	101	В	20	С	22	1BC	0	0	0	-	0	Υ	OK
Rectory Road roundabout	1	101	В	20	D	18	1BD	0	0	0	-	0	Υ	OK
Rectory Road roundabout	1	101	С	1	Α	3	1CA	12	12	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	С	1	В	19	1CB	0	0	0	-	0	Υ	OK
Rectory Road roundabout	1	101	С	1	С	22	1CC	0	0	0	-	0	Υ	OK
Rectory Road roundabout	1	101	С	1	D	18	1CD	10	9	-1	-10%	0	Υ	OK
Rectory Road roundabout	1	101	D	17	Α	3	1DA	5	5	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	D	17	В	19	1DB	0	0	0	-	0	Υ	OK
Rectory Road roundabout	1	101	D	17	С	22	1DC	8	8	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	D	17	D	18	1DD	0	0	0	-	0	Υ	OK

Vehicle Type HGV **VISSIM Node** 102

	MCC	Node						Flow P	eak Time	Diffe	rence		GEH	
Junction Name	Site	No.	From Arm	FromLink	To Arm	ToLink	MCC ID							Individual
	Site	NO.						Observed	Modelled	Value	%	Value	<5	Flows

AECOM 45 Prepared for: The Client Group

Petrol Station Gyratory	2	102	А	10011	Α	15	2AA	0	0	0	-	0	Υ	OK
Petrol Station Gyratory	2	102	Α	10011	В	10	2AB	2	2	0	0%	0	Υ	OK
Petrol Station Gyratory	2	102	Α	34	D	12	2AD	11	11	0	0%	0	Υ	OK
Petrol Station Gyratory	2	102	В	11	Α	15	2BA	3	3	0	0%	0	Υ	OK
Petrol Station Gyratory	2	102	В	11	В	10	2BB	0	0	0	-	0	Υ	OK
Petrol Station Gyratory	2	102	В	11	D	12	2BD	5	5	0	0%	0	Υ	OK
Petrol Station Gyratory	2	102	D	37	А	15	2DA	9	9	0	0%	0	Υ	OK
Petrol Station Gyratory	2	102	D	37	В	10	2DB	7	8	1	14%	0	Υ	OK
Petrol Station Gyratory	2	102	D	37	D	12	2DD	0	0	0	-	0	Υ	OK

VISSIM Node Vehicle Type HGV 103

	мсс	Mada						Flow P	eak Time	Diffe	rence		GEH	
Junction Name	Site	Node No.	From Arm	FromLink	To Arm	ToLink	MCC ID							Individual
	Oito	110.						Observed	Modelled	Value	%	Value	<5	Flows
Great Hautbois Road / Station Road	3	103	Α	4	Α	33	3AA	0	0	0	-	0	Υ	OK
Great Hautbois Road / Station Road	3	103	Α	4	В	34	3AB	13	13	0	0%	0	Υ	OK
Great Hautbois Road / Station Road	3	103	Α	4	С	31	3AC	0	0	0	-	0	Υ	OK
Great Hautbois Road / Station Road	3	103	В	15	Α	33	3BA	14	12	-2	-14%	1	Υ	OK
Great Hautbois Road / Station Road	3	103	В	15	В	34	3BB	0	0	0	-	0	Υ	OK
Great Hautbois Road / Station Road	3	103	В	15	С	31	3BC	0	0	0	-	0	Υ	OK
Great Hautbois Road / Station Road	3	103	С	32	Α	33	3CA	0	0	0	-	0	Υ	OK
Great Hautbois Road / Station Road	3	103	С	32	В	34	3CB	0	0	0	-	0	Υ	OK
Great Hautbois Road / Station Road	3	103	С	32	С	31	3CC	0	0	0	_	0	Y	OK

104 Vehicle Type HGV **VISSIM Node**

	мсс	Mode						Flow P	eak Time	Diffe	rence		GEH	
Junction Name	Site	Node No.	From Arm	FromLink	To Arm	ToLink	MCC ID	Observed	Modelled	Value	%	Value	<5	Individual Flows
Church Loke	4	104	A	24	Α	23	4AA	0	0	0	-	0	Υ	OK
Church Loke	4	104	A	24	В	29	4AB	0	0	0	-	0	Υ	OK
Church Loke	4	104	A	24	С	27	4AC	0	0	0	-	0	Y	OK
Church Loke	4	104	Α	24	D	26	4AD	2	2	0	0%	0	Υ	OK
Church Loke	4	104	В	6	Α	23	4BA	0	0	0	-	0	Υ	OK
Church Loke	4	104	В	6	В	29	4BB	0	0	0	-	0	Y	OK
Church Loke	4	104	В	6	С	27	4BC	1	1	0	0%	0	Y	OK
Church Loke	4	104	В	6	D	26	4BD	5	5	0	0%	0	Y	OK
Church Loke	4	104	С	28	Α	23	4CA	0	0	0	-	0	Y	OK
Church Loke	4	104	С	28	В	29	4CB	0	0	0	-	0	Y	OK
Church Loke	4	104	С	28	С	27	4CC	0	0	0	-	0	Y	OK
Church Loke	4	104	С	28	D	26	4CD	1	1	0	0%	0	Υ	OK
Church Loke	4	104	D	10	Α	23	4DA	1	1	0	0%	0	Y	OK
Church Loke	4	104	D	10	В	29	4DB	8	8	0	0%	0	Υ	OK
Church Loke	4	104	D	10	С	27	4DC	0	0	0	-	0	Υ	OK
Church Loke	4	104	D	10	D	26	4DD	0	0	0	-	0	Υ	OK

VISSIM Node 105 Vehicle Type HGV

AECOM 46 Prepared for: The Client Group

	мсс	Node						Flow P	eak Time	Diffe	rence		GEH	
Junction Name	Site	No.	From Arm	FromLink	To Arm	ToLink	MCC ID				01			Individual
								Observed	Modelled	Value	%	Value	<5	Flows
B1150 Bridge	5	105	Α	12	Α	37	5AA	0	0	0	-	0	Υ	OK
B1150 Bridge	5	105	Α	12	В	12	5AB	19	16	-3	-16%	1	Υ	OK
B1150 Bridge	5	105	В	37	Α	37	5BA	16	17	1	6%	0	Υ	OK
B1150 Bridge	5	105	В	37	В	12	5BB	0	0	0	-	0	Υ	OK

PM - All Vehicles

Vehicle Type Total VISSIM Node 101

		Nodo						Flow Pe	ak Time	Diffe	rence		GEH	
Junction Name	MCC Site	Node No.	From Arm	FromLink	To Arm	ToLink	MCC ID	Observed	Modelled	Value	%	Value	< 5	Individual Flows
Rectory Road roundabout	1	101	А	38	А	3	1AA	1	2	1	100%	1	Υ	OK
Rectory Road roundabout	1	101	A	38	В	19	1AB	11	9	-2	-18%	1	Υ	OK
Rectory Road roundabout	1	101	A	38	С	22	1AC	561	525	-36	-6%	2	Υ	OK
Rectory Road roundabout	1	101	Α	38	D	18	1AD	151	141	-10	-7%	1	Υ	OK
Rectory Road roundabout	1	101	В	20	А	3	1BA	8	8	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	В	20	В	19	1BB	0	0	0	-	0	Υ	OK
Rectory Road roundabout	1	101	В	20	С	22	1BC	10	10	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	В	20	D	18	1BD	3	2	-1	-33%	1	Υ	OK
Rectory Road roundabout	1	101	С	1	Α	3	1CA	628	616	-12	-2%	0	Υ	OK
Rectory Road roundabout	1	101	С	1	В	19	1CB	2	2	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	С	1	С	22	1CC	0	0	0	-	0	Υ	OK
Rectory Road roundabout	1	101	С	1	D	18	1CD	100	97	-3	-3%	0	Υ	OK
Rectory Road roundabout	1	101	D	17	Α	3	1DA	123	120	-3	-2%	0	Υ	OK
Rectory Road roundabout	1	101	D	17	В	19	1DB	1	1	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	D	17	С	22	1DC	76	76	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	D	17	D	18	1DD	0	0	0	-	0	Υ	OK

VISSIM Node Vehicle Type Total 102

		Node					мсс	Flow Pea	ak Time	Diffe	rence		GEH	
Junction Name	MCC Site	No.	From Arm	FromLink	To Arm	ToLink	ID	Observed	Modelled	Value	%	Value	< 5	Individual Flows
Petrol Station Gyratory	2	102	Α	10011	А	15	2AA	0	0	0	-	0	Υ	OK
Petrol Station Gyratory	2	102	Α	10011	В	10	2AB	41	40	-1	-2%	0	Υ	OK
Petrol Station Gyratory	2	102	Α	34	D	12	2AD	408	402	-6	-1%	0	Υ	OK
Petrol Station Gyratory	2	102	В	11	А	15	2BA	41	41	0	0%	0	Υ	OK
Petrol Station Gyratory	2	102	В	11	В	10	2BB	0	0	0	-	0	Υ	OK
Petrol Station Gyratory	2	102	В	11	D	12	2BD	254	263	9	4%	1	Υ	OK
Petrol Station Gyratory	2	102	D	37	А	15	2DA	493	484	-9	-2%	0	Υ	OK
Petrol Station Gyratory	2	102	D	37	В	10	2DB	261	254	-7	-3%	0	Υ	OK
Petrol Station Gyratory	2	102	D	37	D	12	2DD	0	3	3	-	2	Υ	OK

Vehicle Type Total VISSIM Node 103

AECOM 47 Prepared for: The Client Group

		Node					мсс	Flow Pe	ak Time	Diffe	rence		GEH	
Junction Name	MCC Site	No.	From Arm	FromLink	To Arm	ToLink	ID	Observed	Modelled	Value	%	Value	< 5	Individual Flows
Great Hautbois Road / Station Road	3	103	А	4	А	33	3AA	0	0	0	-	0	Υ	OK
Great Hautbois Road / Station Road	3	103	А	4	В	34	3AB	426	417	-9	-2%	0	Υ	OK
Great Hautbois Road / Station Road	3	103	А	4	С	31	3AC	1	1	0	0%	0	Υ	OK
Great Hautbois Road / Station Road	3	103	В	15	А	33	3BA	523	506	-17	-3%	1	Υ	OK
Great Hautbois Road / Station Road	3	103	В	15	В	34	3BB	0	0	0	-	0	Υ	OK
Great Hautbois Road / Station Road	3	103	В	15	С	31	3BC	19	18	-1	-5%	0	Υ	OK
Great Hautbois Road / Station Road	3	103	С	32	А	33	3CA	9	8	-1	-11%	0	Υ	OK
Great Hautbois Road / Station Road	3	103	С	32	В	34	3CB	27	26	-1	-4%	0	Υ	OK
Great Hautbois Road / Station Road	3	103	С	32	С	31	3CC	0	0	0	-	0	Υ	OK

Vehicle Type Total **VISSIM Node** 104

		Mode					MCC	Flow Pe	ak Time	Diffe	rence		GEH	
Junction Name	MCC Site	Node No.	From Arm	FromLink	To Arm	ToLink	MCC ID	Observed	Modelled	Value	%	Value	<5	Individual Flows
Church Loke	4	104	Α	24	А	23	4AA	0	0	0	-	0	Υ	OK
Church Loke	4	104	Α	24	В	29	4AB	16	16	0	0%	0	Υ	OK
Church Loke	4	104	Α	24	С	27	4AC	0	0	0	-	0	Υ	OK
Church Loke	4	104	Α	24	D	26	4AD	28	27	-1	-4%	0	Υ	OK
Church Loke	4	104	В	6	А	23	4BA	24	25	1	4%	0	Υ	OK
Church Loke	4	104	В	6	В	29	4BB	0	0	0	-	0	Υ	OK
Church Loke	4	104	В	6	С	27	4BC	0	0	0	-	0	Υ	OK
Church Loke	4	104	В	6	D	26	4BD	281	277	-4	-1%	0	Υ	OK
Church Loke	4	104	С	28	А	23	4CA	0	0	0	-	0	Υ	OK
Church Loke	4	104	С	28	В	29	4CB	2	2	0	0%	0	Υ	OK
Church Loke	4	104	С	28	С	27	4CC	0	0	0	-	0	Υ	OK
Church Loke	4	104	С	28	D	26	4CD	2	2	0	0%	0	Υ	OK
Church Loke	4	104	D	10	A	23	4DA	37	35	-2	-5%	0	Υ	OK
Church Loke	4	104	D	10	В	29	4DB	260	257	-3	-1%	0	Υ	OK
Church Loke	4	104	D	10	С	27	4DC	1	1	0	0%	0	Υ	OK
Church Loke	4	104	D	10	D	26	4DD	0	0	0	-	0	Υ	OK

Vehicle Type Total **VISSIM Node** 105

		Node					мсс	Flow Pea	ak Time	Diffe	rence		GEH	
Junction Name	MCC Site	No.	From Arm	FromLink	To Arm	ToLink	ID	Observed	Modelled	Value	%	Value	< 5	Individual Flows
B1150 Bridge	5	105	А	12	А	37	5AA	0	0	0	-	0	Υ	OK
B1150 Bridge	5	105	Α	12	В	12	5AB	716	668	-48	-7%	2	Υ	OK
B1150 Bridge	5	105	В	37	Α	37	5BA	756	739	-17	-2%	1	Υ	OK
B1150 Bridge	5	105	В	37	В	12	5BB	0	0	0	-	0	Υ	OK

PM - Cars

VISSIM Node 101 Vehicle Type Car

AECOM 48 Prepared for: The Client Group

	MCC	Nede						Flow Pe	ak Time	Diffe	rence		GEH	
Junction Name	MCC Site	Node No.	From Arm	FromLink	To Arm	ToLink	MCC ID						_	Individual
								Observed	Modelled	Value	%	Value	<5	Flows
Rectory Road roundabout	1	101	Α	38	Α	3	1AA	1	1	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	Α	38	В	19	1AB	11	9	-2	-18%	1	Υ	OK
Rectory Road roundabout	1	101	Α	38	С	22	1AC	448	418	-30	-7%	1	Υ	OK
Rectory Road roundabout	1	101	Α	38	D	18	1AD	120	112	-8	-7%	1	Υ	OK
Rectory Road roundabout	1	101	В	20	Α	3	1BA	7	8	1	14%	0	Υ	OK
Rectory Road roundabout	1	101	В	20	В	19	1BB	0	0	0	-	0	Υ	OK
Rectory Road roundabout	1	101	В	20	С	22	1BC	10	10	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	В	20	D	18	1BD	3	2	-1	-33%	1	Υ	OK
Rectory Road roundabout	1	101	С	1	Α	3	1CA	506	504	-2	0%	0	Υ	OK
Rectory Road roundabout	1	101	С	1	В	19	1CB	2	2	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	С	1	С	22	1CC	0	0	0	-	0	Υ	OK
Rectory Road roundabout	1	101	С	1	D	18	1CD	66	66	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	D	17	Α	3	1DA	97	97	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	D	17	В	19	1DB	1	1	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	D	17	С	22	1DC	56	56	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	D	17	D	18	1DD	0	0	0	-	0	Υ	OK

Vehicle Type Car **VISSIM Node** 102

	мсс	Node						Flow Peak	Time	Differenc	е		GEH	
Junction Name	Site	Noae No.	From Arm	FromLink	To Arm	ToLink	MCC ID							Individual
	Site	NO.						Observed	Modelled	Value	%	Value	<5	Flows
Petrol Station Gyratory	2	102	Α	10011	Α	15	2AA	0	0	0	-	0	Υ	OK
Petrol Station Gyratory	2	102	Α	10011	В	10	2AB	38	38	0	0%	0	Υ	OK
Petrol Station Gyratory	2	102	Α	34	D	12	2AD	328	326	-2	-1%	0	Υ	OK
Petrol Station Gyratory	2	102	В	11	Α	15	2BA	27	29	2	7%	0	Υ	OK
Petrol Station Gyratory	2	102	В	11	В	10	2BB	0	0	0	-	0	Υ	OK
Petrol Station Gyratory	2	102	В	11	D	12	2BD	202	220	18	9%	1	Υ	OK
Petrol Station Gyratory	2	102	D	37	Α	15	2DA	395	397	2	1%	0	Υ	OK
Petrol Station Gyratory	2	102	D	37	В	10	2DB	205	207	2	1%	0	Υ	OK
Petrol Station Gyratory	2	102	D	37	D	12	2DD	0	1	1	-	1	Υ	OK

Vehicle Type Car **VISSIM Node** 103

	мсс	Node						Flow Pe	ak Time	Diffe	rence		GEH	
Junction Name	Site	No.	From Arm	FromLink	To Arm	ToLink	MCC ID	Observed	Modelled	Value	%	Value	< 5	Individual Flows
Great Hautbois Road / Station Road	3	103	Α	4	Α	33	3AA	0	0	0	-	0	Υ	OK
Great Hautbois Road / Station Road	3	103	Α	4	В	34	3AB	344	340	-4	-1%	0	Υ	OK
Great Hautbois Road / Station Road	3	103	Α	4	С	31	3AC	1	1	0	0%	0	Υ	OK
Great Hautbois Road / Station Road	3	103	В	15	Α	33	3BA	411	409	-2	0%	0	Υ	OK
Great Hautbois Road / Station Road	3	103	В	15	В	34	3BB	0	0	0	-	0	Υ	OK
Great Hautbois Road / Station Road	3	103	В	15	С	31	3BC	17	17	0	0%	0	Υ	OK
Great Hautbois Road / Station Road	3	103	С	32	Α	33	3CA	7	7	0	0%	0	Υ	OK
Great Hautbois Road / Station Road	3	103	С	32	В	34	3CB	26	26	0	0%	0	Υ	OK
Great Hautbois Road / Station Road	3	103	С	32	С	31	3CC	0	0	0	-	0	Υ	OK

AECOM 49 Prepared for: The Client Group

VISSIM Node Vehicle Type Car 104

	мсс	Nodo						Flow Pe	ak Time	Differ	rence		GEH	
Junction Name	Site	Node No.	From Arm	FromLink	To Arm	ToLink	MCC ID	Observed	Modelled	Value	%	Value	<5	Individual Flows
Church Loke	4	104	Α	24	Α	23	4AA	0	0	0	-	0	Υ	OK
Church Loke	4	104	А	24	В	29	4AB	14	14	0	0%	0	Υ	OK
Church Loke	4	104	А	24	С	27	4AC	0	0	0	-	0	Υ	OK
Church Loke	4	104	А	24	D	26	4AD	25	25	0	0%	0	Υ	OK
Church Loke	4	104	В	6	Α	23	4BA	17	17	0	0%	0	Υ	OK
Church Loke	4	104	В	6	В	29	4BB	0	0	0	-	0	Υ	OK
Church Loke	4	104	В	6	С	27	4BC	0	0	0	-	0	Υ	OK
Church Loke	4	104	В	6	D	26	4BD	225	225	0	0%	0	Υ	OK
Church Loke	4	104	С	28	Α	23	4CA	0	0	0	-	0	Υ	OK
Church Loke	4	104	С	28	В	29	4CB	2	2	0	0%	0	Υ	OK
Church Loke	4	104	С	28	С	27	4CC	0	0	0	-	0	Υ	OK
Church Loke	4	104	С	28	D	26	4CD	2	2	0	0%	0	Υ	OK
Church Loke	4	104	D	10	Α	23	4DA	33	33	0	0%	0	Υ	OK
Church Loke	4	104	D	10	В	29	4DB	207	210	3	1%	0	Υ	OK
Church Loke	4	104	D	10	С	27	4DC	1	1	0	0%	0	Υ	OK
Church Loke	4	104	D	10	D	26	4DD	0	0	0	-	0	Υ	OK

Vehicle Type Car **VISSIM Node** 105

	MCC	Node						Flow Pe	ak Time	Diffe	rence		GEH	
Junction Name	Site	No.	From Arm	FromLink	To Arm	ToLink	MCC ID	Observed	Modelled	Value	%	Value	< 5	Individual Flows
B1150 Bridge	5	105	A	12	Α	37	5AA	0	0	0	-	0	Υ	OK
B1150 Bridge	5	105	A	12	В	12	5AB	590	549	-41	-7%	2	Υ	OK
B1150 Bridge	5	105	В	37	Α	37	5BA	607	604	-3	0%	0	Υ	OK
B1150 Bridge	5	105	В	37	В	12	5BB	0	0	0	-	0	Υ	OK

PM - LGV

VISSIM Node 101 Vehicle Type LGV

	мсс	Node						Flow P	eak Time	Diffe	rence		GEH	
Junction Name	Site	No.	From Arm	FromLink	To Arm	ToLink	MCC ID	Observed	Modelled	Value	%	Value	< 5	Individual Flows
Rectory Road roundabout	1	101	Α	38	Α	3	1AA	0	0	0	-	0	Υ	OK
Rectory Road roundabout	1	101	А	38	В	19	1AB	0	0	0	-	0	Υ	OK
Rectory Road roundabout	1	101	А	38	С	22	1AC	96	99	3	3%	0	Υ	OK
Rectory Road roundabout	1	101	A	38	D	18	1AD	27	27	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	В	20	Α	3	1BA	0	0	0	-	0	Υ	OK
Rectory Road roundabout	1	101	В	20	В	19	1BB	0	0	0	-	0	Υ	OK
Rectory Road roundabout	1	101	В	20	С	22	1BC	0	0	0	-	0	Υ	OK
Rectory Road roundabout	1	101	В	20	D	18	1BD	0	0	0	-	0	Υ	OK
Rectory Road roundabout	1	101	С	1	Α	3	1CA	101	101	0	0%	0	Υ	OK

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Rectory Road roundabout	1	101	С	1	В	19	1CB	0	0	0	-	0	Υ	OK
Rectory Road roundabout	1	101	С	1	С	22	1CC	0	0	0	-	0	Υ	OK
Rectory Road roundabout	1	101	С	1	D	18	1CD	27	27	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	D	17	Α	3	1DA	22	22	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	D	17	В	19	1DB	0	0	0	-	0	Υ	OK
Rectory Road roundabout	1	101	D	17	С	22	1DC	19	19	0	0%	0	Υ	OK
Rectory Road roundabout	1	101	D	17	D	18	1DD	0	0	0	-	0	Υ	OK

Vehicle Type LGV **VISSIM Node** 102

	MCC	Node						Flow P	eak Time	Diffe	rence		GEH	
Junction Name	Site	No.	From Arm	FromLink	To Arm	ToLink	MCC ID	Observed	Modelled	Value	%	Value	< 5	Individual Flows
Petrol Station Gyratory	2	102	А	10011	Α	15	2AA	0	0	0	-	0	Υ	OK
Petrol Station Gyratory	2	102	А	10011	В	10	2AB	2	2	0	0%	0	Υ	OK
Petrol Station Gyratory	2	102	А	34	D	12	2AD	69	70	1	1%	0	Υ	OK
Petrol Station Gyratory	2	102	В	11	Α	15	2BA	13	11	-2	-15%	1	Υ	OK
Petrol Station Gyratory	2	102	В	11	В	10	2BB	0	0	0	-	0	Υ	OK
Petrol Station Gyratory	2	102	В	11	D	12	2BD	45	40	-5	-11%	1	Υ	OK
Petrol Station Gyratory	2	102	D	37	Α	15	2DA	79	76	-3	-4%	0	Υ	OK
Petrol Station Gyratory	2	102	D	37	В	10	2DB	46	45	-1	-2%	0	Υ	OK
Petrol Station Gyratory	2	102	D	37	D	12	2DD	0	1	1	-	1	Υ	OK

Vehicle Type LGV **VISSIM Node** 103

	мсс	Node						Flow P	eak Time	Differ	ence		GEH	
Junction Name	Site	No.	From Arm	FromLink	To Arm	ToLink	MCC ID							Individual
	Oile	110.						Observed	Modelled	Value	%	Value	<5	Flows
Great Hautbois Road / Station Road	3	103	Α	4	Α	33	3AA	0	0	0	-	0	Υ	OK
Great Hautbois Road / Station Road	3	103	Α	4	В	34	3AB	71	72	1	1%	0	Υ	OK
Great Hautbois Road / Station Road	3	103	Α	4	С	31	3AC	0	0	0	-	0	Υ	OK
Great Hautbois Road / Station Road	3	103	В	15	Α	33	3BA	92	87	-5	-5%	1	Υ	OK
Great Hautbois Road / Station Road	3	103	В	15	В	34	3BB	0	0	0	-	0	Υ	OK
Great Hautbois Road / Station Road	3	103	В	15	С	31	3BC	1	1	0	0%	0	Υ	OK
Great Hautbois Road / Station Road	3	103	С	32	Α	33	3CA	1	1	0	0%	0	Υ	OK
Great Hautbois Road / Station Road	3	103	С	32	В	34	3CB	0	0	0	•	0	Υ	OK
Great Hautbois Road / Station Road	3	103	С	32	С	31	3CC	0	0	0	-	0	Υ	OK

VISSIM Node 104 Vehicle Type LGV

	MCC	Node						Flow P	eak Time	Diffe	rence		GEH	
Junction Name	Site	No.	From Arm	FromLink	To Arm	ToLink	MCC ID	Observed	Modelled	Value	%	Value	< 5	Individual Flows
Church Loke	4	104	А	24	Α	23	4AA	0	0	0	-	0	Υ	OK
Church Loke	4	104	Α	24	В	29	4AB	2	2	0	0%	0	Υ	OK
Church Loke	4	104	Α	24	С	27	4AC	0	0	0	-	0	Υ	OK
Church Loke	4	104	А	24	D	26	4AD	1	1	0	0%	0	Υ	OK
Church Loke	4	104	В	6	Α	23	4BA	6	6	0	0%	0	Υ	OK
Church Loke	4	104	В	6	В	29	4BB	0	0	0	-	0	Υ	OK

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Church Loke	4	104	В	6	С	27	4BC	0	0	0	-	0	Υ	OK
Church Loke	4	104	В	6	D	26	4BD	51	51	0	0%	0	Υ	OK
Church Loke	4	104	С	28	А	23	4CA	0	0	0	-	0	Υ	OK
Church Loke	4	104	С	28	В	29	4CB	0	0	0	-	0	Υ	OK
Church Loke	4	104	С	28	С	27	4CC	0	0	0	-	0	Υ	OK
Church Loke	4	104	С	28	D	26	4CD	0	0	0	-	0	Υ	OK
Church Loke	4	104	D	10	А	23	4DA	2	2	0	0%	0	Y	OK
Church Loke	4	104	D	10	В	29	4DB	45	45	0	0%	0	Y	OK
Church Loke	4	104	D	10	С	27	4DC	0	0	0	-	0	Υ	OK
Church Loke	4	104	D	10	D	26	4DD	0	0	0	-	0	Υ	OK

Vehicle Type LGV **VISSIM Node** 105

	мсс	Node						Flow P	eak Time	Diffe	rence		GEH	
Junction Name	Site	No.	From Arm	FromLink	To Arm	ToLink	MCC ID							Individual
	Site	NO.						Observed	Modelled	Value	%	Value	<5	Flows
B1150 Bridge	5	105	Α	12	Α	37	5AA	0	0	0	-	0	Υ	OK
B1150 Bridge	5	105	Α	12	В	12	5AB	107	111	4	4%	0	Υ	OK
B1150 Bridge	5	105	В	37	Α	37	5BA	122	122	0	0%	0	Υ	OK
B1150 Bridge	5	105	В	37	В	12	5BB	0	0	0	-	0	Υ	OK

PM - HGV

Vehicle Type HGV **VISSIM Node** 101

	MCC	Node						Flow P	eak Time	Diffe	rence		GEH	
Junction Name	Site	No.	From Arm	FromLink	To Arm	ToLink	MCC ID	Observed	Modelled	Value	%	Value	<5	Individual Flows
Rectory Road roundabout	1	101	Α	38	Α	3	1AA	0	0	0	-	0%	Υ	OK
Rectory Road roundabout	1	101	Α	38	В	19	1AB	0	0	0	-	0%	Υ	OK
Rectory Road roundabout	1	101	Α	38	С	22	1AC	7	7	0	0%	0%	Υ	OK
Rectory Road roundabout	1	101	Α	38	D	18	1AD	2	2	0	0%	0%	Υ	OK
Rectory Road roundabout	1	101	В	20	Α	3	1BA	0	0	0	-	0%	Υ	OK
Rectory Road roundabout	1	101	В	20	В	19	1BB	0	0	0	-	0%	Υ	OK
Rectory Road roundabout	1	101	В	20	С	22	1BC	0	0	0	-	0%	Υ	OK
Rectory Road roundabout	1	101	В	20	D	18	1BD	0	0	0	-	0%	Υ	OK
Rectory Road roundabout	1	101	С	1	Α	3	1CA	11	11	0	0%	0%	Υ	OK
Rectory Road roundabout	1	101	С	1	В	19	1CB	0	0	0	-	0%	Υ	OK
Rectory Road roundabout	1	101	С	1	С	22	1CC	0	0	0	-	0%	Υ	OK
Rectory Road roundabout	1	101	С	1	D	18	1CD	5	5	0	0%	0%	Υ	OK
Rectory Road roundabout	1	101	D	17	Α	3	1DA	1	1	0	0%	0%	Υ	OK
Rectory Road roundabout	1	101	D	17	В	19	1DB	0	0	0	-	0%	Υ	OK
Rectory Road roundabout	1	101	D	17	С	22	1DC	1	1	0	0%	0%	Υ	OK
Rectory Road roundabout	1	101	D	17	D	18	1DD	0	0	0	_	0%	Υ	OK

VISSIM Node 102 Vehicle Type HGV

Difference GEH **Junction Name** From Arm FromLink To Arm ToLink MCC ID Flow Peak Time

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	MCC	Node												Individual
	Site	No.						Observed	Modelled	Value	%	Value	<5	Flows
Petrol Station Gyratory	2	102	Α	10011	Α	15	2AA	0	0	0	-	0%	Υ	OK
Petrol Station Gyratory	2	102	Α	10011	В	10	2AB	0	0	0	-	0%	Υ	OK
Petrol Station Gyratory	2	102	Α	34	D	12	2AD	5	5	0	0%	0%	Υ	OK
Petrol Station Gyratory	2	102	В	11	Α	15	2BA	0	0	0	-	0%	Υ	OK
Petrol Station Gyratory	2	102	В	11	В	10	2BB	0	0	0	-	0%	Υ	OK
Petrol Station Gyratory	2	102	В	11	D	12	2BD	2	2	0	0%	0%	Υ	OK
Petrol Station Gyratory	2	102	D	37	Α	15	2DA	10	9	-1	-10%	32%	Υ	OK
Petrol Station Gyratory	2	102	D	37	В	10	2DB	2	2	0	0%	0%	Υ	OK
Petrol Station Gyratory	2	102	D	37	D	12	2DD	0	0	0	-	0%	Υ	OK

Vehicle Type HGV **VISSIM Node** 103

	мсс	Node						Flow P	eak Time	Diffe	rence		GEH	
Junction Name	Site	No.	From Arm	FromLink	To Arm	ToLink	MCC ID	Observed	Modelled	Value	%	Value	<5	Individual Flows
Great Hautbois Road / Station Road	3	103	А	4	А	33	3AA	0	0	0	-	0%	Υ	OK
Great Hautbois Road / Station Road	3	103	A	4	В	34	3AB	5	5	0	0%	0%	Υ	OK
Great Hautbois Road / Station Road	3	103	Α	4	С	31	3AC	0	0	0	-	0%	Υ	OK
Great Hautbois Road / Station Road	3	103	В	15	Α	33	3BA	10	9	-1	-10%	32%	Υ	OK
Great Hautbois Road / Station Road	3	103	В	15	В	34	3BB	0	0	0	•	0%	Υ	OK
Great Hautbois Road / Station Road	3	103	В	15	С	31	3BC	0	0	0	-	0%	Υ	OK
Great Hautbois Road / Station Road	3	103	С	32	Α	33	3CA	0	0	0	-	0%	Υ	OK
Great Hautbois Road / Station Road	3	103	С	32	В	34	3CB	0	0	0	-	0%	Υ	OK
Great Hautbois Road / Station Road	3	103	С	32	С	31	3CC	0	0	0	-	0%	Υ	OK

VISSIM Node 104 Vehicle Type HGV

	MCC	Node						Flow Peak Time		Difference			GEH	
Junction Name	Site	No.	From Arm	FromLink	To Arm	ToLink	MCC ID							Individual
	Oito	110.						Observed	Modelled	Value	%	Value	<5	Flows
Church Loke	4	104	Α	24	Α	23	4AA	0	0	0	-	0%	Υ	OK
Church Loke	4	104	Α	24	В	29	4AB	0	0	0	-	0%	Υ	OK
Church Loke	4	104	Α	24	С	27	4AC	0	0	0	-	0%	Υ	OK
Church Loke	4	104	Α	24	D	26	4AD	0	0	0	-	0%	Υ	OK
Church Loke	4	104	В	6	Α	23	4BA	1	1	0	0%	0%	Υ	OK
Church Loke	4	104	В	6	В	29	4BB	0	0	0	-	0%	Υ	OK
Church Loke	4	104	В	6	С	27	4BC	0	0	0	-	0%	Υ	OK
Church Loke	4	104	В	6	D	26	4BD	2	2	0	0%	0%	Υ	OK
Church Loke	4	104	С	28	Α	23	4CA	0	0	0	-	0%	Υ	OK
Church Loke	4	104	С	28	В	29	4CB	0	0	0	-	0%	Υ	OK
Church Loke	4	104	С	28	С	27	4CC	0	0	0	-	0%	Υ	OK
Church Loke	4	104	С	28	D	26	4CD	0	0	0	-	0%	Υ	OK
Church Loke	4	104	D	10	Α	23	4DA	0	0	0	-	0%	Υ	OK
Church Loke	4	104	D	10	В	29	4DB	3	2	-1	-33%	63%	Υ	OK
Church Loke	4	104	D	10	С	27	4DC	0	0	0	-	0%	Y	OK
Church Loke	4	104	D	10	D	26	4DD	0	0	0	-	0%	Y	OK

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VISSIM Node 105 Vehicle Type HGV

	МСС	Node						Flow Peak Time		Difference			GEH	
Junction Name	Site	No.	From Arm	FromLink	To Arm	ToLink	MCC ID	Observed	Modelled	Value	%	Value	<5	Individual Flows
B1150 Bridge	5	105	Α	12	Α	37	5AA	0	0	0	-	0%	Υ	OK
B1150 Bridge	5	105	Α	12	В	12	5AB	7	7	0	0%	0%	Υ	OK
B1150 Bridge	5	105	В	37	А	37	5BA	11	11	0	0%	0%	Υ	OK
B1150 Bridge	5	105	В	37	В	12	5BB	0	0	0	-	0%	Υ	OK

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Appendix E – Forecast Reports





North Walsham Modelling

Forecast Report

ESCO Developments, Flagship Housing Group and Lovell Partnerships

22nd September 2023

Quality information

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1. Introduction

Base VISSIM Model

- 1.1 The 2022 VISSIM Base model for North Walsham has been used as a starting point to develop the forecast scenarios. AECOM developed and validated the Vissim Base model at the end of 2022.
- 1.2 The 2022 Base model was successfully calibrated and validated to replicate the existing operation during the traffic surveys for the North Walsham Model area, shown in Figure 1-1. Further details regarding the Base model operation and the calibration and validation results can be found in the VISSIM Local Model Validation Report for North Walsham: "North Walsham Local Model Validation Report."

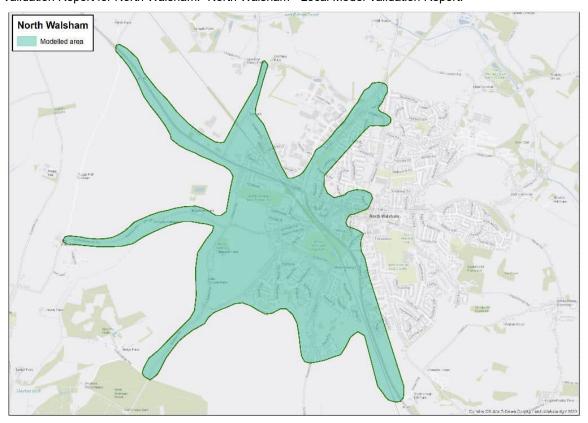


Figure 1-1 - North Walsham Modelled Area

1.3 The forecast year models have been developed for the 2036 forecast year. The models were developed for the Weekday AM and PM peak hours defined as 07:45 – 08:45 in AM and 16:30 – 17:30 in PM. Thirty-minute warm-up and fifteen-minute cool-down periods have also been modelled to saturate the network with traffic and allow journeys to be completed after the peak hour.

Model Purpose

- 1.4 The forecast models have been used to assess the operation of the network in 2036 in line with the forecast assumptions contained in the Transport Assessment (TA) for North Walsham Western Urban Extension (NWWUE). Three different scenarios: 'Do Minimum', 'Do Something', and 'Do Something with Mitigation' have been developed for the 2036 forecast year.
- 1.5 The Do Minimum scenario includes the estimated traffic growth in the area for the forecast year and proposed infrastructure changes at the Norwich Road/A149/Grammar School Road junction. The infrastructure changes are discussed in the Network Coding section.
- 1.6 The Do Something scenario has been developed using the Do Minimum scenario as a starting point. In addition to the same demand and network changes included in the Do Minimum scenario, the Do Something

- scenarios include the additional trips generated by the NWWUE which were added on top of the Do Minimum demand and the proposed Link Road through the NWWUE development.
- 1.7 The Do Something with Mitigation scenario is the Do Something scenario with a proposed mitigation on Aylsham Road. Further detail on the differences between scenarios can be found in Table 2-1.
- 1.8 The operation of the Do Minimum model has been used as a benchmark to assess the impact of the trip generation and infrastructure changes linked to the NWWUE included in the Do Something scenarios.

Report Structure

- 1.9 The remainder of the report is structured as follows:
 - Section 2 provides an overview of the forecast scenarios and outlines the development of the forecast model networks;
 - Section 3 describes the demand development methodology for future scenarios;
 - Section 4 describes the assignment methodology;
 - Section 5 presents and analyses the forecast modelling results;
 - Section 6 provides an analysis of key areas/ locations in the models; and
 - Section 7 provides a summary and conclusions.

2. Forecast Model Development

Overview

- 2.1 The North Walsham forecast models were coded using the same software version (Vissim 21.00-12) as used to develop the 2022 Base models. This section outlines the changes made to the Base models to build the forecast models.
- 2.2 Three forecast model scenarios were developed:
 - 2036 'Do Minimum' model for AM and PM peak periods;
 - 2036 'Do Something' model for AM and PM peak periods; and
 - 2036 'Do Something + Mitigation' model for AM and PM peak periods.
- 2.3 The demand and network assumptions included in each scenario have been summarised in Table 2-1.

Table 2-1 - Forecast Scenarios

Scenario	Network	Demand
Do Minimum	Base Model network + B1150/A149 Improvement	2022 Base * 2022-2036 Growth Factor
Do Something	Do Minimum network + Link Road	Do Minimum + WUE 2036 Demand
Do Something + Mitigation	Do Something network + Aylsham Road Improvement	Do Minimum + WUE 2036 Demand

Network Coding

2.4 This section discusses the committed schemes and development sites coded in the forecast scenarios. Unless otherwise stated, all the modelling elements not affected by the proposed schemes – such as the desired speed decisions, reduced speed areas, public transport, and priority rules – have been coded consistently with the 2022 Base model.

Network Coding – Do Minimum

2.5 The Do Minimum network has been updated to include the proposed new layout for the B1150 / A149 / Grammar School Road junction. The layout for this junction is shown below in Figure 2-1.

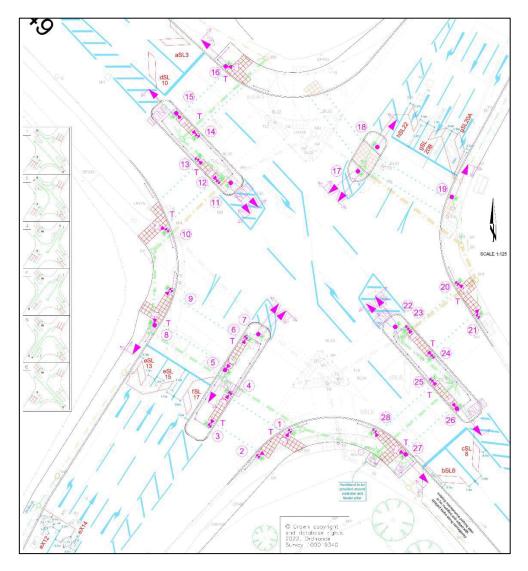


Figure 2-1 - B1150 / A149 / Grammar School Road Traffic Signal Layout

- 2.6 The timings at the signalised junctions have been optimised to reflect the predicted growth in traffic flows. The proposed signal optimisation has been consistently applied in all the forecast scenarios and assumes that the existing signal controllers will be appropriately maintained and updated in the future.
- 2.7 Furthermore, some additional priority rules have been added to the models to accurately represent the expected cooperative/ keep clear driving behaviours at locations which become more congested in the future year models, due to higher traffic flows. These rules would have no impact in the base year as this congestion is not present.

Network Coding – Do Something

- 2.8 The Do Something scenarios have been developed using the Do Minimum as a starting point, including the B1150 / A149 / Grammar School Road junction improvement shown in Table 2-1. In addition to the changes and optimisation included in the Do Minimum scenarios, the Do Something scenarios also include the new link road through the NWWUE development and the roundabout junctions at either end to connect to the existing network.
- 2.9 The 2036 scenarios include the full extent of the proposed link road within the existing road network. Figure 2-2 shows the alignment of the NWWUE link road, highlighting the key junctions and signalised crossings included in the model, which include the access junctions with the B1150 and A149, the junctions with Aylsham Road and Skeyton Road and the crossing of Weavers Way.



Figure 2-2 – Do Something Network

Network Coding – Do Something with Mitigation

2.10 The Do Something with Mitigation scenarios have been developed using the Do Something as a starting point. In addition to the changes included in the Do Something scenarios, the Do Something with Mitigation scenarios also include the proposed one-way signalised layout on Aylsham Road under the bridge. The proposed layout is shown below in Figure 2-3.

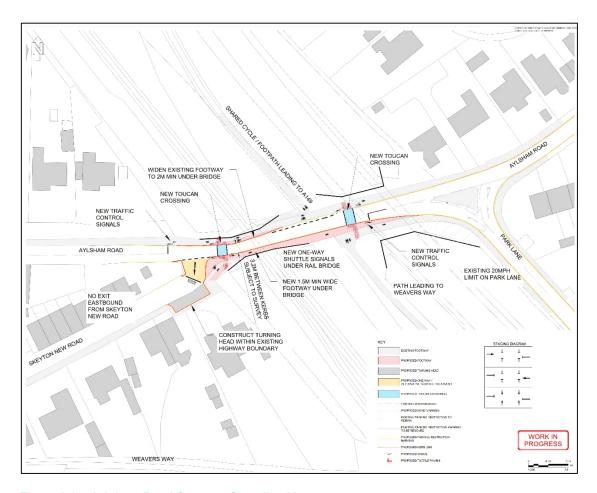


Figure 2-3 – Aylsham Road One-way Signalised Layout

2.11 The signals at the proposed one-way signalised junction have been optimised, with signal timings adapting to arrival patterns, allowing the model to provide a more realistic representation of the proposed signal operation, minimising delay.

3. Future Year Demand

Zoning

- 3.1 The zoning system developed for the Vissim Base model has also been used for the Do Minimum models.
- 3.2 The zoning system included in the Do Something scenarios has been updated to include the additional loading points for the NWWUE demand. In the Do Something scenario, seven additional zones have been added to represent access points to the development.
- 3.3 Table 3-1 shows the correspondence between the zone numbers and the development sites.

Table 3-1 - Development Zones

Development Site	Zone
Residential Zone South	25
Residential Zone Central	26
Residential Zone North Central	27
Residential Zone North	28
Local Centre / School	29
Employment North Central	30
Employment North	31

3.4 Figure 3-1 shows the locations of the VISSIM zones in the Do Something networks.

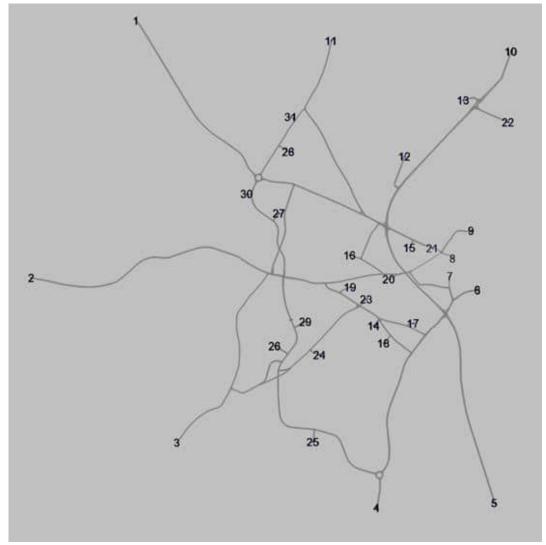


Figure 3-1 - Do Something Scenario Zones

Demand Methodology

- 3.5 The forecast Vissim demand matrices were derived using the growth factors and the trip distribution from the Transport Assessment (TA) developed by AECOM.
- 3.6 Table 3-2 shows the growth factors derived for each forecast year based on TEMPRO, as set out in the TA. These growth factors were applied to the Base model demand matrices to uplift traffic volumes for the 2036 Do Minimum scenarios.

Table 3-2 - Growth Factors

Vehicle 2036 AM 2036 PM Car/LGV 1.084 1.080 HGV 1.039 1.039

- 3.7 The NWWUE trip generation and trip distribution assumptions included in the TA have been used to derive the number of additional trips associated with the NWWUE and the distribution in North Walsham. These trips have been added to the Do Minimum scenarios to develop the Do Something forecast demand matrix forecasts.
- 3.8 Table 3-3 details the additional trips included in the Do Something models for each forecast year.

Table 3-3 - Do Something Development Demand

Development Demand 2036 AM 2036 PM

Car/LGV	1,261	1,013
HGV	12	7

- 3.9 It should be noted that the development trip totals were provided in two vehicle types: Cars/Light Goods Vehicles (LGVs) and Heavy Goods Vehicles (HGVs). However, since the Vissim models categorise Cars and LGVs as separate vehicle types, Car and LGV proportions were calculated from the base matrix and used to split the development demand.
- 3.10 The absolute demand changes for each Origin-Destination (O-D) pair were applied by vehicle class (Cars, LGVs and HGVs) to the base peak hour matrices from the Vissim base model to develop the Forecast demand matrices.
- 3.11 The forecast peak hour matrices were profiled into 15-minute periods using the same profiles used in the Vissim base model matrices to develop each 15-minute matrix, creating six matrices for each vehicle type.

Routing Assumptions

- 3.12 There are multiple routes available between the development zones and the eastern side of the town centre. For a few O-D pairs, the assignment of trips within the model area was not considered realistic, due to some town-centre networks not being included in the model area, such as King's Arms Street or Yarmouth Road (due to lack of survey data). In these cases, the model was unable to dynamically adjust routeing to respond to delay increases, as the destinations were fixed.
- 3.13 The O-D patterns were therefore adjusted in a few cases. Google Maps was used to indicate which routes would be attractive, as shown in Figure 3-2, to define adjustments to the preferred town centre destination zones for each of the development zones. These routing assumptions have been developed consistently with the TA to provide a realistic representation of the trip distribution expected in the area.

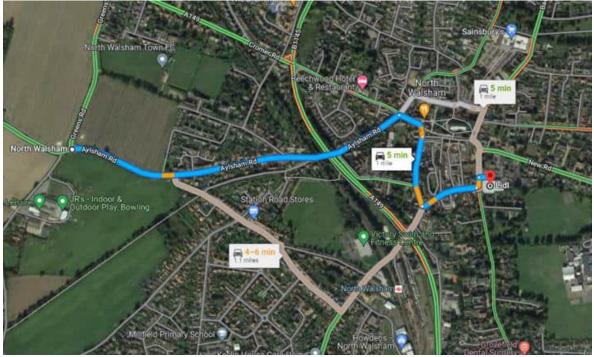


Figure 3-2 - Route Comparison from Development Location to Zone 6

4. Model Assignment

Convergence

- 4.1 The model assignment and convergence parameters for the 2036 models used the same settings as the base year models with a minor change in the Kirchhoff parameter (it was changed from 10 to 3.5), as it was not possible to converge the 2036 Do Something PM model using the same parameters defined in the Base model, as there are significant changes in future congestion patterns. The Kirchhoff parameter is consistent in all the 2036 scenarios to allow reliable comparison of Do Minimum and Do Something scenarios. Further details of the convergence process followed can be found in the North Walsham Vissim Local Model Validation Report (LMVR).
- 4.2 Fixed signal timings, based on average green times, were used during forecast model convergence, allowing the model to reach a stable convergence.
- 4.3 The Kirchoff parameter affects the flow balance between the lowest cost route for each O-D pair and the alternative routes. Analysis was undertaken of the 2036 AM model assignments, which converged using both settings, which showed that the routing changes caused by the different Kirchhoff values had a negligible effect on the model operation.

5. Model Evaluation

Introduction

- 5.1 This section presents the analysis of results for the Do Minimum, Do Something and Do Something with Mitigation forecast scenarios. The results were extracted for the following models and analysed:
 - Base (2022) AM and PM peak hours;
 - Do Minimum (2036) AM and PM peak hours;
 - Do Something (2036) AM and PM peak hours; and
 - Do Something with Mitigation (2036) AM and PM peak hours.
- 5.2 The analysis in the following section has been divided into the peak hours for each scenario, as each has unique characteristics.
- 5.3 The results were extracted from the models and averaged for 20 simulation runs with different random seeds. Different seeds randomise the release of vehicles into the network, resulting in a different chain of events, replicating daily variability.

AM Peak Hour Results

5.4 This section presents results for the modelled network in the AM period and includes an analysis of total delay, plots of average speeds and journey times within the modelled area.

Network Performance – AM Peak

5.5 The Network Performance results and average speed plots have been extracted from the models to assess the operation of the overall network. These results show the overall delays for each scenario to enable comparison of the performance of the network.

Average Delay

- 5.6 Average delay, including latent delay, has been extracted from the models in seconds per vehicle for the AM peak. The average delay is higher in all forecast scenarios when compared to the Base model, which has an average delay of 69 seconds per vehicle. The Do Minimum has 82 seconds per vehicle; the Do Something has 100 seconds per vehicle and Do Something with Mitigation has 105 seconds per vehicle.
- 5.7 The increase in average delay in the Do Something with Mitigation scenario is caused by the additional delay and routing changes in the area as a result of the proposed mitigation scheme. The results are shown in Figure 5-1 below.



Figure 5-1 – AM Average Delay Per Vehicle (In Seconds)

5.8 The AM forecast models have an average of 2 vehicles in latent demand. This result is caused by vehicles trying to join the network just as the model is finishing and is considered negligible.

Average Speed Plots

- 5.9 The average speeds have been plotted on the network for the Base and Forecast models (Do Minimum, Do Something and Do Something with Mitigation) in Figure 5-2 to Figure 5-5.
- 5.10 A comparison between the speed plots for the Base AM model and the speed plots for the forecast models indicates that the main congestion points across the network remain consistent (darker blue areas) although the increased demand results in longer queues in future.
- 5.11 The Do Minimum scenario results predict slow moving traffic/ queues which extend along B1150 Norwich Road northbound, approaching the A149 / Norwich Road / Grammar School Road signalised junction. Although there are a significant number of additional trips from the NWSUE in the Do Something model, the Do Something scenario only predicts slightly lower speeds along B1150 Norwich Road compared to the Do Minimum scenario, since the Link Road mitigates for much of the impact of the NWWUE trips.
- 5.12 The Do Something with Mitigation scenario shows a very similar performance to the Do Something. The main differences are observed in Aylsham Road, where the proposed mitigation scheme results in a minor increase in delays and queues approaching the underpass, since the signals mean vehicles have to stop. The changes on the B1150 Norwich Road are caused by the routing changes predicted by the model, as drivers change their route to avoid the additional delays on Aylsham Road.
- 5.13 The operation of other key locations identified in the model, such as Cromer Road, or the A149/ B1150 junction are broadly consistent with the existing traffic conditions in all the forecast models.

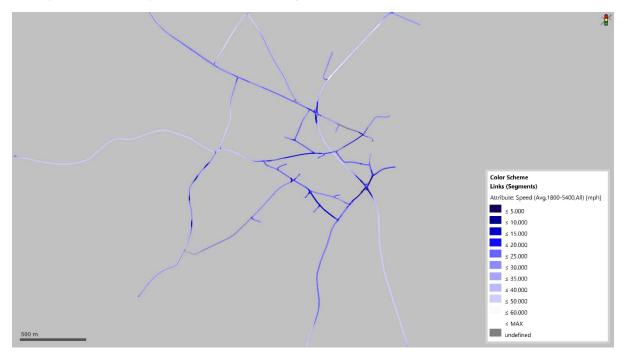


Figure 5-2 - AM Base Speeds

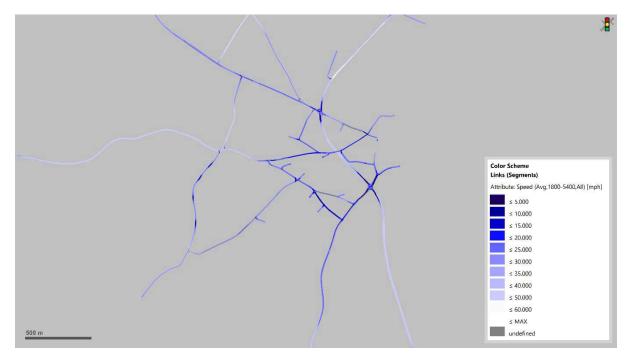


Figure 5-3 - AM Do Minimum 2036 Speeds

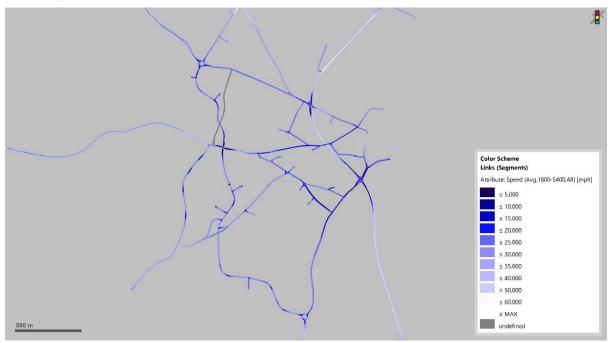


Figure 5-4 – AM Do Something 2036 Speed Plot

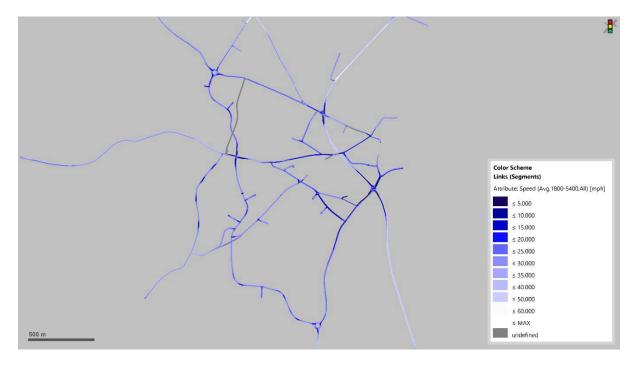


Figure 5-5 - AM Do Something with Mitigation 2036 Speed Plot

Journey Times

- 5.14 As part of the performance assessment carried out in the present study, the key journey time routes have been analysed to compare delays across the forecast scenarios in the AM peak hour.
- 5.15 Figure 5-6 and Figure 5-9 show the journey time routes selected within the model area, Journey Time Route 2 (A149 and B1145), and Journey Time Route 8 (B1150 Norwich Road, A149, and B1145).

Journey Time Route 2 - A149 and B1145

5.16 Figure 5-6 below shows Journey Time Route (JTR) 2, along the A149 and B1145.



Figure 5-6 – Journey Time Route 2 Diagram

5.17 Figure 5-7 and Figure 5-8 show the modelled results for the Base and all Forecast scenarios in the AM peak hour, for Journey Time Route 2.

- 5.18 Consistent with the average speed analysis above, the journey time results for JTR 2 show that the increase in demand included in the forecast scenarios does not significantly affect the operation of the A149 route, with only a slight increase in journey times in the Do Minimum scenario, relative to the Base year, and a more significant increase in the Do Something scenarios (with and without mitigation).
- 5.19 The additional delay in the Do Something scenarios, in both directions, is focused on the southern section, which includes the Norwich Road (B1150) junction with the A149. In the northbound direction, the overall journey time is 24 seconds higher in the Do Something scenario and 26 seconds higher for the Do Something with Mitigation, relative to the Do Minimum. In the southbound direction, the overall journey time in the Do Something is 30 seconds higher than the Do Minimum and 35 seconds higher for the Do Something with Mitigation, relative to the Do Minimum.

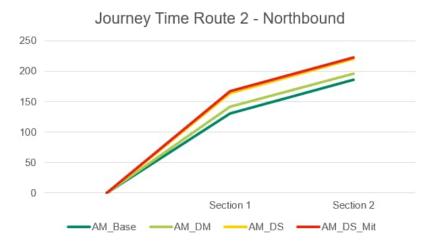


Figure 5-7 - Journey Time 2 Northbound AM



Figure 5-8 - Journey Time 2 Southbound AM

Journey Time Route 8 - B1150, A149, and B1145

5.20 Figure 5-9 below shows Journey Time Route (JTR) 8, along the B1150, A149 and B1145.



Figure 5-9 – Journey Time Route 8 Diagram

- 5.21 Figure 5-10 and Figure 5-11 show the modelled results for the Base and all Forecast scenarios in the AM peak hour, for Journey Time Route 8.
- 5.22 The northbound journey times on JTR 8 in the forecast models are higher than the Base, especially on the two southernmost sections, which include the effects of the congestion at the A149/Norwich Road/Grammar School Road Junction. The overall journey time on this route for the Do Minimum is 400 seconds, with the journey times for the Do Something and the Do Something with Mitigation 40 seconds and 41 seconds higher respectively.
- 5.23 There is a smaller difference between the journey times on JTR 8 southbound between the different scenarios, with the Do Something and Do Something with Mitigation models have a journey time 26 seconds higher (for both scenarios) across the route compared to the Do Minimum.



Figure 5-10 – Journey Time 8 Northbound AM



Figure 5-11 - Journey Time 8 Southbound AM

PM Peak Hour Results

5.24 This section presents the results for the modelled network in the PM peak hour for all modelled scenarios. It includes an analysis of total delay, average speed results and journey times within the modelled area.

Network Performance – PM Peak

5.25 The Network Performance results and average speed plots have been extracted from the models to assess the operation of the overall network. These results show the overall delays for each scenario to enable comparison of the performance of the network in each scenario.

Average Delay

- 5.26 Average delay, including latent delay, has been extracted from the models in seconds per vehicle for the PM peak. The average delay is higher in all forecast year scenarios when compared to the base year, where there is an average delay of 76 seconds per vehicle. There is an averaged delay of 129 seconds per vehicle in the Do Minimum, while the Do Something and Do Something with Mitigation models have an average delay of 115 and 125 seconds per vehicle respectively.
- 5.27 The Do Something results show that the Link road creates an alternative route in the network improving the overall performance of the model.
- 5.28 The increase in average delay in the Do Something with Mitigation scenario is caused by routing changes in the area resulting from the proposed mitigation scheme. The results are shown in Figure 5-12 below.



Figure 5-12 - PM Average Delay Per Vehicle (In Seconds)

5.29 The PM forecast models have an average of 3 vehicles in latent demand. This result is caused by vehicles trying to join the network just as the model is finishing and is considered negligible.

Average Speed Plots

- 5.30 The average speeds have been plotted on the network for the Base and Forecast PM models Figure 5-13 to Figure 5-16.
- 5.31 A comparison between the PM base year speed plots and the speed plots for the forecast models indicates that the main low speed areas across the network remained consistent (darker blue areas) differing only in magnitude.
- 5.32 There are slow speeds in the Do Minimum scenario along the B1150 Norwich Road northbound, approaching the A149 / Norwich Road / Grammar School Road signalised junction. The Do Something scenario speed plot is similar with queues along the B1150 Norwich Road, but despite the increased number of trips, the average speed is similar due to the addition of the Link Road, which reduces the number of vehicles using B1150 Norwich Road.
- 5.33 The Do Something with Mitigation scenario shows a very similar operation to the Do Something scenario, with only a slight reduction in speeds on Aylsham Road and the B1150 Norwich Road. The decrease in speeds on Aylsham Road is caused by the mitigation scheme, as the introduction of the signals means vehicles need to stop. The reduction in speeds on the B1150 Norwich Road is due to more vehicles choosing this route as due to the additional delay on Aylsham Road.
- 5.34 The operation of other key locations identified in the model, such as Cromer Road, or the A149/ B1150 junction are broadly consistent with the existing traffic conditions in all the forecast models.

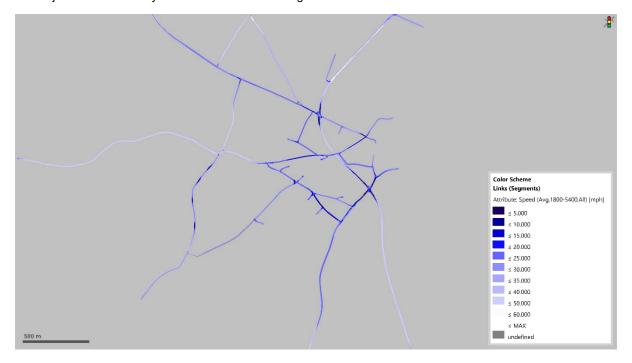


Figure 5-13 - PM Base Speeds

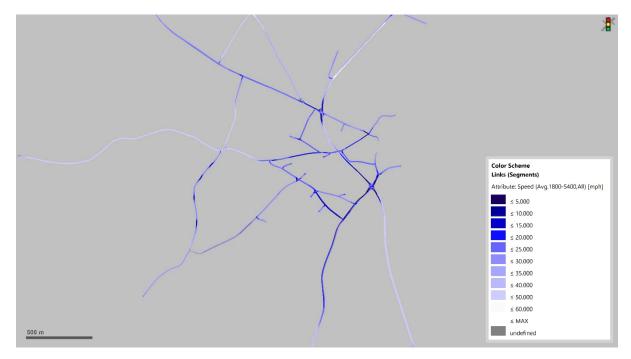


Figure 5-14 - PM Do Minimum 2036 Speeds

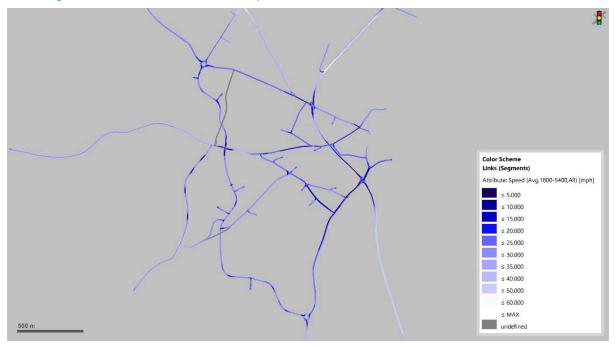


Figure 5-15 – PM Do Something 2036 Speeds

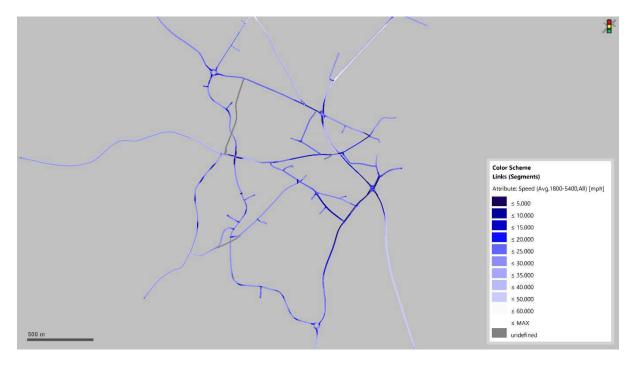


Figure 5-16 – PM Do Something with Mitigation 2036 Speeds

Journey Times - PM Peak

- 5.35 As part of the performance assessment carried out in the present study, the key journey time routes have been analysed to compare delays across the forecast scenarios in the AM peak hour.
- 5.36 Figure 5-17 and Figure 5-20 shown in the PM peak section show the key journey time routes selected within the model area, Journey Time Route 2 (A149 and B1145), and Journey Time Route 8 (B1150 Norwich Road, A149, and B1145).

Journey Time Route 2 - A149 and B1145

5.37 Figure 5-17 below shows Journey Time Route (JTR) 2, along the A149 and B1145.



Figure 5-17 – Journey Time Route 2 Diagram

- 5.38 Figure 5-18 and Figure 5-19 show the modelled results for the Base and forecast scenarios in the PM peak hour, for Journey Time Route 2.
- 5.39 The increased demand in the Do Something and Do Something with Mitigation models translates to an increased delay on the northbound approach to the A149/Norwich Road/Grammar School Road junction. This junction cannot accommodate the forecast demand in the 2036 Do Minimum PM, so is further over capacity when the development trips are added. The Do Something shows an increase in journey time of 39 seconds, relative to the Do Minimum, while the Do Something with Mitigation show an increase of 44 seconds.
- 5.40 The journey time results are not significantly different between the Do Minimum and Do Something for JTR 2 southbound on the northern section of the route; there are higher journey times in the Do Something scenario, relative to the Do Minimum on the southern section of the route, but in the Do Something with Mitigation scenario the overall journey times are only slightly higher than the Do Minimum.



Figure 5-18 - Journey Time Route 2 Northbound PM



Figure 5-19 Journey Time Route 2 Southbound PM

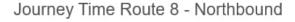
Journey Time Route 8 - B1150, A149, and B1145

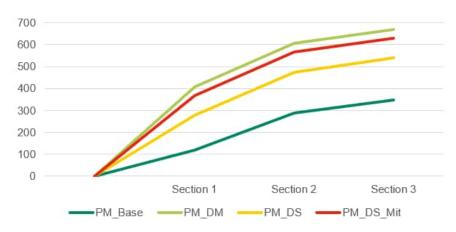
5.41 Figure 5-20 below shows Journey Time Route (JTR) 8, which runs along the B1150, A149 and B1145.



Figure 5-20 - Journey Time Route 8 Diagram

- 5.42 Figure 5-21 and Figure 5-22 show the modelled results for the Base and forecast scenarios in the PM peak hour, for Journey Time Route 8.
- 5.43 The JTR 8 northbound journey times in the 2036 forecast models are higher than the Base year, especially on the two southernmost sections, which include the effects of the congestion in the A149/Norwich Road/Grammar School Road junction. The overall Do Something journey time is 130 seconds faster than the Do Minimum and the Do Something with Mitigation is 38 seconds faster. It can be observed that despite the increase in trips from the NWWUE, the Link Road releaves some of the congestion on the B1150 Norwich Road.
- 5.44 In the Do Something with Mitigation scenario, vehicles which are deterred from routing along Aylsham Road due to the mitigation, add to the already congested B1150 Norwich Road route, increasing the journey times through the junction. However, the journey time is still faster than the Do Minimum scenario.
- 5.45 There is a smaller difference on JTR 8 southbound between the different scenarios: the Do Something is 32 seconds slower than the Do Minimum, while Do Something with Mitigation is 9 seconds slower than the Do Minimum.





5.1

Figure 5-21 – Journey Time 8 Northbound PM

Journey Time Route 8 - Southbound

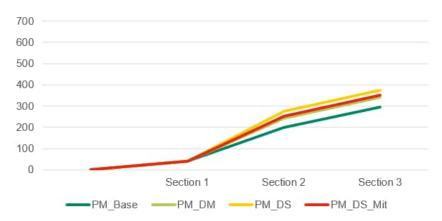


Figure 5-22 – Journey Time 8 Southbound PM

6. Junction Analysis

Introduction

6.1 This section presents the analysis of results for the junctions within the study area which have been identified from the survey data/observations in the model area as having the most significant impact on network operation.

Key Junctions

- 6.2 The key locations are defined as follows and can also be seen in Figure 6-1 below:
 - 1 Cromer Road / A149 / B1145 Junction;
 - 2 Cromer Road / Aylsham Road / Mundesley Road Junction;
 - 3 B1150 Norwich Road / A149 Junction; and
 - 4 Norwich Road / Millfield Road Junction.
- 6.3 These locations have been analysed individually in the models to extract queue and delay results for the Do Minimum, Do Something, and Do Something with Mitigation scenarios, to provide an assessment of the NWWUE development impact.
- 6.4 The junction analysis results have been extracted from the Forecast models for each junction. The Millfield Road junction has been run independently with the signals at B1150 Norwich Road / A149 / Grammar School Road being deactivated so that queues and delays can be accurately attributed to this junction.
- 6.5 It should be noted that the operation of some of these key locations depends on variable factors such as on-street parking and courtesy/give-way behaviours, which have been modelled and calibrated to observed queuing patterns/ levels of delay.



Figure 6-1 - Key Junctions in North Walsham Model Area

Cromer Road / A149 / B1145 Junction (1)

- 6.6 Figure 6-2 and Figure 6-3 show the queues and delays in the AM and PM peak hours at the Cromer Road / A149 / B1145 junction. The queue results are set out in the top junction layout and the delays are in the bottom junction layout.
- 6.7 The model results show that the NWWUE development demand included in the AM and PM Do Something / Do Something with Mitigation scenarios results in only a negligible increase in queues and delays at the junction.

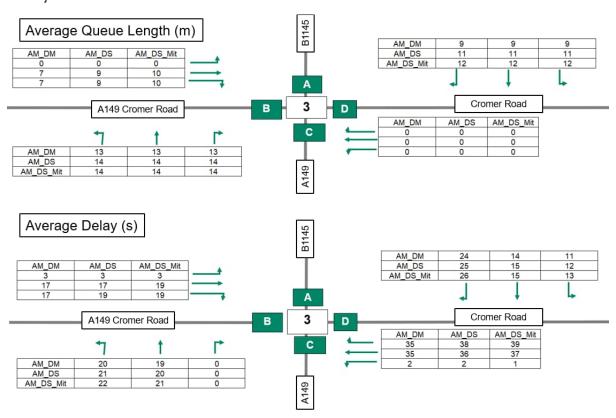


Figure 6-2 - Queues in metres and delay in seconds - AM Peak

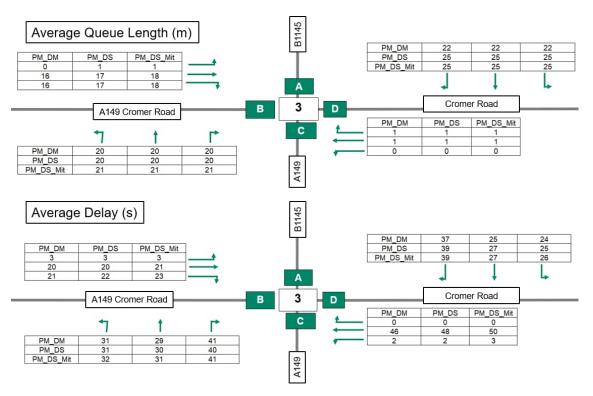
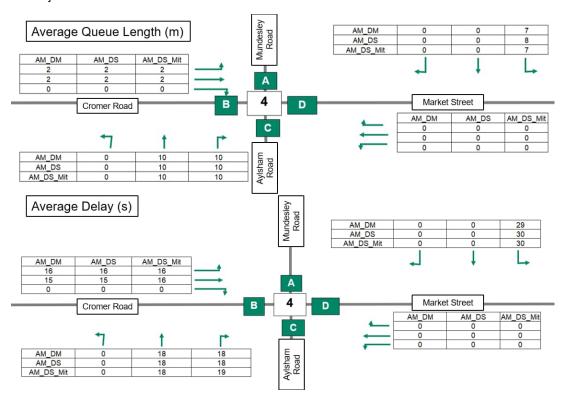


Figure 6-3 - Queues in metres and delay in seconds - PM Peak

Cromer Road / Aylsham Road / Mundesley Road Junction (2)

- 6.8 Figure 6-4 and Figure 6-5 show the queues and delays in the AM and PM peak hours at the Cromer Road / Aylsham Road / Mundesley Road junction. The queue results are set out in the top junction layout and the delays are in the bottom junction layout.
- 6.9 The model results show that the NWWUE development demand included in the AM and PM Do Something / Do Something with Mitigation scenarios results in only a negligible increase in queues and delays at the junction.



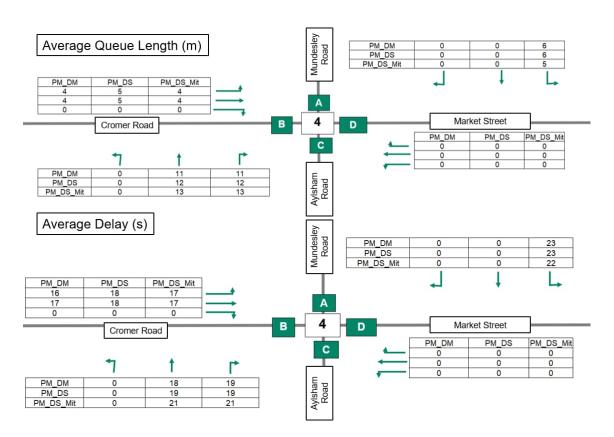


Figure 6-4 - Queues in metres and delay in seconds - AM peak

Figure 6-5 - Queues in metres and delay in seconds - PM peak

B1150 Norwich Road / A149 Junction (3)

- 6.10 Figure 6-6 shows the queues and delays at the signalised junction between Norwich Road and A149 (North Walsham Bypass) in the AM peak hour. The queue results are set out in the top junction layout and the delays are in the bottom junction layout.
- 6.11 The junction analysis results show that the A149/Norwich Road/Grammar School Road junction does not provide enough capacity to accommodate the forecasted demand in the AM Do Something / Do Something with Mitigation, resulting in significant queues and delays approaching the junction, with Norwich Road being the most affected.
- 6.12 When comparing the Do Minimum with the Do Something scenario, the addition of the NWWUE development trips in the AM Do Something scenario results in an increase in delay of approximately 150 seconds approaching the junction from the west for the left-turn, though this reduces to approximately 50-60 seconds for the straight-ahead and right-turn movements. The main capacity issue is for the left-turn movement from Norwich Road to the A149 northbound; due to the extensive queuing on this approach the left-turn flare struggles to be accessed, as vehicles need to change lanes twice, and is therefore inefficiently utilised and there is also limited green time allocated to the left-turn movement.
- 6.13 The increase in delay noted above in the Do something scenario relative to the Do Minimmum is also reflected in longer queues. Queues increase by approximately 120 metres on the Norwich Road approach. The queues generated at the A149/ Norwich Road/Grammar School Road junction reach the Norwich Road/Millfield Road junction reducing gap availability for the vehicles from Millfield Road to access Norwich Road northbound.
- When comparing the Do Something scenario with the Do Something with Mitigation, it can be observed that the mitigation scheme causes a small, but consistent increase in queues and delays at all arms of the junction. This is caused by the mitigation making Aylsham Road a less attractive route and vehicles rerouting through this junction.

6.15 The increase in delay at the other arms and movements is significantly lower at approximately 10 to 20 seconds on the remaining three arms.

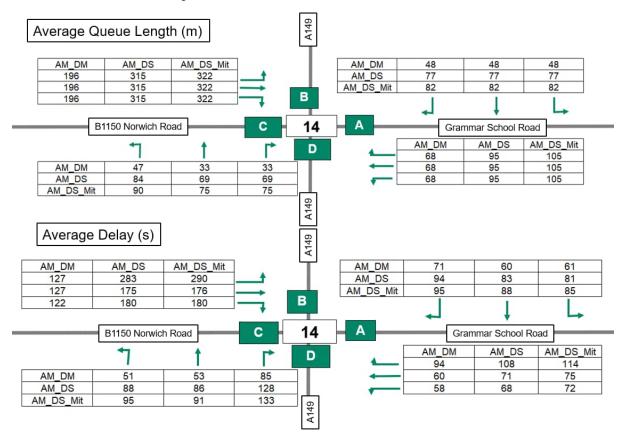


Figure 6-6 - Queues in metres and delay in seconds - AM peak

- 6.16 Figure 6-8 shows the queues and delays at the signalised junction between Norwich Road and A149 for the PM peak hour.
- 6.17 As in the AM peak, the junction analysis results show that the A149/Norwich Road/Grammar School Road junction does not provide enough capacity to accommodate the demand in any of the forecast scenarios, resulting in significant queues and delays approaching the junction, especially in Norwich Road.
- 6.18 The addition of the NWWUE development trips and link road in the Do Something scenario results in an approximate 10-second reduction in delay approaching the junction from B1150 Norwich Road. There are, however, increases in delay of approximately 30-50 seconds in the remaining three arms.
- 6.19 When comparing the Do Minimum scenario to the Do Something, the average queue length along B1150 Norwich Road was reduced by approximately 80 metres in the Do Something scenario. However, the A149 arms and Grammar School Road arm increased by approximately 50-60 metres. Delays follow similar suit as there is a decrease in the B1150 Norwich Road but an increase in the rest of the arms. This is caused by the routing allowed by the Link Road. Additionally, this effect seems to be also caused by the signals at the junction, which respond differently to the different arrival patterns.
- 6.20 When comparing the Do Somethingscenario to the Do Something with Mitigation scenario it can be observed that the mitigation causes more delay, which results in more vehicles routeing through the B1150 Norwich Road junction, increasing delay in this location. This changes the arrival patterns at the junction, meaning these is less queueing on the A149 southbound but an increased queue on Norwich Road in the Do Something with Mitigation.
- 6.21 The routing patterns in the PM peak are mainly formed by vehicles travelling to North Walsham town centre from the main access points (Norwich road and A149). The Link Road together with Aylsham Road provides a suitable alternative route that allows some of these vehicles to reach the town centre and avoid the delays at Norwich road / A149 junction. Figure 6-7, shows the different routes in blue, orange and green.

- 6.22 It should be noted that the additional delay in Aylsham Road created by the proposed mitigation makes both routes (Link Road in blue and Millfield Road in orange) less attractive, reducing the number of vehicles that choose this route over the B1150 Norwich Road / A149 junction (green in the figure).
- 6.23 This difference between Do Something and Do Something with Mitigation is not apparent in the AM peak due to the different routing patterns and the tidal nature of flows.

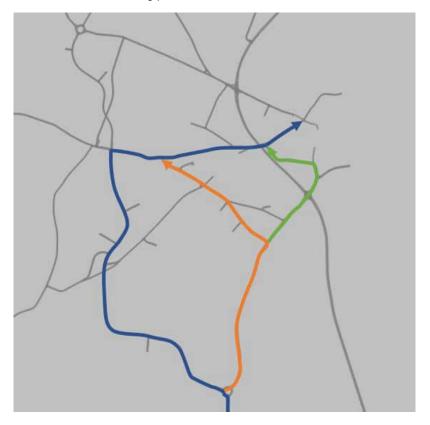


Figure 6-7 Alternative routes into North Walsham town centre from the south.

- 6.24 Changes in delay and queues on Grammar School Road and the A149 Northbound are negligible between the Do Something and the Do Something with Mitigation.
- 6.25 The difference in queues and delays between the Do Minimum and Do Something is lower than in the AM Peak, due to higher congestion levels in the PM Do Minimum scenario and the different travel patterns generated by the NWWUE development.

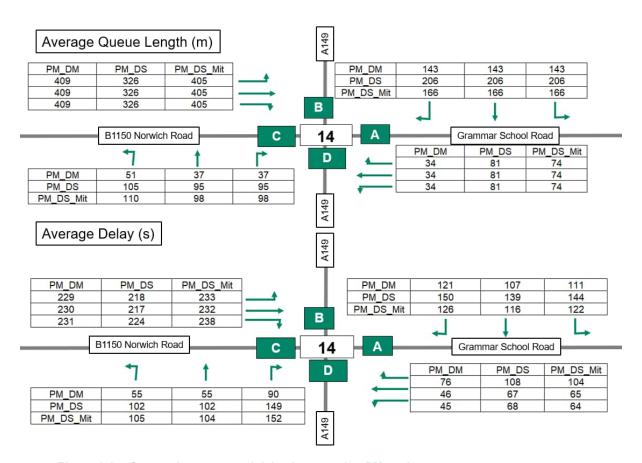


Figure 6-8 - Queues in metres and delay in seconds - PM peak

Norwich Road / Millfield Road Junction (4)

- 6.26 Figure 6-9 shows the queues and delays at the signalised Norwich Road/ Millfield Road junction for the AM peak hour. The queue results are set out in the top junction layout and the delays are in the bottom junction layout.
- 6.27 The results show no significant impact on this junction in the AM and PM peaks as the queues and delays are relatively stable after additional trips from the NWWUE development. It should be noted that the operation of this junction is likely to be affected by the queues generated at the A149/Norwich Road/Grammar School Road junction.

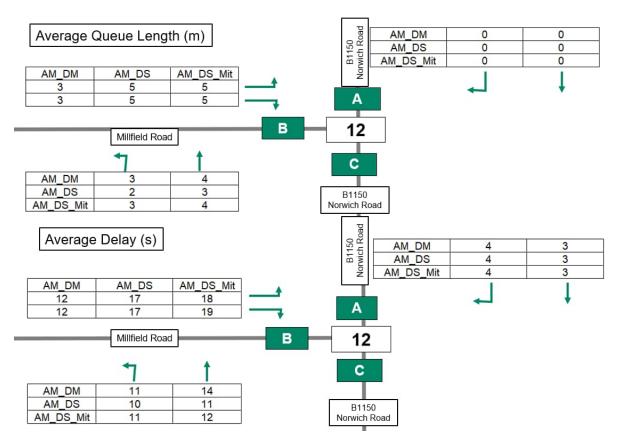


Figure 6-9 - Queues in metres and delay in seconds - AM peak

6.28 Figure 6-10 shows the queues and delays at the Norwich Road/ Millfield Road junction in the PM peak hour.

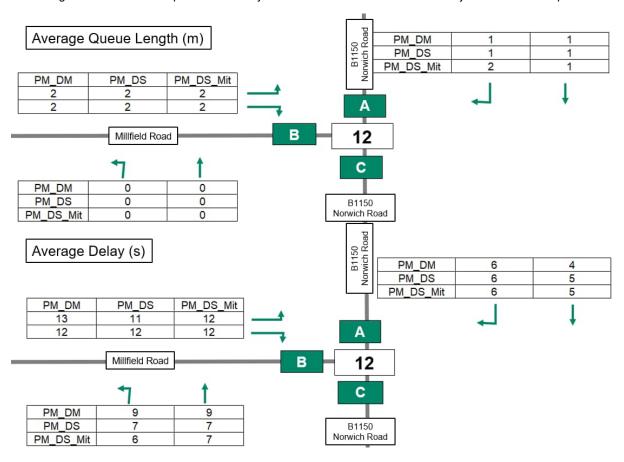


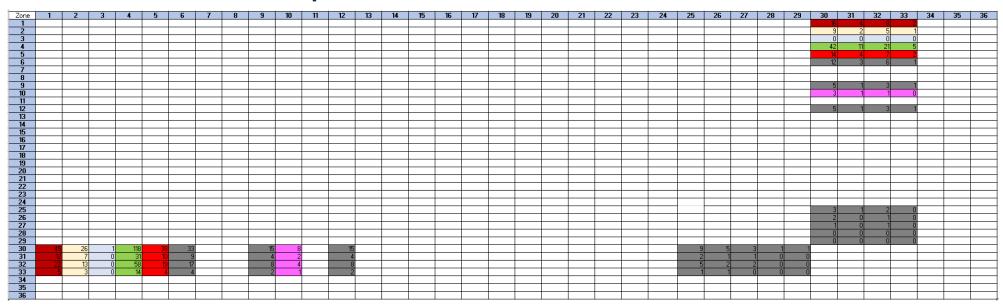
Figure 6-10 - Queues in metres and delay in seconds - PM peak

7. Conclusions

- 7.1 The forecast Vissim models have been developed and updated to represent the 2036 future year scenarios for the Do Minimum (future growth without North Walsham Western Urban Extension (NWWUE) but including the proposed infrastructure changes at the B1150 / A149 signalised junction) and Do Something (with NWWUE). A further Do Something with Mitigation model has also been developed to include the Aylsham Road one-way signalised junction under the bridge. The comparison of the Do Something and Do Minimum has been made to assess the impact of the NWWUE development.
- 7.2 The models show that the Norwich Road / A149 signalised junction struggles to accommodate the forecasted demand, resulting in longer queues and delays on all approaches which can impact other junctions such as the Norwich Road / Millfield Road junction. While there is an increase in queue and delay in the AM peak, in the PM peak, the Do Something model has a shorter queue length and lower delay when compared to the Do Minimum PM. The Do Something with Mitigation PM peak has a similar queue length and delay as the Do Minimum PM model.
- 7.3 The Do Something with Mitigation models increase slightly queue lengths and delays at other locations in the network, such as Aylsham Road with the Link Road junction, due to the mitigation reducing the attractiveness of the Aylsham Road underpass. However, these rerouting effects are considered negligible when comparing the Do Something and Do Something with Mitigation scenarios.
- 7.4 The model operation and results from the other key locations identified in the area, such as Aylsham Road or the Cromer Road/ B1145 signalised junction, show that the additional NWWUE trip generation in the 2036 forecast year will not significantly increase gueues and delays at these locations.

8. Appendix A - Demand Development

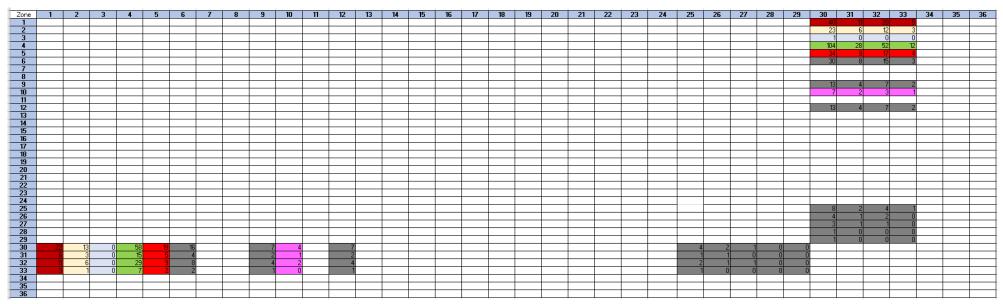
External Residential Trips – AM Peak



Internal Residential Trips – AM Peak

Zone	30	31	32	33	34	35	36
30					87	7	7
31					23	2	2
32					43	4	4
33					10	1	1
34	31	8	16	4			
35	3	1	1	0			
36	3	1	1	0			·

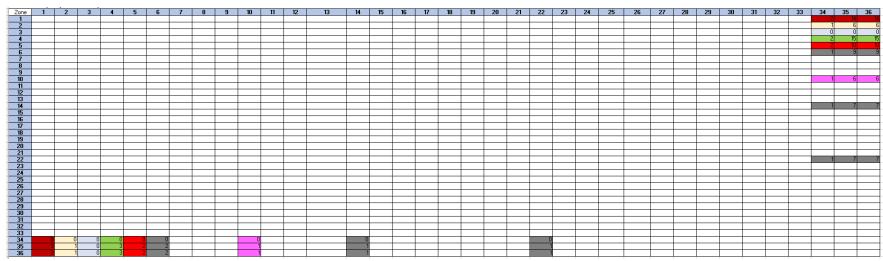
External Residential Trips – PM Peak



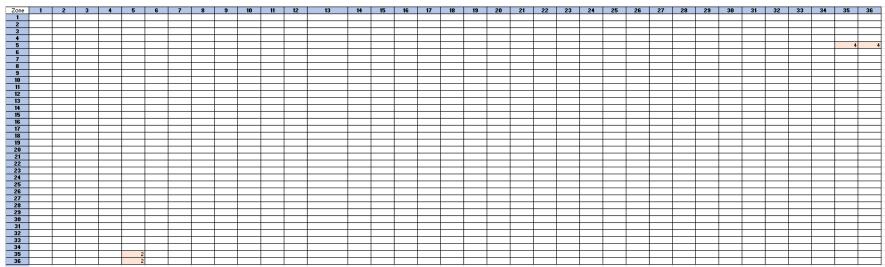
Internal Residential Trips – PM Peak

Zone	30	31	32	33	34	35	36
30					2	3	3
31					1	1	1
32					1	1	1
33					0	0	0
34	4	1	2	0			
35	5	1	2	1			
36	5	1	2	1			

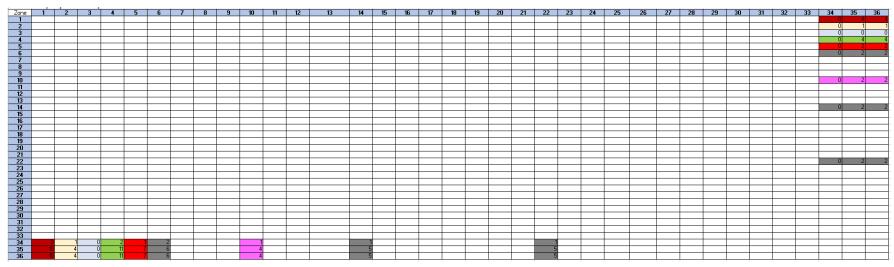
Employment Trips (Car/LGV) – AM Peak



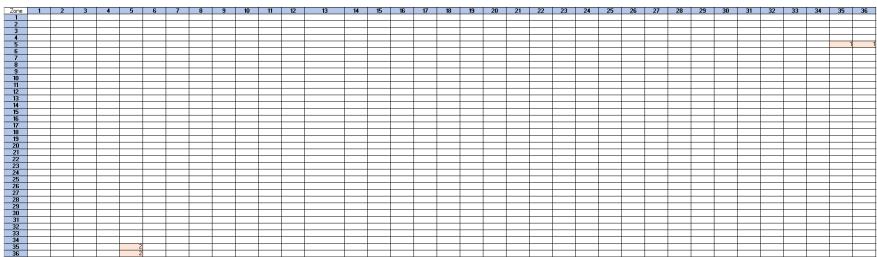
Employment Trips (HGV) – AM Peak



Employment Trips (Car/LGV) – PM Peak



Employment Trips (HGV) – PM Peak



aecom.com





Coltishall Forecast Model Report

The Client ESCO Developments, Flagship Housing Group and Lovell Partnerships

22nd September 2023

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1. Introduction

Background

- 1.1 ESCO Developments, Flagship Housing Group and Lovell Partnerships ('The Client Group') have commissioned AECOM to develop Vissim forecast models of the village of Coltishall to assess the future operation of the road network and the potential impact of the North Walsham Western Urban Extension (NWWUE).
- 1.2 The Vissim models have been developed for the 2036 year to assess the impact of the NWWUE development and predict the future traffic conditions in the model area. The growth in traffic demand and the additional demand generated by the NWWUE has been calculated in line with the Transport Assessment (TA) developed by AECOM.
- 1.3 This Forecast Modelling Report documents the development of the models from the base year scenario and presents the results of the future year assessments.

Base Vissim Model

- 1.4 The 2022 Vissim Base model for Coltishall has been used as a starting point to develop the forecast scenarios. AECOM developed and validated the Vissim Base model in late 2022.
- 1.5 The Base model was successfully calibrated and validated to replicate the existing operation during the traffic surveys, for the Coltishall modelled area, as shown in Figure 1-1. Further details regarding the Base model operation and the calibration and validation results can be found in the Vissim Local Model Validation Report (LMVR) for Coltishall.



Figure 1-1 Coltishall Vissim Model Area

1.6 The forecast year models have been developed for the 2036 forecast year. The models were developed for the Weekday AM and PM peak hours, defined as 07:45 – 08:45 and 16:30 – 17:30. Fifteen-minute warm-up and cool-down periods have also been modelled to saturate the network with traffic, before the evaluated peak hour, and allow journeys to complete after the peak hour.

Model Purpose

- 1.7 The forecast models have been used to assess the operation of the network in 2036 in line with the forecast assumptions contained in the Transport Assessment for the NWWUE. Three different scenarios: 'Do Minimum', 'Do Something', and 'Do Something with Mitigation' have been developed for the 2036 forecast year. Definition of these scenarios and the changes they include from the base modelling can be found in Table 2-1.
- 1.8 The operation of the Do Minimum model was used as a benchmark to assess the impact of the trips generated by the NWWUE which were included in the Do Something scenarios.

Report Structure

- 1.9 The remainder of the report is structured as follows:
 - Section 2 outlines the development of the forecast models and scenarios that have been tested;
 - Section 3 describes the demand development methodology for the future year;
 - Section 4 describes the assignment methodology;
 - Section 5 presents and analyses the forecast modelling results;
 - Section 6 presents and analyses the operation of the key areas; and
 - Section 7 provides a summary and concludes the forecast modelling.

2. Forecast Model Development

Overview

- 2.1 The Coltishall forecast models were coded using the same version of Vissim 21.00-12 (64-bit) used to develop the 2022 Base models. This section outlines the changes made to the Base models to build the forecast models.
- 2.2 Three forecast model scenarios were developed:
 - 2036 'Do Minimum' model for AM and PM peak periods;
 - 2036 'Do Something' model for AM and PM peak periods; and
 - 2036 'Do Something with Mitigation' model for AM and PM peak periods.
- 2.3 The networks and demand flows used for each of the scenarios are set out in Table 2-1 below.

Table 2-1 Forecast Scenarios

Scenario	Network	Demand
2036 Do Minimum	Base Model network	2022 Base * 2022-2036 Growth Factor
2036 Do Something	Base Model network	2036 Do Minimum + NWWUE 2036 Demand
2036 Do Something with Mitigation	Base Model network + Right-turn lane on Norwich Road	2036 Do Minimum + NWWUE 2036 Demand
	+ Removal of on-street parking on High Street	

Network Coding

- 2.4 There are no proposed changes to the network in the 2036 Do Minimum and Do Something scenarios, so all modelling features such as the desired speed decisions, reduced speed areas, public transport and priority rules remain consistent with the Base models.
- 2.5 The Do Something with Mitigation scenario includes a network change along B1150 Norwich Road, where a 20-metre right turn pocket is introduced to avoid right turners to the B1354 Church Street blocking northbound traffic on B1150 Norwich Road. The general layout of this infrastructure change can be seen in Figure 2-1 below.

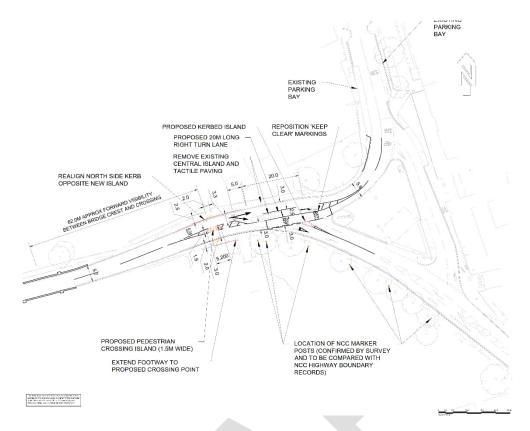


Figure 2-1 B1150 Norwich Road Proposed Infrastructure Change Layout

2.6 The Do Something with Mitigation scenario also includes removal of on-street parking along High Street in the PM peak. The PM base model includes a section of carriageway where traffic cannot pass in both directions at the same time, to replicate observed behaviour caused by the on street parking. This is not included in the AM peak base year as this behaviour/ parking was not observed, with traffic flowing freely along this section. The presence of parked cars can be seen in Figure 2-2, in an image taken from Google StreetView. This image shows that cars are parked on both sides of the street, which limits the road space available for vehicles to pass. In addition, Figure 2-3 shows a still taken from the in-vehicle footage used to survey journey times in the PM period, which shows how parked cars impede the free flow of traffic in both directions.



Figure 2-2 Parked cars on High Street



Figure 2-3 PM queuing on High Street, from floating car footage

2.7 It should be noted that the links at the edges of the forecast models have been extended to allow the models to capture the full extent of longer queues caused by the increased traffic volumes in future years. These are only theoretical extensions, so the full extent of the delay is reported in the results, however, this does not represent any change to the modelled area.

3. Future Year Demand

Introduction

The forecast demand included in the Vissim models has been derived from the Transport Assessment (TA) developed by AECOM.

Zoning

- 3.2 Since the forecast models do not include any significant network changes from the base models, the zoning system developed for the Vissim Base models remains unchanged in the forecast scenarios.
- 3.3 A map of the zones from the forecast scenarios has been reproduced below in Figure 3-1.



Figure 3-1 Vissim Forecast Model Zone Map

Demand Methodology

- 3.4 The forecast Vissim demand matrices were derived using the growth factors and the trip distribution from the TA developed by AECOM. A complete list of the development demand matrices can be found in Appendix A.
- 3.5 Table 3-1 shows the growth factors derived from the Trip End Model Presentation Program (TEMPro) for each forecast year. These have been taken from the TA. These growth factors were applied to the base model demand matrices to uplift traffic volumes for the Do Minimum scenarios.

Table 3-1 Growth Factors

Vehicle Type 2036 AM 2036 PM Car 1.084 1.080 LGV 1.084 1.080 HGV 1.050 1.050

3.6 The NWWUE trip generation and trip distribution assumptions included in the TA have been used to derive the number of additional trips and routes through Coltishall associated with the NWWUE. Table 3-2 details the additional development-related trips included in the Do Something and Do Something with Mitigation

models which would travel through Coltishall on their journey to and from the development. Full details of the forecast demand changes can be found in Appendix A.

Table 3-2 WUE Development Demand

Development Demand 2036 AM 2036 PM

Car / LGV	260	251	
HGV	0	0	

- 3.7 It should be noted that the development trip totals were provided split into two vehicle types: Cars/Light Good Vehicles (LGVs) and Heavy Goods Vehicles (HGVs). However, the Vissim models categorise Cars and LGVs as separate vehicle types. To account for this, Car and LGV proportions were calculated from the base matrix and used to split the development demand.
- 3.8 The development of additional demand from Zone 4 to itself included in the figures provided by the TA was manually reduced to 0 in the Vissim model. These trips were determined to be U-turns that would realistically occur outside the modelled area.
- 3.9 The absolute demand changes for each Origin-Destination (OD) pair were applied by vehicle class (Cars, LGVs and HGVs) to the base peak hour matrices from the Vissim base model to develop the Forecast demand matrices.
- 3.10 The forecast peak hour matrices were profiled into 15-minute periods using the same profiles used in the Vissim base model matrices to develop each 15-minute matrix, creating six matrices for each vehicle type.



4. Model Assignment and Evaluation

- 4.1 The assignment methodology used in the forecast models has been kept consistent with the base models and as set out in the LMVR.
- 4.2 The evaluation results are based on the average of 20 simulation runs with different random seeds.

 Different random seeds randomise the release of vehicles into the network, resulting in a different chain of events, replicating daily variability.



5. Model Results

Introduction

- 5.1 This section presents the analysis of results for the Base, Do Minimum, Do Something, and Do Something with Mitigation forecast scenarios. The results were extracted for the following models:
 - Base (2022) AM and PM peak hours;
 - Do Minimum (2036) AM and PM peak hours;
 - Do Something (2036) AM and PM peak hours; and
 - Do Something with Mitigation (2036) AM and PM peak hours.
- 5.2 The analysis in the following section has been divided into the AM and PM peak hours which have unique characteristics. A detailed analysis of the critical areas in the network is provided in Section 6.

AM Results

5.3 This section presents results for the full modelled network in the AM period and includes an analysis of average delay, plots of average speeds and journey times within the modelled area.

Network Performance – AM Peak

5.4 The Network Performance results and average speed plots have been extracted from the models to assess the operation of the overall network. These results provide the overall delays for each scenario to enable comparison of the performance of the network in each scenario.

Average Delay

- 5.5 Figure 5-1 shows the average delay per vehicle within the network for the four scenarios for the AM peak
- 5.6 The graph shows that there is a large increase in average delay per vehicle in the Do Minimum, Do Something, and Do Something with Mitigation scenarios, when compared to the base scenario. The Do Minimum scenario increases to an average of 118 seconds per vehicle from 84 seconds per vehicle in the Base. While the Do Something scenario has the greatest average delay, increasing to 236 seconds per vehicle. However, when the mitigation is in place, the average delay is reduced to 141 seconds per vehicle, so the mitigation is predicted to offset most of the impact of the additional NWWUE trips, so the development would only increase delay by 23 seconds on average.

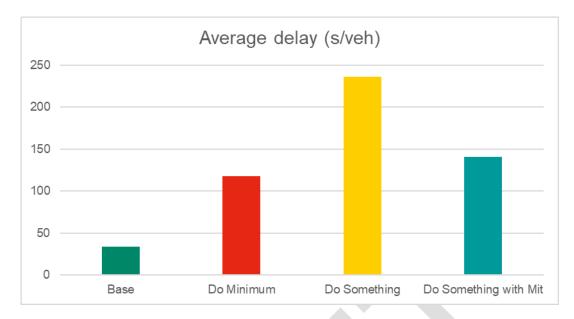


Figure 5-1 Average AM Delay

Average Speed Plots

- 5.7 The average speed results have been plotted on the modelled network for the AM Base and the three AM forecast scenarios and these are shown in Figure 5-2 through to Figure 5-5.
- 5.8 The increase in NWWUE demand included in the Do Something scenario increases queues through Colitshall, as shown in Figure 5-4. A significant proportion of this congestion originates from the right turn from Norwich Road to the B1354, just before the garage; the increase in southbound traffic volumes significantly reduces the gaps available for right-turning vehicles, blocking the eastbound and northbound movements. The speeds are higher in the Do Something with Mitigation scenario, due to the provision of a right-turn pocket, allowing traffic to flow more freely on the B1150 Norwich Road northbound.

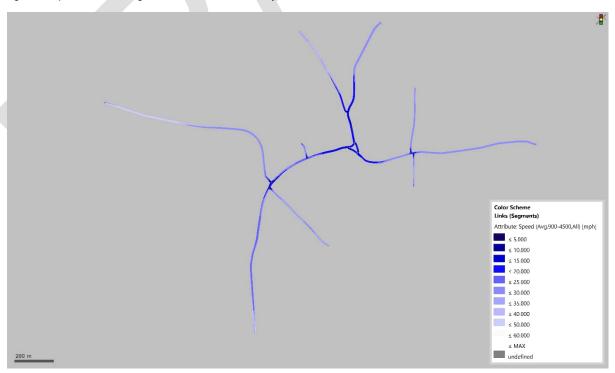


Figure 5-2 Base AM Average Speeds

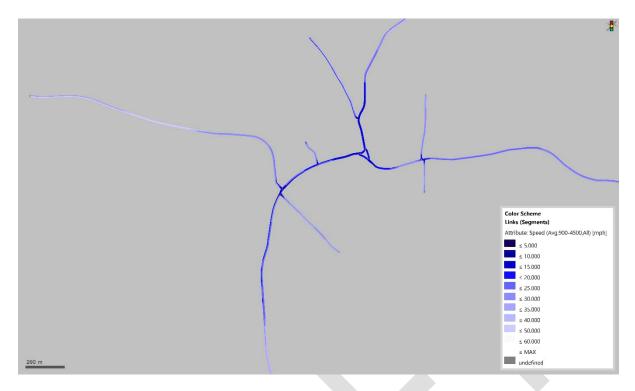


Figure 5-3 2036 AM Do Minimum Speeds

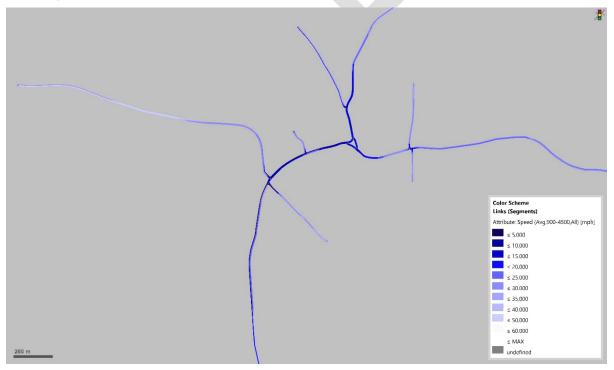


Figure 5-4 2036 AM Do Something Speeds

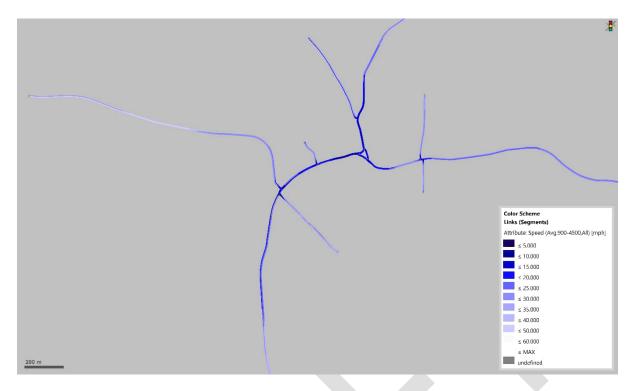


Figure 5-5 2036 AM Do Something with Mitigation Speeds

Journey Time Results - AM Peak

Journey time data has been extracted for the forecast model for the two journey time routes which were validated in the base model. The results have been used to compare delays across the forecast scenarios for the AM peak hour. Figure 5-6 shows the two journey time routes defined within the model area.

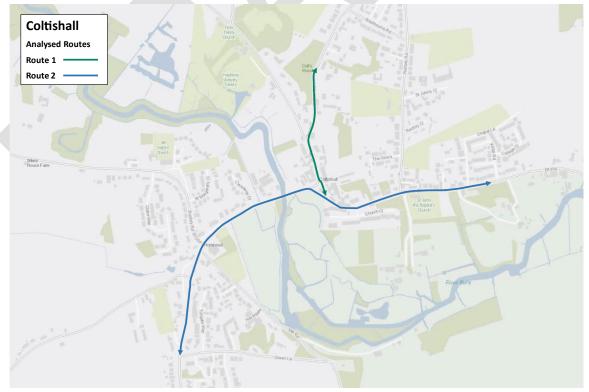


Figure 5-6 Coltishall Routes

5.10 Journey Time Route (JTR) 1 is along the B1150 Station Road and High Street to the junction of the B1150 and B1354 to the south of the Petrol Filling Station (PFS) in the centre of Coltishall. Journey Time Route

- (JTR) 2 extends along the B1150 Norwich Road from the junction with Green Lane, over the river bridge and along the B1354 to the junctions with Kings Road.
- 5.11 Figure 5-7 to Figure 5-10 show the modelled results for the Base and all forecast scenarios in the AM peak hour, for the defined routes.
- 5.12 The journey time results for the forecast models are broadly similar for all routes when compared to the Base. For the JTR 1 in the northbound direction, the Do Minimum, Do Something and Do Something with Mitigation scenarios have similar journey times to the Base in both directions, although the Do Something journey times are slightly longer overall.
- 5.13 The journey times for JTR 2 westbound are also broadly similar for all forecast scenarios, although there is an increase of just under 20 seconds in the Do Something scenarios.
- 5.14 The journey times on JTR 2 eastbound are consistent with the average speed analysis above, with significant increase in journey times in the Do Something scenario, relative to the Do Minimum due to blocking back from the right turn into the B1354, which results in longer queues. However, it can be seen than the provision of the right turn pocket in the Do Something with Mitigation scenario, significantly reduces journey times, bringing them down to a similar level to the Do Minimum scenario.

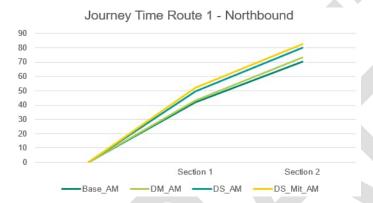


Figure 5-7 Journey Time Route 1 - Northbound



Figure 5-8 Journey Time Route 1 – Southbound



Figure 5-9 Journey Time Route 2 - Eastbound



Figure 5-10 Journey Time Route 2 - Westbound

PM Results

5.15 This section presents the network performance results for the modelled network in the PM peak hour. It includes an analysis of average delay, average speed results and journey times within the modelled area as a whole.

PM - Overall Network Performance

5.16 The Network Performance results and average speed plots have been extracted from the model to assess the operation of the entire network. These results provide an overview of the delays in each scenario for comparison.

Average Delay

- 5.17 Figure 5-13 shows the average delay per vehicle within the network across the four PM scenarios.
- 5.18 The graph shows there is a significant predicted increase in delay in the Do Minimum scenario relative to the Base year, with delay increasing from 48 seconds per vehicle to 145 seconds per vehicle. When the additional NWWUE trips are added this delay increases to 321 seconds per vehicle. The main causes of this additional delay is queuing at the parked cars (observed in the PM scenario and modelled in the base year) which allow only one direction of traffic to pass at a time.
- 5.19 The average delay per vehicle is reduced to 137 seconds per vehicle in the Do Something with Mitigation scenario, showing that the proposed mitigation offsets the impact of the development traffic in the PM peak, with average delay below the level in the Do Minimum.

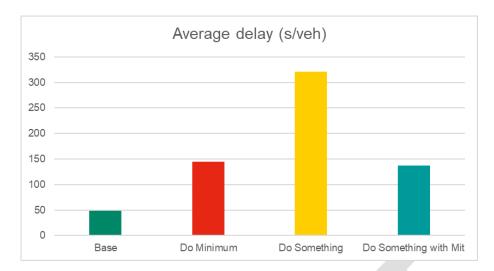


Figure 5-11 Average PM Delay

Average Speed Plots

- 5.20 The average speed results for the Base PM models and the three forecast scenarios are shown in Figure 5-12 to Figure 5-15 below.
- 5.21 The speed plots show how the additional demand added in the Do Minimum, Do Something and Do Something with Mitigation scenarios increases the queue lengths (red and dark red areas) in the network, especially along the High Street area.
- 5.22 The results show how the additional demand added to each scenario gradually increases the queue lengths (red and dark red areas) in the network, especially along the High Street area, as shown in Figure 5-14. This queue along the B1150 is caused by a section of the High Street effectively being a single lane due to on-street parking in the PM peak. Furthermore, over 90% of the NWWUE development trips that travel through Coltishall do so via the High Street, resulting in queues building up along the B1150.
- 5.23 It should be noted that the operation of this movement was highlighted as a capacity pinch point in the base model. The operation and cooperative behaviour along the one-way section of the High Street is dependent on the arrival patterns and demand levels in northbound and southbound directions.
- 5.24 The Do Something with Mitigation scenario assumes that parking restrictions will avoid vehicles parking on street in this short section of the High Street which has such a significant impact on two-way flow. The models predict that the queues and delay along High Street would be reduced significantly, increasing the speeds of vehicles along that route.

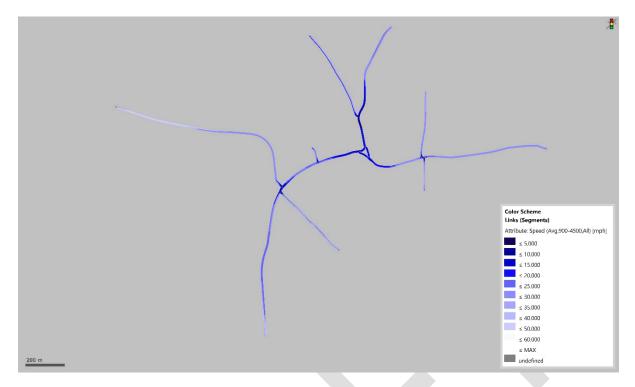


Figure 5-12 Base PM Speeds

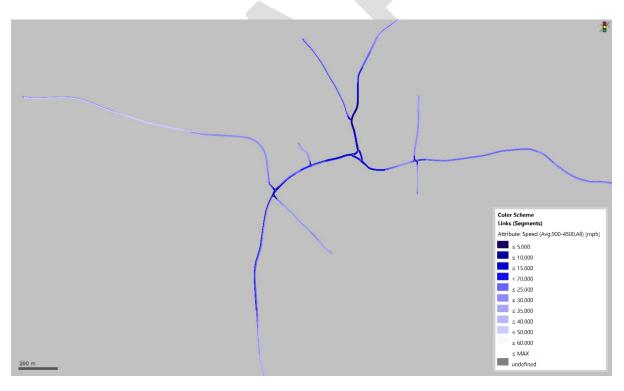


Figure 5-13 2036 PM Do Minimum Speeds

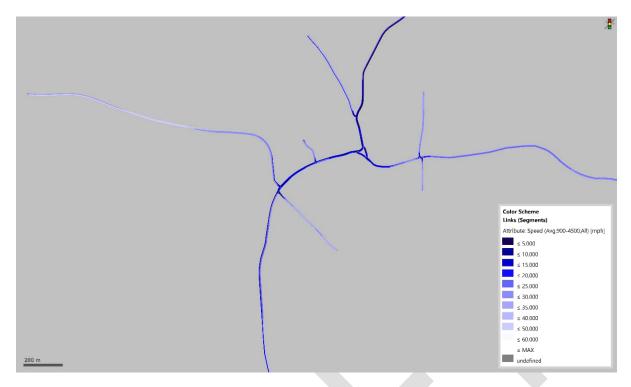


Figure 5-14 2036 PM Do Something Speeds



Figure 5-15 2036 PM Do Something with Mitigation Speeds

Journey Time Results – PM Peak

- 5.25 Modelled journey times have been extracted for the two routes which were validated in the base model and compared across scenarios. These are shown in Figure 5-6.
- 5.26 Figure 5-16 to Figure 5-19 show the modelled results for all the forecast scenarios along the base year journey time routes in the model.
- 5.27 The journey time results show that the operation of High Street, where traffic cannot pass in both directions at once at the parked cars, has an impact on the results for Journey Time Route (JTR) 1

(northbound and southbound) in the Do Minimum and Do Something scenarios, with the delay increasing as traffic volumes increase.

- 5.28 In the northbound direction, the journey time is 103 seconds in the Do Minimum and 60 seconds higher in the Do Something. In the Do Something with Mitigation scenario, where the on-street parking on the High Street is restricted, the journey time is reduced and is 17 seconds faster than the Do Minimum.
- 5.29 Similarly, in the southbound direction, the 2036 Do Minimum results show that it will take 161 seconds to travel along the full route. The journey times along this route are predicted to increase significantly in the Do Something scenario, as a result of the additional development demand. However, the model results show that the two way operation due to removal of parked cars in the Do Something with Mitigation scenario will completely offset the development impact, reducing the journey times along this route to only 67 seconds.
- 5.30 For JTR 2 eastbound the removal of on-street parking also has a positive effect, reducing the Do Something with Mitigation journey time to a similar level as the Do Minimum scenario.

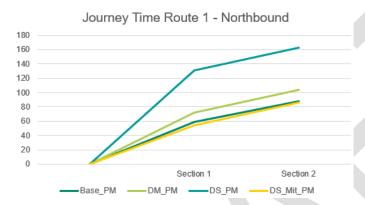


Figure 5-16 Journey Time Route 1 - Northbound



Figure 5-17 Journey Time Route 1 - Southbound



Figure 5-18 Journey Time Route 2 - Eastbound



Figure 5-19 Journey Time Route 2 - Westbound

6. Junction Analysis

Introduction

6.1 Figure 6-1 below shows the key junctions/ locations identified from the survey data/ observations in the model area that most impact network operation.

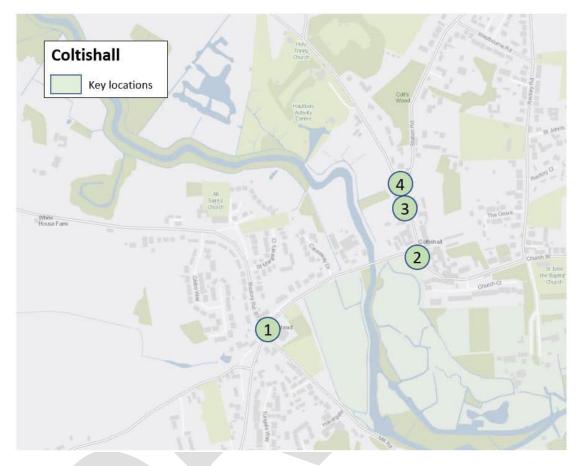


Figure 6-1 Key locations in Coltishall

- 6.2 The key locations are defined as follows:
 - 1.Rectory Road/ B1150 roundabout;
 - 2. High Street/ B1354 gyratory at the Petrol Filling Station;
 - 3. High Street at the war memorial; and
 - 4. High Street / Great Hautbois Road priority junction.
- 6.3 These locations have been analysed individually in the models to extract queue and delay results for the Do Minimum, Do Something and Do Something with Mitigation scenarios, to provide an assessment of the NWWUE development impact.
- 6.4 It should be noted that the operation of some of these critical locations depends on variable factors such as on-street parking and courtesy/give-way behaviours, which have been modelled and calibrated to observed queuing patterns/ levels of delay.

Rectory Road / Norwich Road Roundabout (1)

- 6.5 Figure 6-2 shows the queues and delays at the AM peak hour at the Rectory Road / Norwich Road Roundabout. The queue results are set out in the top junction layout and the delays are in the bottom junction layout.
- 6.6 The model results show that the NWWUE development demand included in the Do Something scenario results in a small increase in queues and delays at the junction.
- 6.7 It is worth noting that this delay and queue have been analysed with this junction operating in isolation the full model results show that the queue from B1150 Norwich Road at the gyratory would impact this junction in some scenarios.

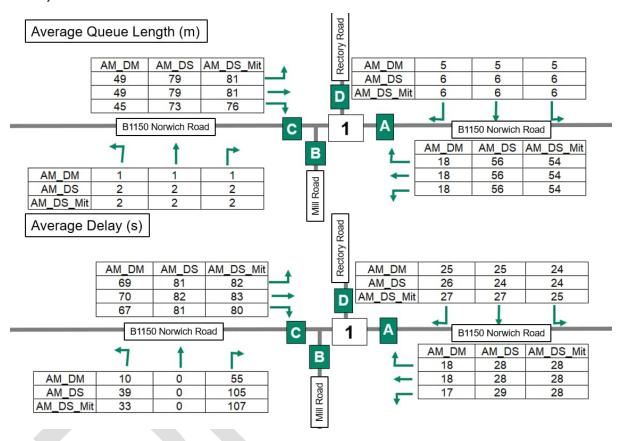


Figure 6-2 Queues in metres and delay in seconds - AM peak

- 6.8 Figure 6-3 shows the queues and delays in the PM peak hour at the Rectory Road / Norwich Road miniroundabout.
- 6.9 The model results show that the NWWUE development demand included in the Do Something scenario results in approximately 30 seconds more delay on Norwich Road northbound. The delay increase is also reflected in a longer section of slow-moving traffic approaching the roundabout, approximately 100 metres in length. The gueues and delay in the Do Something with Mitigation scenario are similar.

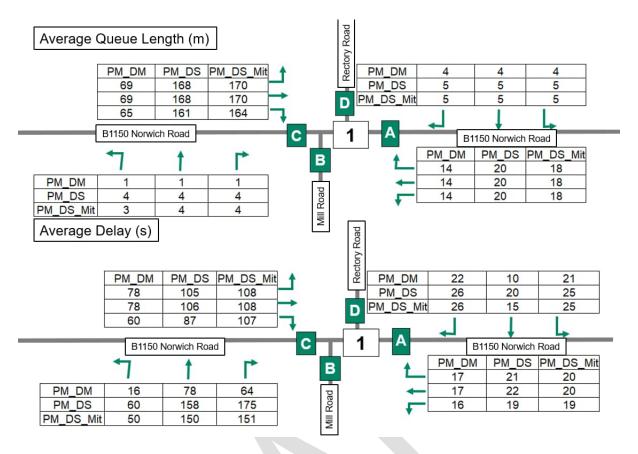


Figure 6-3 Queues in metres and delay in seconds - PM peak

Norwich Road and B1354 Gyratory (PFS) (2)

- 6.10 Figure 6-4 shows the queues and delays at the gyratory between Norwich Road and B1354 in the AM peak hour.
- 6.11 The model results show that the NWWUE development trips in the Do Something scenario result in approximately 80 seconds more delay on the eastbound approach to the gyratory. The increase in delay is also reflected in longer queues, approximately 390 metres in length, on the eastbound approach.
- 6.12 The junction analysis results show that the right turn from Norwich Road to the B1354, just before the Petrol Filling Station (PFS), is over capacity with the Do Something forecast trips. The additional southbound traffic volumes in this scenario result in fewer gaps for right turners, so right turners block vehicles travelling ahead.
- 6.13 The results for Do Something with Mitigation scenario, where a right turn pocket is provided, has a similar queue length and delay as the Do Minimum scenario along B1150 Norwich Road eastbound, effectively mitigating the impacts of the NWWUE development.
- 6.14 There are no significant increases or reductions in delay across the other arms.

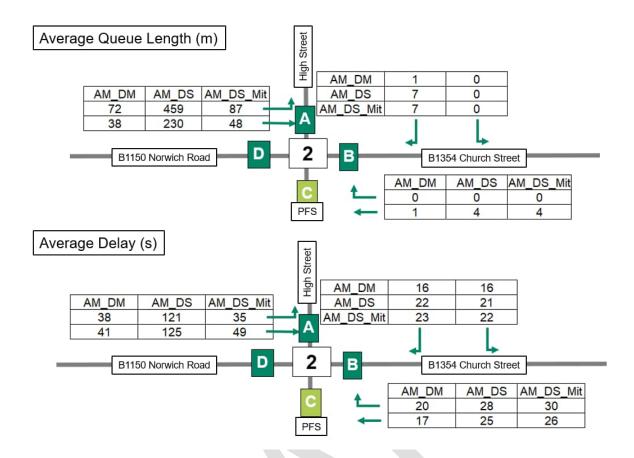


Figure 6-4 Queues in metres and delay in seconds - AM peak

- 6.15 Figure 6-5 shows the queues and delays at the gyratory between Norwich Road and B1354 (PFS) in the PM peak hour.
- 6.16 The model results show that the NWWUE development demand in the Do Something scenario increases queues and delays along B1150 Norwich Road eastbound by approximately 150 metres and 40 seconds respectively. The Do Something with Mitigation scenario, however, reduces the queues and delays to lower levels that in the Do Minimum scenario; the mitigations (right turn pocket and removal of on-street parking o the High Street), effectively mitigate the impacts of both the NWWUE and the projected growth in the area.

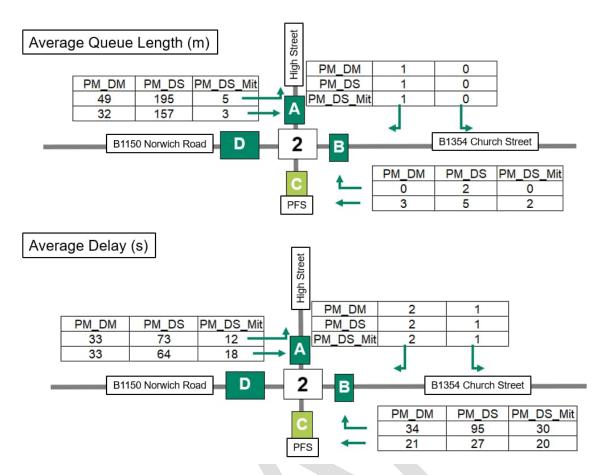


Figure 6-5 Queues in metres and delay in seconds - PM peak

High Street (3)

- 6.17 Figure 6-6 shows the queues and delays at High Street northbound and southbound in the AM peak hour.
- 6.18 There are no queues and no significant delays in any scenarios, which is consistent with the Base model where there are no vehicles parked on-street in the AM causing vehicles to give way.

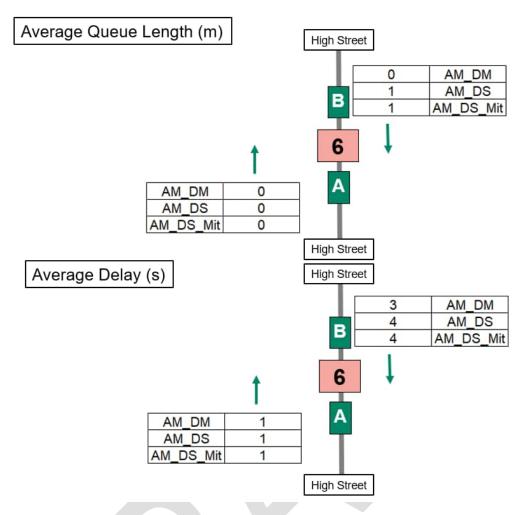


Figure 6-6 Queues in metres and delay in seconds - AM peak

6.19 Figure 6-7 shows the queues and delays on the High Street in the PM peak hour.

The Do Minimum model results show a southbound queue of approximately 120 metres long and 108 seconds of delay caused by the section where two way flow isn't possible, which is caused by the on-street parking.

- 6.20 The Do Something scenario shows a significant increase in the queues and delays due to the NWWUE development demand along this route. It should be noted that due to the cooperative nature of the calibrated driving behaviour in the model where parking limits capacity, the increase in queue lengths is not directly related to the direction of the flow.
- 6.21 The Do Something with Mitigation scenario, which removes the on-street parking on High Street, removes all restrictions along the road therefore allowing traffic to flow freely without having to give way. This means that there are average queue lengths of one metre and an average delay of 14 seconds along the southbound movement.

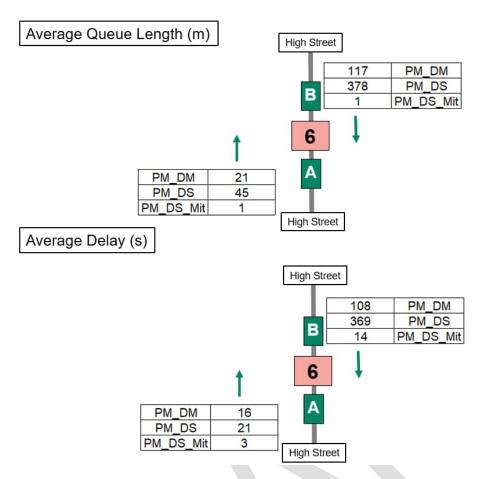


Figure 6-7 Queues in metres and delay in seconds - PM peak

High St / Gt Hautbois Rd / Station Rd Junction (4)

- 6.22 Figure 6-8 shows the queues and delays at the High Street / Great Hautbois Road / Station Road priority junction in the AM peak hour.
- 6.23 There are no average queues along High Street or Great Hautbois Road and an insignificant average queue length on Station Road in any of the forecast scenarios. There is a slight increase in delay and queue lengths from the Do Minimum to Do Something scenario along the Station Road arm, but this junction is predicted to operate within capacity when assessed in isolation.

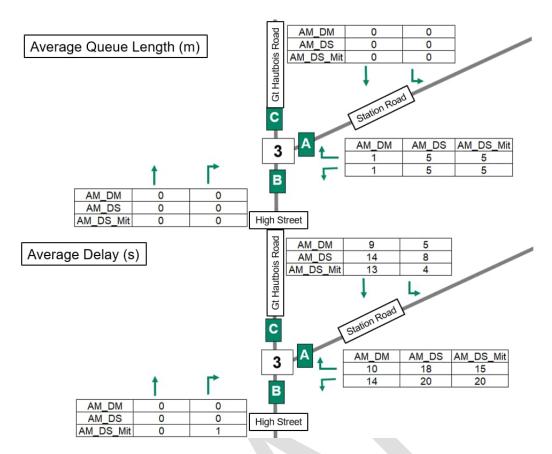


Figure 6-8 Queues in metres and delay in seconds - AM peak

6.24 Figure 6-9 shows the queues and delays on the High Street in the PM peak hour for the different scenarios tested. There is a slight increase in delay on Great Hautbois Road, however the junction operates within capacity when assessed in isolation.

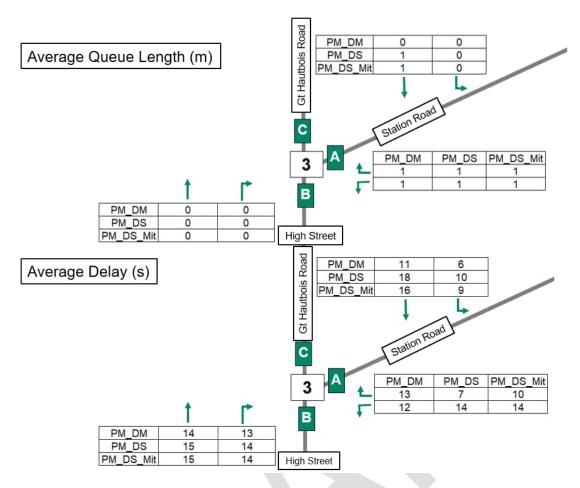


Figure 6-9 Queues in metres and delay in seconds - PM peak

7. Conclusions

- 7.1 The 2036 forecast Vissim models were developed to assess future network conditions and the impact of the North Walsham Western Urban Extension (NWWUE) development.
- 7.2 The predicted demand growth and the additional demand generated by the NWWUE taken from the Transport Assessment (TA) was added to the 2022 Vissim Base model demand to calculate the Vissim forecast demand for all the modelled scenarios.
- 7.3 The analysis of the modelling results has highlighted two key locations in Coltishall where increased queuing and delay are predicted in 2036 withinout the NWWUE development (the Do Minimum scenario). The models predict that these queues and delays will be significantly worsened as a result of the increase in traffic from the NWWUE.
- 7.4 Mitigations were identified and tested in the Do Something with Mitigation scenario: provision of a right turn pocket into the B1354 from Norwich Road to avoid blocking of the Norwich Road and removal of on street parking on a short stretch of the High Street to allow two-way movement. The models predict that almost all the development impact observed in the Do Something scenario in the AM and PM peaks would be mitigated for and that the performance of the network through Coltishall would be similar to the Do Minimum scenario with the mitigations in place.



Appendix A – Demand Development Matrices

Table 7-1 2036 AM Forecast Demand

Zone	1	2	3	4	5	6	7	8	9	Sum
1				0.6						0.6
2				2.5						2.5
3										0.0
4	0.4	0.7		2.8		1.5			188.3	193.7
5										0.0
6				1.1						1.1
7				0.6						0.6
8										0.0
9				61.4						61.4
Sum	0.4	0.7	0.0	69.0	0.0	1.5	0.0	0.0	188.3	

Table 7-2 2036 PM Forecast Demand

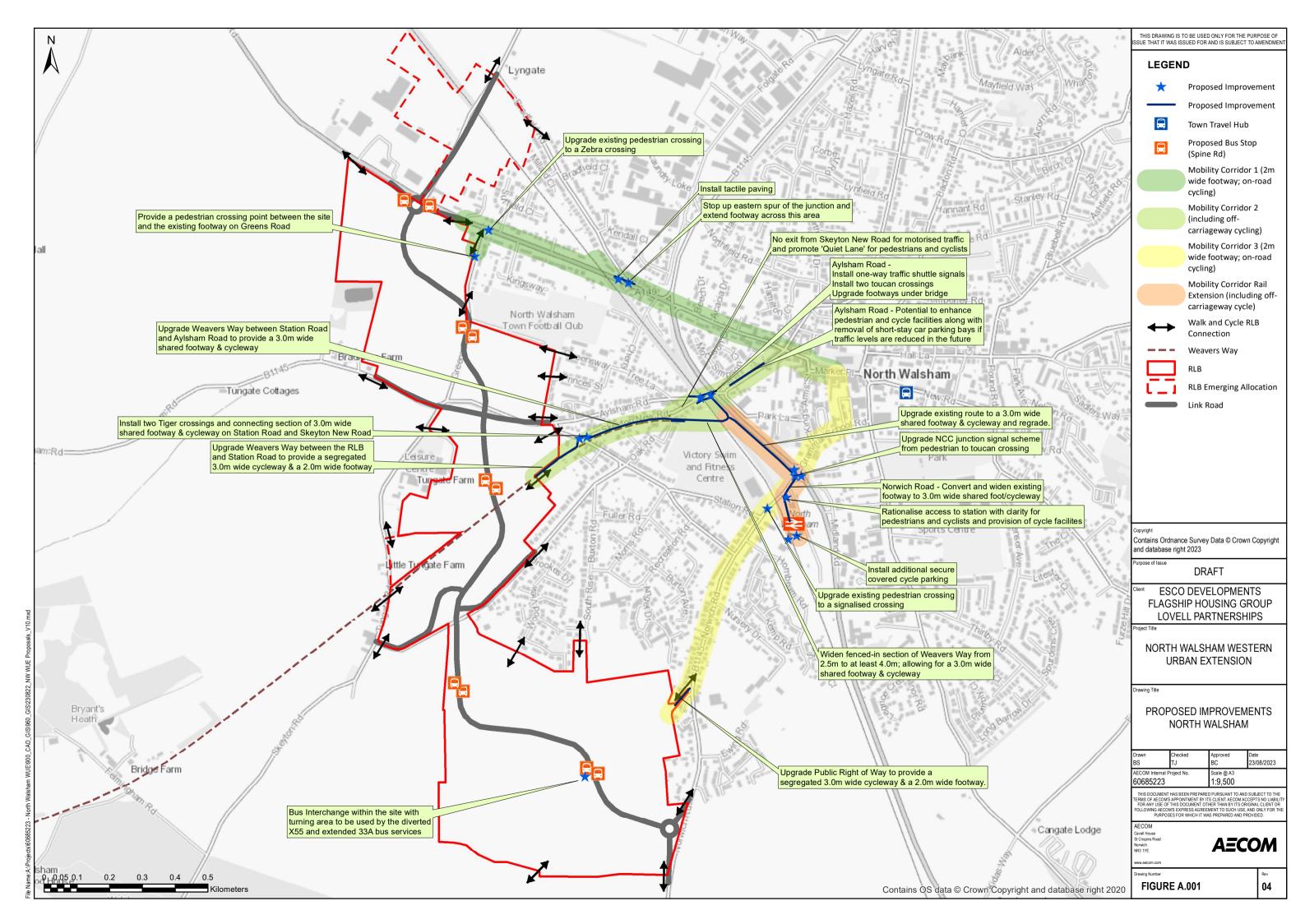
Zone	1	2	3	4	5	6	7	8	9	Sum
1				0.4						0.4
2				0.6						0.6
3										0.0
4	0.7	2.9		2.9		1.3			71.8	79.6
5										0.0
6				1.4						1.4
7				0.4						0.4
8										0.0
9				168.6						168.6
Sum	0.7	2.9	0.0	174.3	0.0	1.3	0.0	0.0	71.8	-

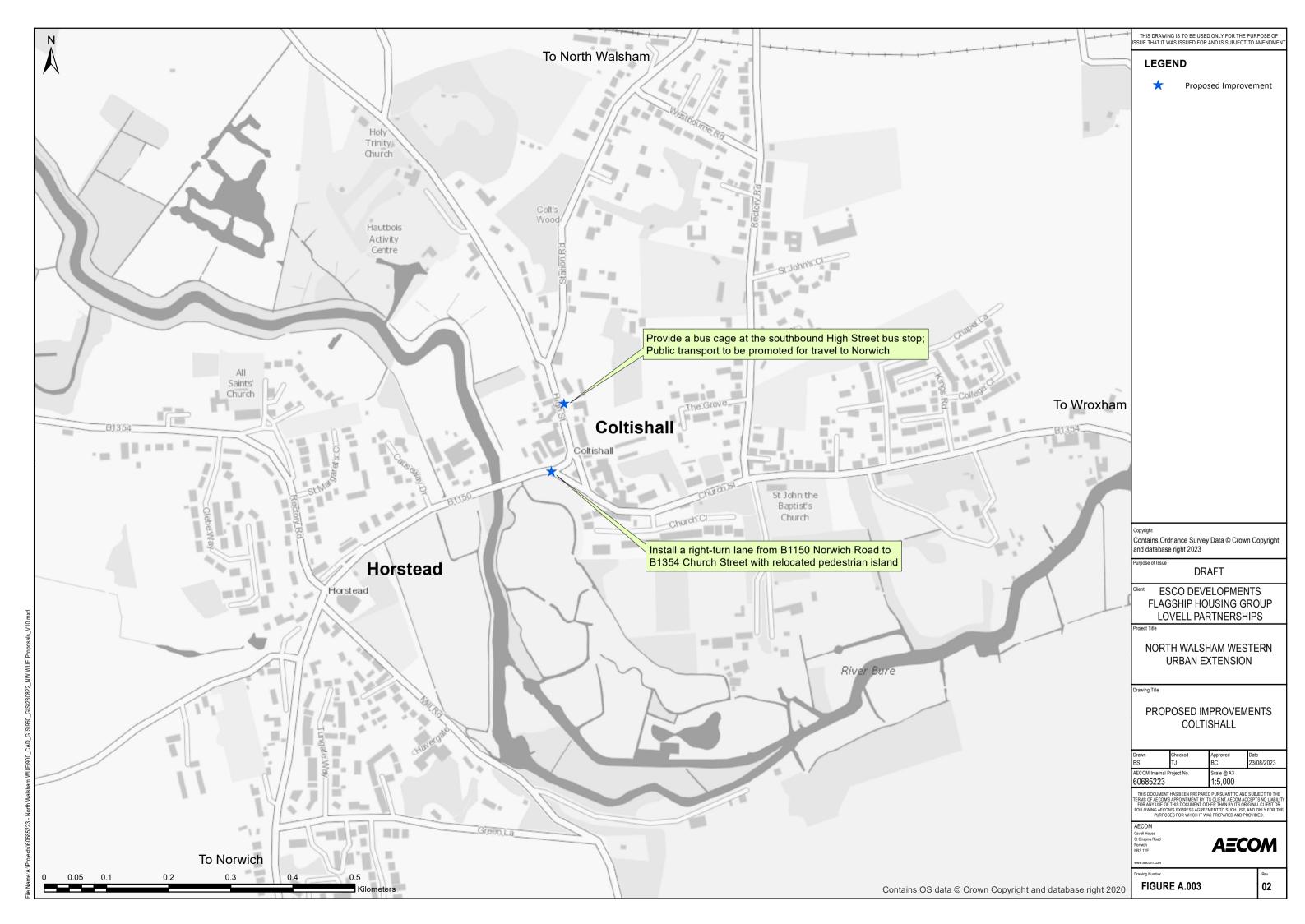
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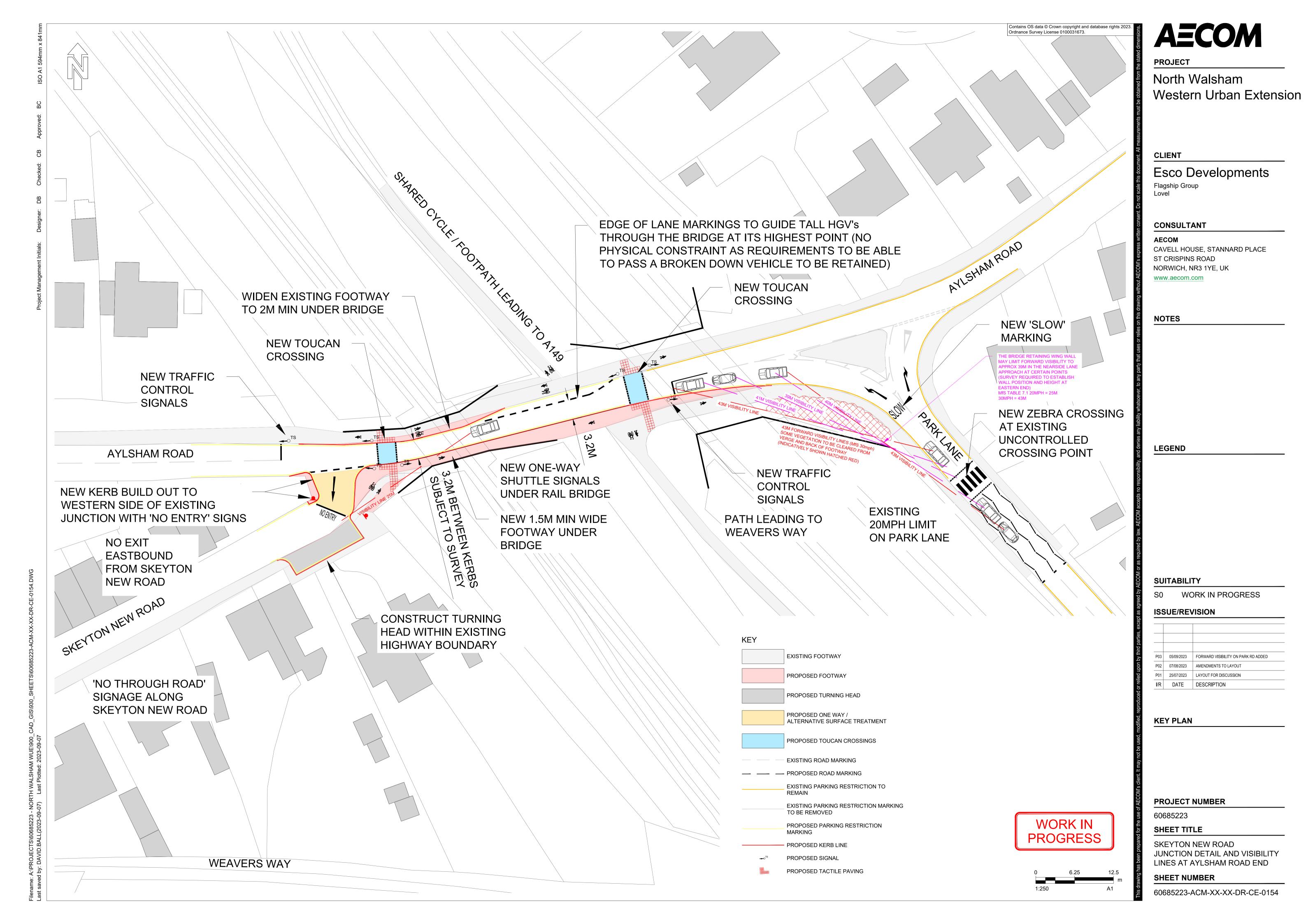


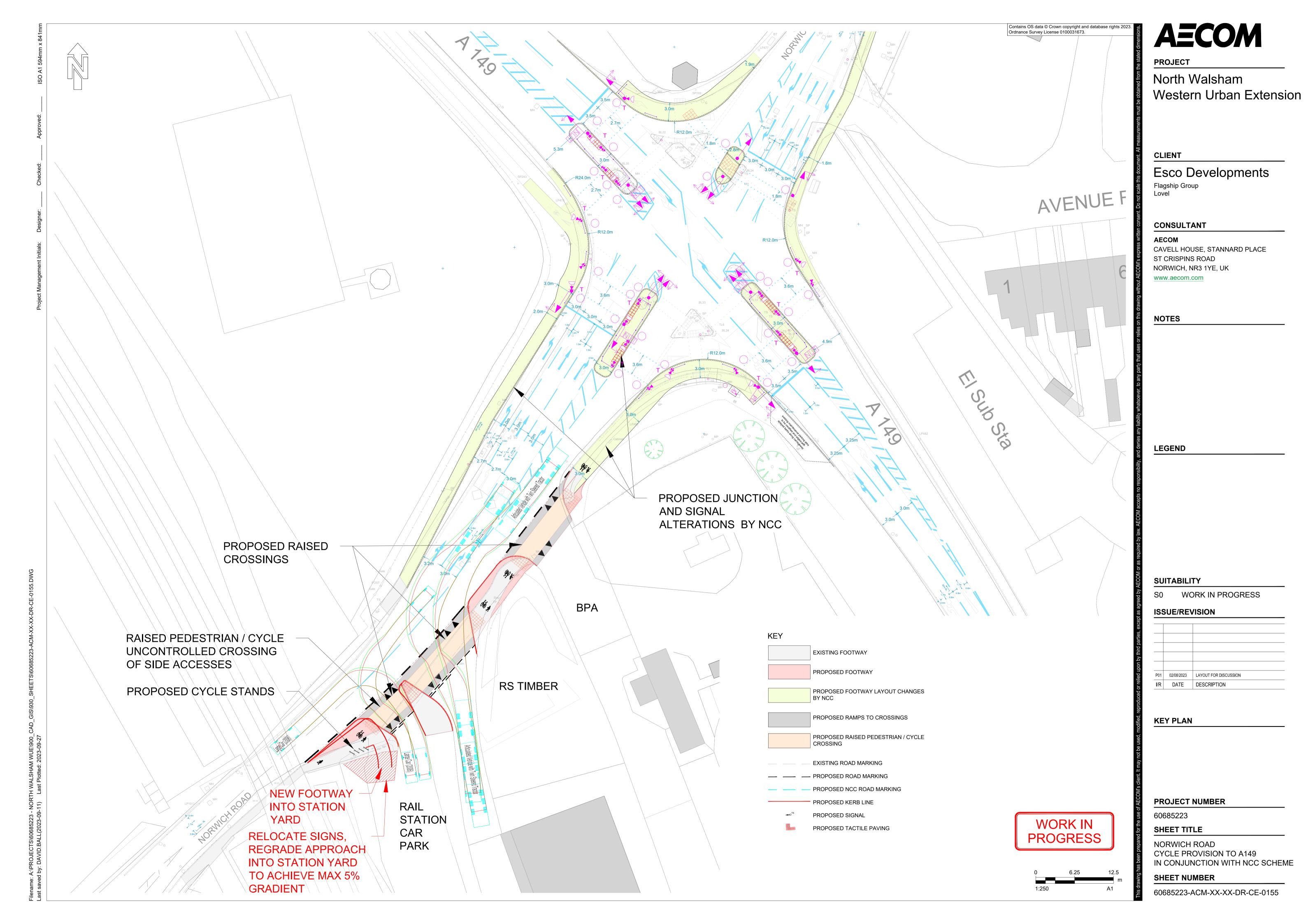
Appendix F – Proposals and Design Drawings

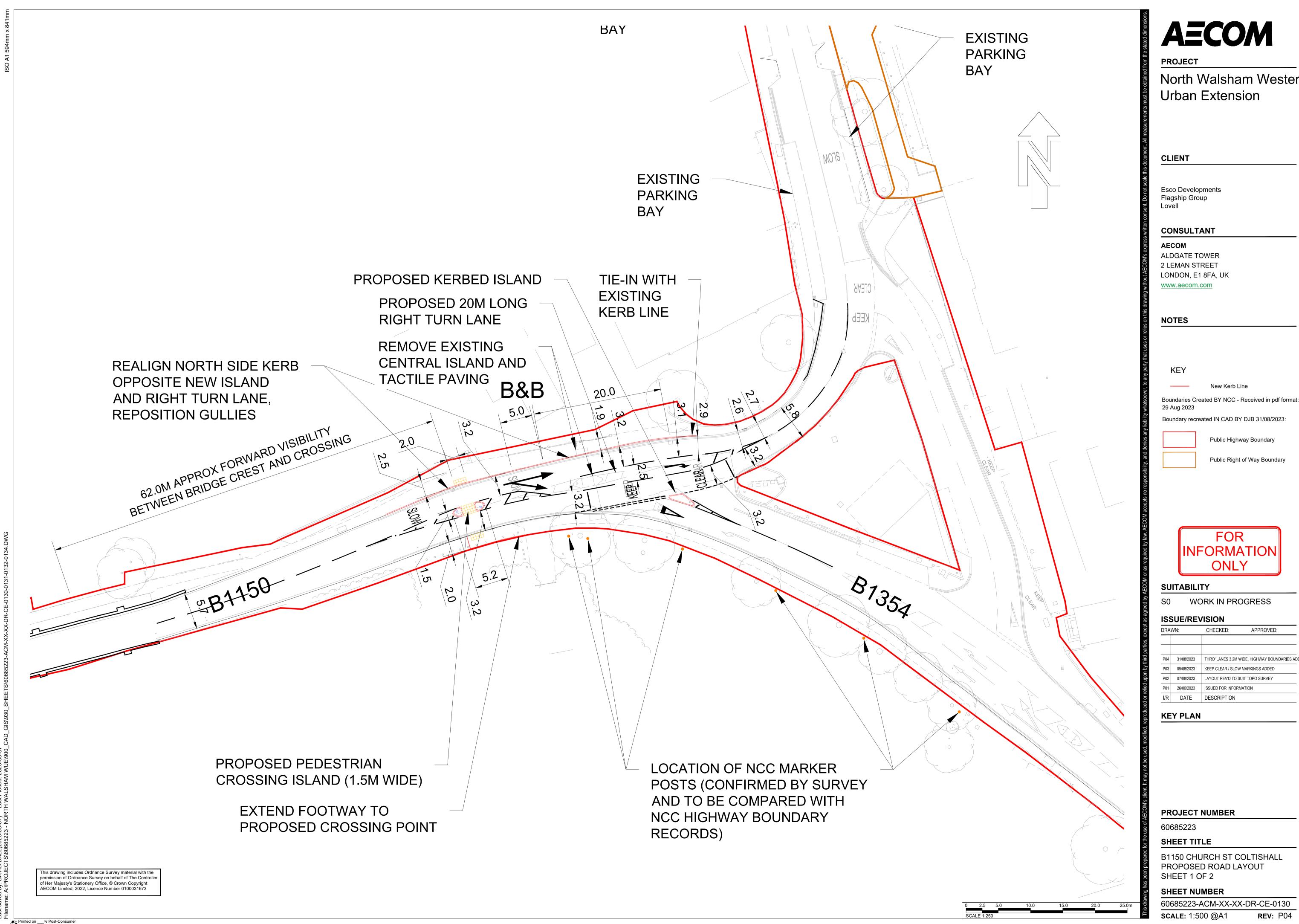












North Walsham Western

DRAWN.		CHECKED.	AFFROVED.
P04	31/08/2023	THRO' LANES 3.2M	WIDE, HIGHWAY BOUNDARIES ADI
P03	09/08/2023	KEEP CLEAR / SLOV	V MARKINGS ADDED
P02	07/08/2023	LAYOUT REV'D TO S	SUIT TOPO SURVEY
P01	26/06/2023	ISSUED FOR INFOR	MATION
I/R	DATE	DESCRIPTION	



AECOM

PROJECT

North Walsham Western **Urban Extension**

CLIENT

OWNER/CLIENT

Esco Developments Flagship Group Lovell

CONSULTANT

AECOM

ALDGATE TOWER 2 LEMAN STREET LONDON, E1 8FA, UK

www.aecom.com

NOTES

INFORMATION

SUITABILITY

WORK IN PROGRESS

ISSUE/REVISION

DRAWN:		CHECKED:	APPROVED:	
P01	07/08/2023	ISSUED FOR INFORMA	TION	
I/R	DATE	DESCRIPTION		

KEY PLAN

PROJECT NUMBER

60685223

SHEET TITLE

NORTH WALSHAM ROAD COLTISHALL PROPOSED BUS STOP

SHEET NUMBER

60685223-ACM-XX-XX-DR-CE-0133

SCALE: 1:500 @A1

Appendix G – Stage 1 Road Safety Audit Report and Designers Response





NORTH WALSHAM WESTERN EXTENSION: B1150 NORWICH RD CYCLE IMPROVEMENTS & AYLSHAM RD SHUTTLE WORKING

STAGE 1 SAFETY AUDIT

REPORT REF: **B1150/025** August 2023

Report Prepared for: AECOM



Report Author: Nevil Calder BSc(Hons) CEng MICE MCIHT MSoRSA NH Cert Comp

Report Status:

Issue	Status	Purpose	Name/Signature	Date
1	Stage 1 Safety Audit Report	Client issue	Nevil Calder	22/08/23
2	Designer's Response	Designer response to Safety Issues raised	Bevin Carey	29/09/23
Choose an item.	Choose an item.	Choose an item.		



INTRODUCTION

This report contains the results of a Stage 1 Safety Audit carried out on the above scheme. The Audit was carried out at the request of AECOM on behalf of Norfolk County Council Growth and Development. A formal Audit Brief was not provided.

The Audit Team is independent of the project design team and has had no involvement with the project. The Audit Team membership was as follows:-

Nevil Calder BSc(Hons) CEng MICE, MCIHT, MSoRSA (Audit Team Leader)

Principal Engineer Highway Safety

WSP

Kevin Allen BEng (Hons), I Eng, MCIHT, MSoRSA (Audit Team Member)

Project Engineer

Network Safety + Sustainability

Norfolk County Council

The Audit took place via online conferencing on 16 August 2023. The audit comprised an examination of the supplied documentation (see Appendix A) and a site inspection by the Audit Team Leader on 22 August 2023 at 10:20 which lasted around 30 minutes. During the site visit the weather was sunny and the road surface dry. Traffic flows were moderate and generally free flowing.

The terms of reference are as described in Community and Environmental Services Highways Service Manual Procedure SP03-07-P01. The Auditors have examined and reported only on the road safety implications of the scheme within the main report.

The proposal involves traffic management improvements in North Walsham in connection with the western urban extension of the town. The audited scheme comprises provision of shareduse foot/cycleway on approach to the railway station on Norwich Rd, together with introduction of signalised shuttle working on an existing narrow section of Aylsham Rd and foot/cycleway provision. The latter also involves a short length of one-way restriction on Skeyton New Road at its junction with Aylsham Rd.

3 File Ref: B1150/025 Audit Date: 16/08/2023



The auditors have reviewed the five year (to end Mar 2023) collision record for the location. During this period there were 4 personal injury collisions (1 serious, 3 slight) recorded in vicinity of the Norwich Rd scheme but they appear to have no bearing on the proposals. There were no recorded collisions in vicinity of the Aylsham Rd proposals.

A comments section has been included in Appendix B. The issues noted are not necessarily safety issues. They relate either to wider network implications, safety issues identified outside the scope of the audited scheme or suitability of a particular design choice.



ITEMS RAISED AT PREVIOUS AUDIT

The Audit Team are not aware of any previous audit of this scheme.

ITEMS RAISED AT THIS STAGE 1 AUDIT

1.0 General

1.1 Problem – vehicle collisions with NMUs

Location – Aylsham Rd proposed signalised NMU crossings

The proposed location of 'toucan style' crossings within the signalised shuttle length is not one the Audit Team has met before. While the indicative signal staging is simple, the inter-green timings and mid-shuttle vehicle detection are not clear. The location of the signal controlled NMU crossings some 50m after the vehicle stop lines will require sufficient time for vehicles to clear the crossings before NMUs can safely receive a green signal. The Audit Team wonder whether such long clearance times might lead to driver adaptation? Also, since the vehicle stop lines are remote from the signal crossings; would a driver who overruns the start of vehicle red or is then delayed by some unforeseen event, subsequently stop 50m later at the NMU crossing's red signal without a further stop line? Any failure to stop would pose a risk of vehicle/NMU collision

Recommendation – that proposals for vehicle detection, inter-green timings and stop line location are subject to early design discussion with traffic signals specialists to ensure safe operation.

Designer's Response:

The vehicle detection, inter-green timings and stop line locations are to be implemented where appropriate at as part of the next stage of design.

Network Management Decision:

5 File Ref: B1150/025 Audit Date: 16/08/2023



2.0 Alignment

2.1 Problem – vehicle/cycle overtake collisions

Location – Aylsham Rd under the rail bridge

The length of shuttle working is such that some drivers following an on-road cyclist may be tempted to overtake within it. The Audit Team note that proposed carriageway width under the rail bridge varies between 3.2m and approx. 4.5m. This could lead to driver misjudgement and inadequate safe overtaking clearance, resulting in collision.

Recommendation – that the carriageway width is regularised, avoiding tapering widths between 3.2 and 4.0m.

Designer's Response:

The carriageway width within the shuttle working length is to be reviewed once a Topo survey has been carried out, and the tapered width reduced in length to minimise the risk of collision between vehicles overtaking cyclists.

Edge of lane markings on the northern side of the carriageway are to be retained but realigned to achieve a clear width of 3.2m along the shuttle one way signalled working length and to guide high HGV's into the middle of the road when going under the arched rail bridge.

Network Management Decision:

2.2 Problem – tail-end collisions

Location – Park Lane into Aylsham Rd westbound

Traffic leaving the Park Lane gyratory into Aylsham Rd westbound may encounter stationary traffic at the proposed signals. A forward visibility splay of 25m is proposed here which is appropriate for speeds of 20mph. However the Audit Team consider that actual traffic speeds on this one-way un-calmed approach may be somewhat higher, leading to a risk of tail-end collision.

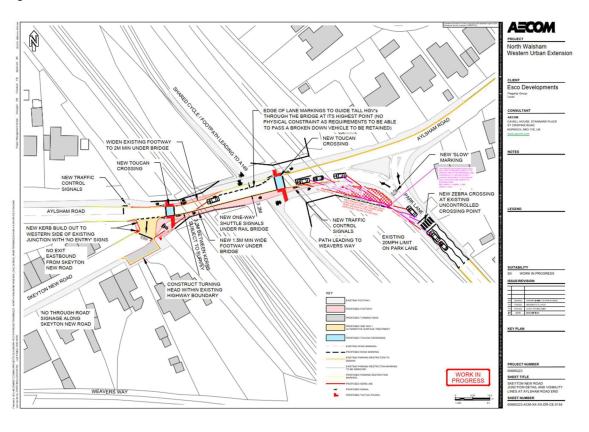
6



Recommendation – that the proposed visibility splay should be based on actual measured traffic speeds.

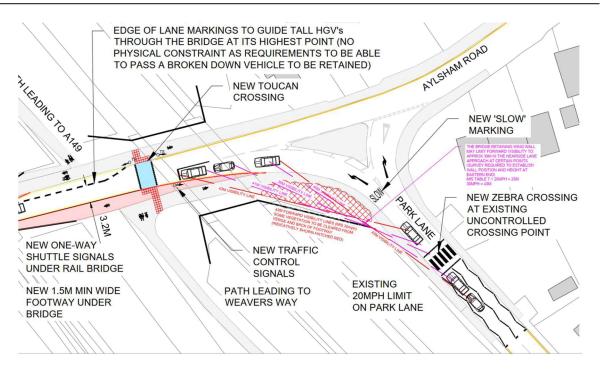
Designer's Response:

As suggested by the RSA1 comment above, a higher traffic speed of say 30mph would require a forward stopping sight distance of 43m. If the existing vegetation is adjacent to the railway embankment and retaining wall is trimmed back it may be possible to achieve the required 43m forward visibility. This would reduce down to approx 39m over a short distance where the existing bridge retaining wall would obstruct visibility. The exact position, length and height of the wall will require further survey work to establish achievable forward visibility although at present the visibility is greatly reduced by poorly maintained and overgrown vegetation.



7





We also propose the introduction of a zebra crossing at the existing drop kerb and tactile paved crossing on Park Lane would provide priority for pedestrians over vehicles and also help reduce traffic speeds on the present 20mph speed restricted approach to Aylsham Road, whilst also providing a new facility to access the cycle route and the surgery on Park Lane.

Network Management Decision:

3.0 Junctions

3.1 Problem – junction collisions

Location - Skeyton New Road one-way plug

The short length of one-way southbound operation may leave it prone to abuse. This concern is exacerbated by lack of any carriageway width restriction on the northbound side. This could result in northbound drivers emerging at the junction in collision with other traffic.

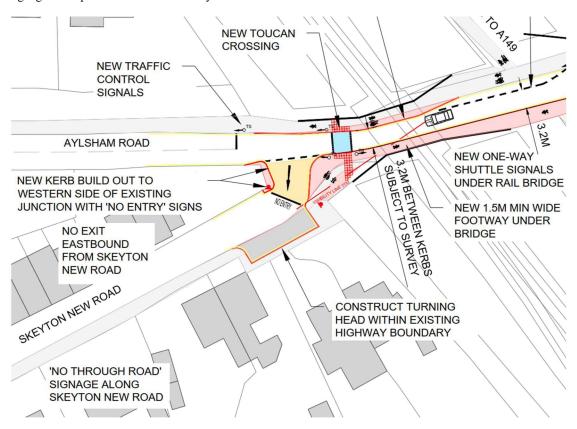
Recommendation – that the one-way section of the junction is redesigned, perhaps with a western kerbline build-out, to better deter northbound abuse of the restriction.

8



Designer's Response:

The junction of Skeyton New Road with Aylsham Road has been reviewed and the western side build-out widened to allow for new 'No Entry' signs facing northbound traffic. It is also proposed that access only signage is adopted on either end of Skeyton New Road.



Network Management Decision:

4.0 Non-motorised Users

4.1 Problem – collisions between NMUs and access traffic

Location – Norwich Road - RS Timber access/rail station access

The proposed RS Timber access bellmouth appears to be unnecessarily wide, increasing pedestrian and cycle exposure when crossing it, while the refuge area

Audit Date: 16/08/2023



between this and the station access is insufficiently wide to shelter a crossing cyclist. This increases the risk of NMU collision with turning/exiting traffic.

Recommendation – that the accesses are redesigned to better protect NMUs crossing them.

Designer's Response:

Noted. Detailed design works will be undertaken in relation to the proposals in this location including a Topo survey and highway boundary information. Careful consideration of the needs of all users will be needed. Where possible the RS Timber Works access will be narrowed increasing the protected areas for pedestrians and cyclists.

Network Management Decision:

4.2 Problem – vehicle/pedestrian collisions

Location – Norwich Road rail station access junction

The proposal appears to perpetuate the existing situation where pedestrians accessing/exiting the rail station must share the access carriageway with vehicular traffic at the junction. This exposes them to risk of collision with turning traffic and is likely to be intimidating for some.

Recommendation – that a footway should extend at least around the bellmouth area to protect pedestrians until clear of the junction area.

Designer's Response:

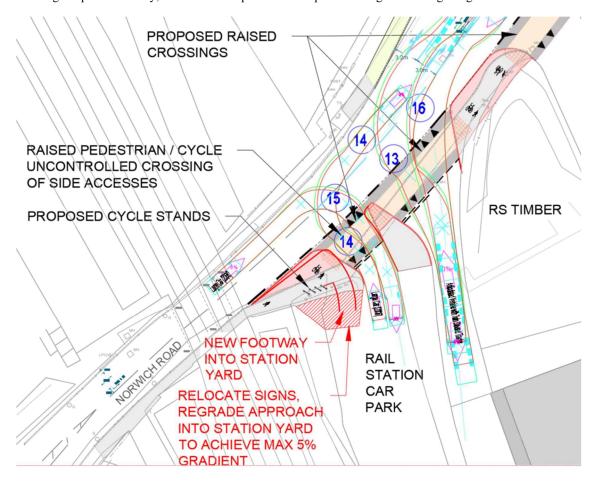
The available width of the existing station access is limited by the entrance to RS Timber to the north east and existing railway station signs and cabinet equipment to the south west.

The entrance could be improved to provide a separate footway for pedestrians if the existing signs and above ground cabinet equipment were relocated, however it is assumed that these features are beyond the limits of the highway boundary, and as such would require the railway companies permission. There is a large level difference between the station access and the adjacent footpath which would mean that the station access would require regrading into the station parking area again beyond the highway boundary. See extract from the

Tile Ref: B1150/025 Audit Date: 16/08/2023



proposed layout drawing 60685225-ACM-XX-XX-DR-CE-0155 below with a schematic alternate kerb layout showing a separate footway, this or similar options to be explored during detail design stage.





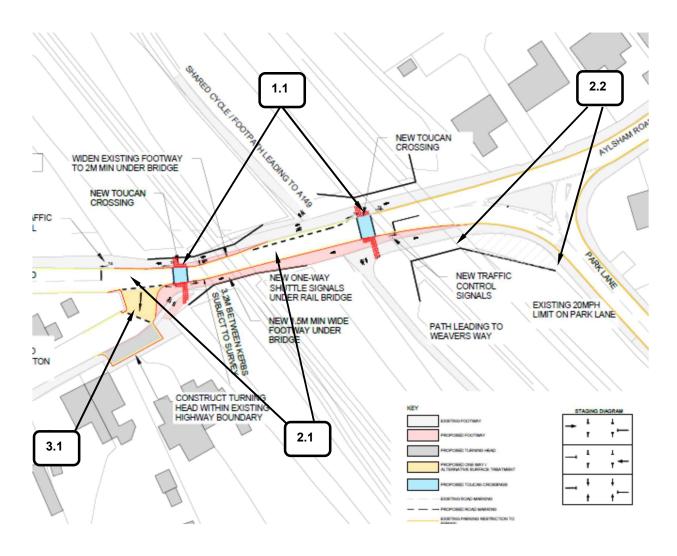
Network Management Decision:

5.0 Signs, Lighting and Markings

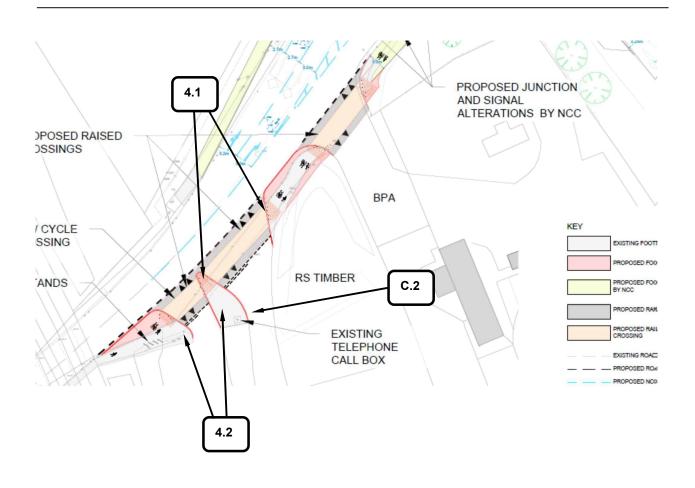
5.1 No comment



6.0 Problem Location Plans









AUDIT TEAM STATEMENT

We certify that this audit has been carried out in accordance with Norfolk County Council Community and Environmental Procedure SP03-07-P01

Dated 22 August 2023

Signed Kevin Allen

Dated 22 August 2023



APPENDIX A: Audit Brief

The following documents were submitted for this Road Safety Audit:

Document Ref.	Scale (if	Title
	applicable)	
60685223-ACM-XX-XX-DR-CE-0154 P02		Skeyton New Rd Junction Detail
60685223-ACM-XX-XX-DR-CE-0152 P02		Skeyton New Rd Visibility Lines
60685223-ACM-XX-XX-DR-CE-0153 P01		Skeyton New Rd Vehicle Turning Paths
60685223-ACM-XX-XX-DR-CE-0155 P01		Norwich Rd Cycle Provision
60685223-ACM-XX-XX-DR-CE-0156 P01		Norwich Rd Vehicle Turning Paths
Forecast Traffic Data		
5 yr road accident details		

No Departures from Standard were notified



APPENDIX B: Comments

C.1 The Audit Team note that visibility at the western end Skeyton New Rd is currently restricted by adjacent hedge and weed growth which has been allowed to encroach right up the carriageway edge. Although this is an existing situation, some increased use of the junction will arise from the proposed one-way plug at the other end of Skeyton New Rd. Discussion with the local highway authority is suggested with a view to remedial measures to improve visibility.



Designer's Response:

Accepted. This will be discussed with the Highway Authority as part of delivery of the works on Skeyton New Road at the next stage of design.

C.2 On Norwich Road the 'existing telephone call box' noted on the drawings at the station access no longer exists.

Designer's Response:

Noted

emplate Version #11 09/14

Tile Ref: B1150/025 Audit Date: 16/08/2023



NORTH WALSHAM WESTERN EXTENSION: B1150 COLTISHALL TRAFFIC MANAGEMENT

STAGE 1 SAFETY AUDIT

REPORT REF: **B1150/026** August 2023

Report Prepared for: AECOM



Report Author: Nevil Calder BSc(Hons) CEng MICE MCIHT MSoRSA NH Cert Comp

Report Status:

Issue	Status	Purpose	Name/Signature	Date
1	Stage 1 Safety Audit Report	Client issue	Nevil Calder	22/08/23
2	Designer's Response	Designer response to Safety Issues raised	Bevin Carey	27/09/23
Choose an item.	Choose an item.	Choose an item.		

North Walsham Western Extension: B1150 Coltishall TM Stage 1 Safety Audit



INTRODUCTION

This report contains the results of a Stage 1 Safety Audit carried out on the above scheme. The Audit was carried out at the request of AECOM on behalf of Norfolk County Council Growth and Development. A formal Audit Brief was not provided.

The Audit Team is independent of the project design team and has had no involvement with the project. The Audit Team membership was as follows:-

Nevil Calder BSc(Hons) CEng MICE, MCIHT, MSoRSA (Audit Team Leader)

Principal Engineer Highway Safety

WSP

Kevin Allen BEng (Hons), I Eng, MCIHT, MSoRSA (Audit Team Member)

Project Engineer

Network Safety + Sustainability

Norfolk County Council

The Audit took place via online conferencing on 16 August 2023. The audit comprised an examination of the supplied documentation (see Appendix A) and a site inspection by the Audit Team Leader on 22 August 2023 at 09:30 which lasted around 30 minutes. During the site visit the weather was sunny and the road surface dry. Traffic flows were moderate and generally free flowing. Speeds varied depending on traffic flow but were frequently observed to be above 20mph.

The terms of reference are as described in Community and Environmental Services Highways Service Manual Procedure SP03-07-P01. The Auditors have examined and reported only on the road safety implications of the scheme within the main report.

The proposal involves traffic management improvements in Coltishall in connection with the planned western urban extension of North Walsham. The audited scheme involves provision of a right turn lane at the junction of B1150 and B1354 including relocation of a pedestrian refuge, together with provision of bus stop markings on Church St approx. 100m to the north.

3 File Ref: B1150/026 Audit Date: 16/08/2023

North Walsham Western Extension: **B1150 Coltishall TM** Stage 1 Safety Audit



The auditors have reviewed the five-year (to end Mar 2023) collision record for the location. During this period there were 2 personal injury collisions (both slight) recorded in the vicinity of the scheme. One involved centreline crossover on the bend just north of the B1354 junction, reflecting the narrow carriageway there. The other occurred at the bridge to the west but appears anomalous, involving manoeuvring to give precedence to an emergency vehicle.

A comments section has been included in Appendix B. The issues noted are not necessarily safety issues. They relate either to wider network implications, safety issues identified outside the scope of the audited scheme or suitability of a particular design choice.

File Ref: B1150/026 Audit Date: 16/08/2023



ITEMS RAISED AT PREVIOUS AUDIT

The Audit Team are not aware of any previous audit of this scheme.

ITEMS RAISED AT THIS STAGE 1 AUDIT

- 1.0 General
- 1.1 No comment

2.0 Alignment

2.1 Problem – kerb strikes/loss of control or head-on collisions

Location – B1150 westbound at proposed RTL

The RTL layout reduces the width of the westbound through-lane where it passes the western corner of the filing station. There is a low brick wall here immediately at the carriageway edge (see photo), raising concern over vehicle edge strikes with potential for loss of control. Alternatively, drivers' natural 'edge-shyness' may cause them to overrun the RTL resulting in head-on collision with an eastbound vehicle entering it.



Recommendation – that the westbound through-lane should be a minimum of 3.2m adjacent to the low brick wall of the filling station and 3m elsewhere. The swept paths



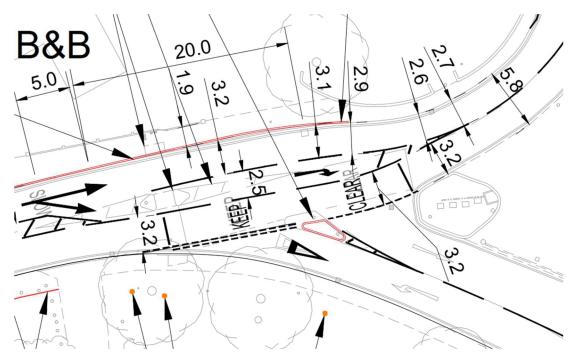
File Ref: B1150/026



suggest that the proposed RTL might be shortened slightly at its eastern end to facilitate this.

Designer's Response:

The Westbound through lane width has been reviewed and the design adjusted to achieve the suggested 3.2m width adjacent to the low height wall on the boundary of the service station.



Network Management Decision:

2.2 Problem – kerb strikes/loss of control

Location – B1150 westbound at proposed refuge island

The proposal indicates a westbound through-lane width of only 3m between kerbs where it passes the refuge island. On a classified road this is considered inadequate (despite the 20mph speed limit), raising the risk of vehicle kerb strikes with potential for loss of control.

Recommendation – that the through-lanes adjacent to the refuge island should be a minimum of 3.2m between kerbs

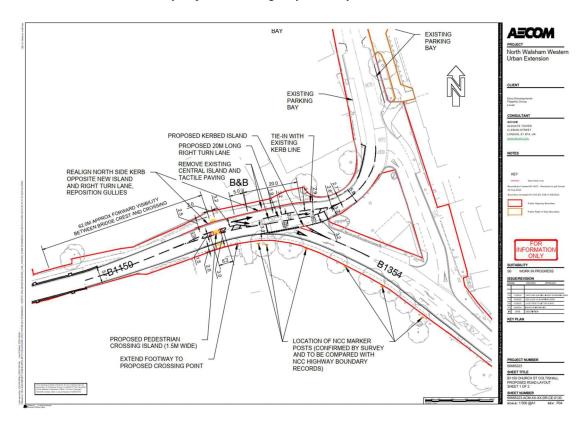
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Designer's Response:

The through lane widths adjacent to the proposed pedestrian refuge island have been increased to 3.2m as recommended by para 2.2 above.

To achieve 3.2m wide through lanes each side of the pedestrian refuge, the existing northern kerb line has been shifted northwards as indicated in the extract below. The revised drawing 60685223-ACM-XX-XX-DR-CE-0130-P04 also shows the recently acquired NCC Highway boundary details.



Network Management Decision:

3.0 Junctions

3.1 No comment

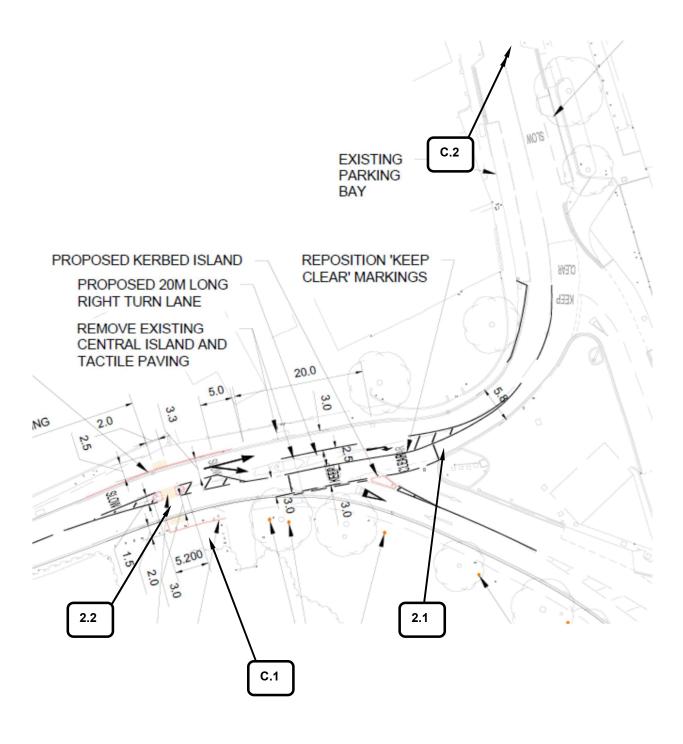
North Walsham Western Extension: B1150 Coltishall TM Stage 1 Safety Audit



- 4.0 Non-motorised Users
- 4.1 No comment
- 5.0 Signs, Lighting and Markings
- 5.1 No comment



6.0 Problem Location Plan



Template Version #11 09/14 KJA

File Ref: B1150/026 Audit Date: 16/08/2023

North Walsham Western Extension: B1150 Coltishall TM Stage 1 Safety Audit



AUDIT TEAM STATEMENT

We certify that this audit has been carried out in accordance with Norfolk County Council Community and Environmental Procedure SP03-07-P01

Signed (ATL) Nevil Calder

Dated 22 August 2023

Signed K.J. W. Kevin Allen

Dated 22 August 2023

North Walsham Western Extension: B1150 Coltishall TM Stage 1 Safety Audit



APPENDIX A: Audit Brief

The following documents were submitted for this Road Safety Audit:

Document Ref.	Scale	Title
	(if applicable)	
60685223-ACM-XX-XX-DR-CE-0130 P03	1:500	Proposed Road Layout (1 of 2)
60685223-ACM-XX-XX-DR-CE-0133 P01	1:500	Proposed Bus Stop
60685223-ACM-XX-XX-DR-CE-0131 P04	1:250	Vehicle Tracking (1 of 3)
60685223-ACM-XX-XX-DR-CE-0134 P03	1:250	Vehicle Tracking (2 of 3)
60685223-ACM-XX-XX-DR-CE-0135 P04	1:250	Vehicle Tracking (3 of 3)
Forecast Traffic Data		
5 yr road accident details		

No Departures from Standard were notified



APPENDIX B: Comments

C.1 The swept path shown for a tanker exiting the pump house to the west (turning left) overruns an area of third party land to the west of the access. This may not therefore be practicable, rendering the manoeuvre impossible with the proposed refuge location. It is suggested that this be discussed with Anglian Water at an early stage to confirm the viability of the proposal.

Designer's Response:

The tanker provision to the pump house facility is to be discussed in detail with Anglian Water.

C.2 It was noted that Dwg 0133 omits a section of existing on-street parking bays on the eastern side just south of the war memorial.

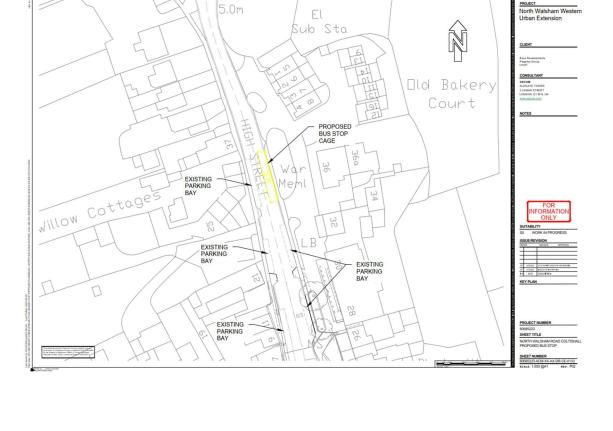
Designer's Response:

Noted that existing on-street parking bay was missing from drawing. This has now been added to Drg ...1033-P02.

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Tile Ref: B1150/026 Audit Date: 16/08/2023

AECOM



Grove House

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Tile Ref: B1150/026 Audit Date: 16/08/2023